NAVAL POSTGRADUATE SCHOOL
Monterey, California

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THESIS

DISPERSION SENSITIVITY OF THE EIGHT INCH
ADVANCED RAMJET MUNITIONS TECHNOLOGY
PROJECTILE DUE TO WIND
AND MINOR THRUST ERRORS

by

Steven Ronald Poole

September 1984

Thesis Advisor: A. E. Fuhs

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SHORT PERIOD RESONANCE
THRUST-DRAG BALANCE

20. ABSTRACT *(Continue on reverse side if necessary and identify by block number)*

Advanced Ramjet Munitions Technology (ARMT) is an ongoing project within the Defense Advanced Research Projects Agency (DARPA) to research ramjet munitions. The ARMT eight inch projectile uses ramjet thrust for a boosted trajectory, but operates on a thrust drag balance concept to create a pseudo-vacuum trajectory during powered flight. The trajectory was

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constant thrust errors under 5% was within a 600 foot radius
at terminal guidance over a range of 33 miles.

Dispersion Sensitivity of the Eight Inch
Advanced Ramjet Munitions Technology Projectile
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Submitted in partial fulfillment of the
requirements for the degree of

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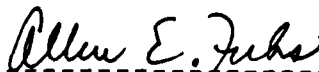
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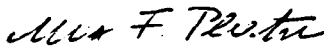
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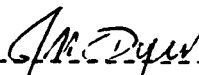
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ABSTRACT

Advanced Ramjet Munitions Technology (ARMT) is an ongoing project within the Defence Advanced Research Projects Agency (DARPA) to research ramjet munitions.The ARMT eight inch projectile uses ramjet thrust for a boosted trajectory, but operates on a thrust drag balance concept to create a pseudo vacuum trajectory during powered flight.The trajectory was analyzed using an IBM 370 computer simulation for three and five degrees of freedom. Work was also done to adapt the Ballistics Research Laboratories six degrees of freedom program to the IBM system.Projectile aerodynamic and mass properties were obtained from the Norden Systems Wind Tunnel Data. Dispersion from the vacuum trajectory due to wind prior to ramjet burnout proved minor.Dispersion due to constant thrust errors under 5% was within a 600 foot radius at terminal guidance over a range of 33 miles.

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TABLE OF SYMBOLS AND ABBREVIATIONS

ABBREVIATIONS:

AIFS -ADVANCED INDIRECT FIRE SYSTEM

ARMT -ADVANCED RAMJET MUNITIONS TECHNOLOGY

BRL -BALLISTICS RESEARCH LABORATORY

IODE -INTERACTIVE ORDINARY DIFFERENTIAL EQUATION
          SOLVER

NPGS -NAVAL POSTGRADUATE SCHOOL

SYMBOLS:

FORMULA	PROGRAMS	DESCRIPTION	UNITS
α	A	angle of attack	radians
β	B	sideslip angle	radians
δ	DE	angle between body axis and inertial axis (yaw plane)	radians
γ	GA	angle between inertial axis and relative wind, yaw plane	radians
λ	LAMBDA	wavelength	feet
ρ	RO	air density	$lbf-s^2/ft^4$
ω	-	angular velocity	rads/sec
Ω	O	angle between relative wind and inertial axis (pitch plane)	radians
θ	THE	angle between body axis and inertial axis(yaw)	radians
C_d	CD	drag coefficient	

C_{do}	CDO	zero lift drag coefficient	
C_l	CL	lift coefficient	
C_{l_α}		slope lift coefficient	
C_m	CM	moment coefficient	
C_{m_α}	CMA	slope moment coefficient	
C_{mq}	CMT	damping coefficient	
X_{cp}		centre of pressure location(from spike)	inches
X_{cg}		centre of gravity location(from spike)	inches
C	C	thrust error coefficient	
d	DI	projectile diameter	inches
D	DRAG	Drag	lbf
D_w		Drag due to wind	lbf
f		frequency	Hz
g	G	gravity	ft/sec
I	I	moment of inertia	slug-ft
I_{sp}	ISP	specific impulse	"sec"
L	L	lift	lbf
L_w		net lift due to transients	lbf
m	M	mass	lbm
q	Q	dynamic pressure	lbf/ft^2-s^2
U	V	relative wind	ft/sec
V		initial velocity projectile	ft/sec

Vcg	VCG	centre of gravity velocity	ft/sec
Vw	VW (3 deg) VWXY(5 deg) VWXZ(5deg)	wind velocity	ft/sec
Vwo		initial wind speed	ft/sec
X	X	range	ft
Y	Y	crossrange	ft
Z	Z	height	ft

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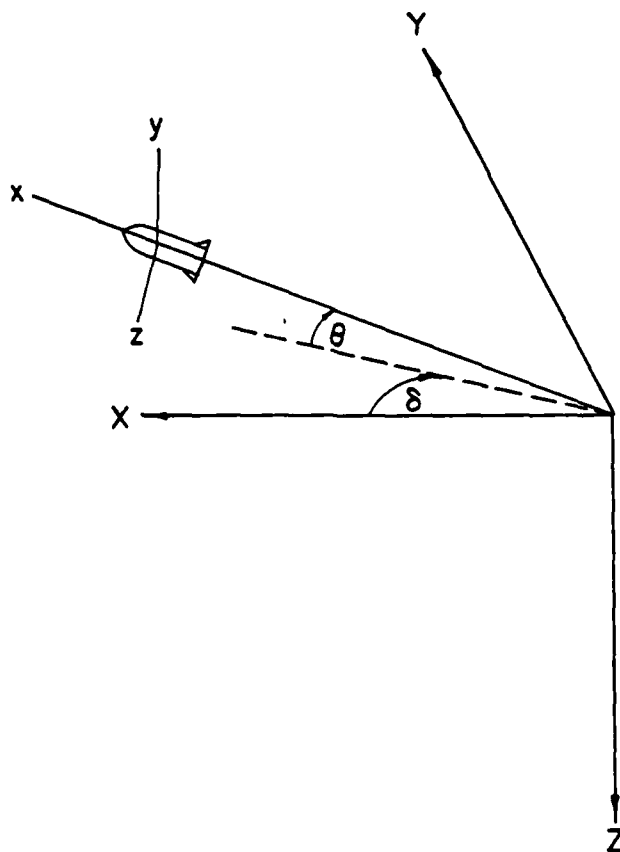
ACKNOWLEDGEMENT

I wish to thank John Croce of Scientific Applications Incorporated, Martin Fink of United Technologies Norden Systems, Colonel Rene Larriva of Defence Advanced Research Projects Agency ,Dr. Charles Murphy of the Ballistics Research Laboratories and their associates for the time, advice and resources they provided me for this thesis.I most gratefully thank the Distinguished Professor Allen Fuhs for his support and patience in introducing me to the ballistics field and establishing such worthy contacts. Without his interest in allowing me to pursue this subject I could never have achieved even a rudimentary introduction to ballistics.

I would be remiss if I did not thank my wife, Marie Josee, and my two children,Crista and Eric, for helping create the atmosphere I needed to succeed in the academic environment.

I. INTRODUCTION

A. ARMT OPERATIONAL CONCEPT

Conventional artillery uses unguided projectiles to destroy a variety of targets including armored vehicles. Ballistic information and professional experience are used to direct fire onto a target with little chance of a direct hit in the first few rounds. A forward observer provides feedback to the guns for correction until the target is destroyed with subsequent rounds. Generally this approach is limited to the 30 kilometer range and often point target locations are not known.

The ARMT projectile, formerly called AIFS, changes the conventional concept by providing a fire and forget, boosted and terminally guided projectile with a highly predictable trajectory. Conventional heat seekers and target identification systems are short range and require a blunt nose which has high drag. Active radar is not practical. Long ranges of 60 kilometers are achieved by using solid fuel ramjet propulsion with an axisymmetric air inlet spike. An accurately predicted trajectory is achieved by ensuring thrust equals drag to produce zero axial acceleration and create a pseudo-vacuum trajectory during powered flight. At a preset time (near ideal condition ramjet burnout) the inlet spike is discarded and canards are deployed for

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terminal guidance control. A passive or reflected target energy system will be used for terminal guidance. Research is ongoing and sponsored by DARPA. Projectile characteristics are at Appendix A.
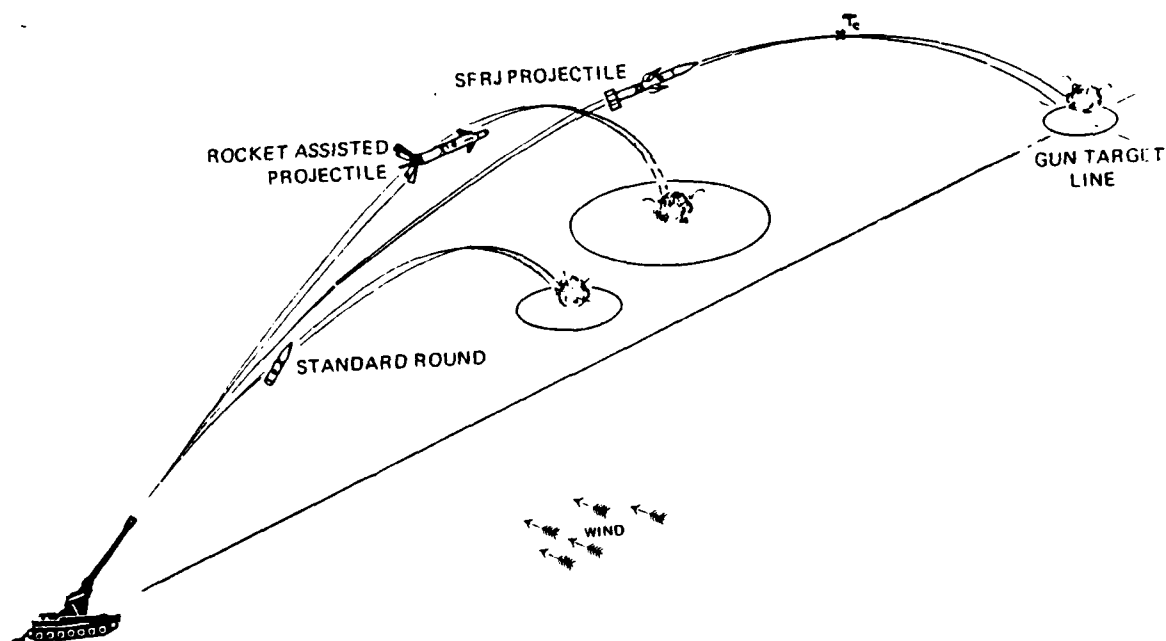
Figure 1-1 ARMT Trajectory Concept

B.   THRUST DRAG BALANCE CONCEPT

Balanced thrust drag implies that the thrust equals the drag vectors during powered flight. The aim of the balance is to negate meteorological variations throughout the trajectory by reducing all force vectors to zero except gravity. The resulting pseudo-vacuum trajectory is highly predictable. The balance is accomplished by measuring axial acceleration and maintaining it at zero.Appendix B explores this concept in detail.   The potential errors include transients due to wind induced reactions and measurement errors in the technical application of the balance in flight. Further, any asymmetries such as aerodynamic misalignment or thrust will produce a lateral force which must be offset by a small roll rate(sixth degree of freedom).   This allows longitudinal forces to be the significant forces.

The concept of thrust drag balance is best demonstrated in Figures 1-2 and 1-3.In Figure 1-2 the centre of gravity of the projectile is flying at an angle of attack (alpha) with a velocity vector (Vcg) relative to a fixed earth reference frame. The aerodynamic forces are lift(L) and drag(D). Assuming static static stability and neglecting transient dynamics, the angle of attack becomes zero, which

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reduces lift to zero.If thrust equals drag then only the gravitational force exists.

If a crosswind(Vw) is applied, the projectile cocks into the wind because of the aerodynamic force acting on the centre of pressure. Adjusting the thrust and again assuming static stability the drag can be offset as shown in Figure 1-3 by applying the correct thrust.For future reference the component of drag normal to the plane containing Vcg is Dw.
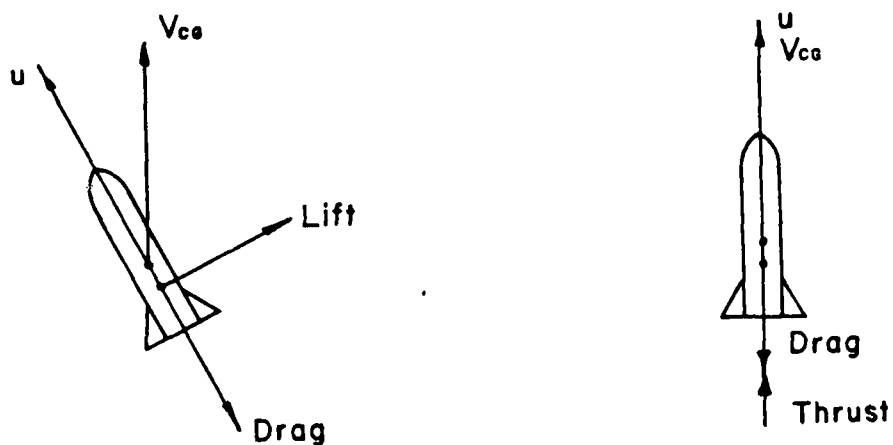
Figure 1-2 Projectile Dynamics Thrust Equals Drag

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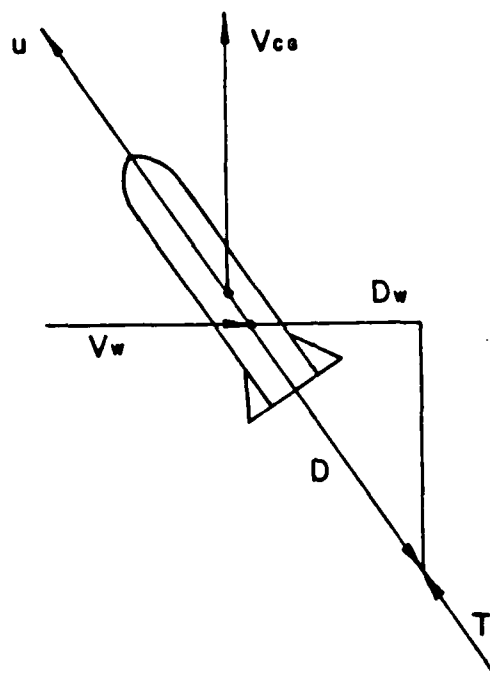
Figure 1-3 Projectile Dynamics With Crosswind

If a tailwind or headwind is applied, thrust is adjusted
to compensate in the same manner.

The dynamics or transient effects due to wind which
create damped oscillatory motion have a cumulative net lift
effect(as shown in Figure 1-4) as angle of attack is
proportional to lift.The area under the curve in Figure 1-4

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does not average to zero due to the damping. For future reference this lift due to wind will be referred to as Lw.
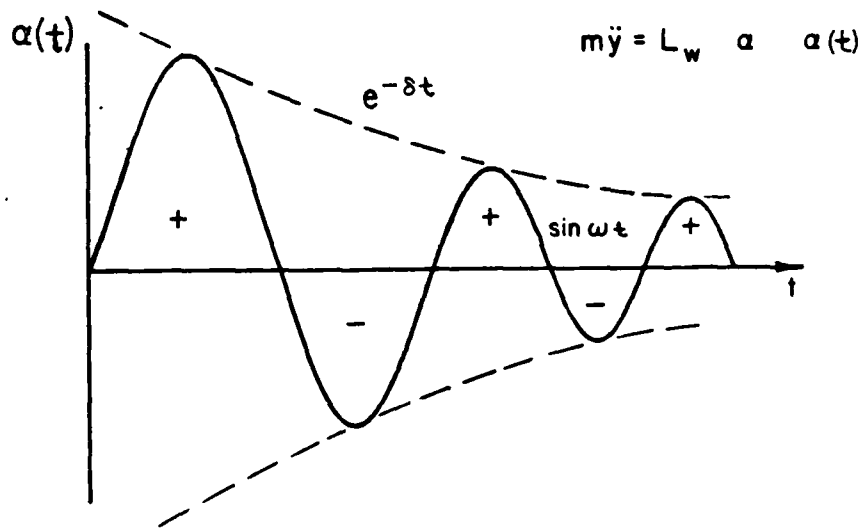
Figure 1-4   Angle Of Attack Versus Time

Calculations integrating alpha(t) twice to demonstrate the above in the yaw or pitch plane are at Appendix B.

C.   THESIS SCOPE

It is emphasized that the scope of this thesis is to analyze dispersion from the pseudo-vacuum trajectory at terminal guidance time for the eight inch ARMT projectile. In colloquial terms the "basket " from which the projectile will be guided to target was determined. Further, this basket is based on thrust errors and wind effects for a

launch angle of 45 degrees and muzzle velocity of MACH 2.2 at sea level. Linearized aerodynamics were used in all calculations. No attempt was made to establish a "footprint" for projectile impact.

II. TRAJECTORY ANALYSIS METHODOLOGY

A. VACUUM TRAJECTORY ANALYSIS

A short and simple BASIC program was written to establish the vacuum trajectory and fuel burn time of the projectile in a two dimensional scenario where thrust exactly equaled drag. The Standard U.S. Atmosphere was used and the drag coefficient linearized [Reference 1]. The program listing and baseline data are at Appendix D. The key parameters and equations used are listed at Appendices A and D.The baseline pseudo-vacuum trajectory is shown in Figure 2-1.

B. THREE-DEGREES-OF-FREEDOM MODEL

The computer simulation was established using the Interactive Ordinary Differential Equation (IODE) library program at NPGS. A listing of the three degrees of freedom equations is in the IODE specifications at Appendix E. The simulation is based on wind tunnel results from Norden Systems [References 2 and 3] and assumes a horizontal plane at 30000 feet altitude.This height was chosen as significant flight time is at altitude and the time of flight in this plane was near actual flight time. Primarily the model was used to study crosswind effects but resonance with the projectile short period was simulated. Different thrust

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scenarios were also used. Figure 2-2 depicts the model in the X-Y plane.

burnout time=101 secs
burnout range=175100 feet
burnout height=10990 feet
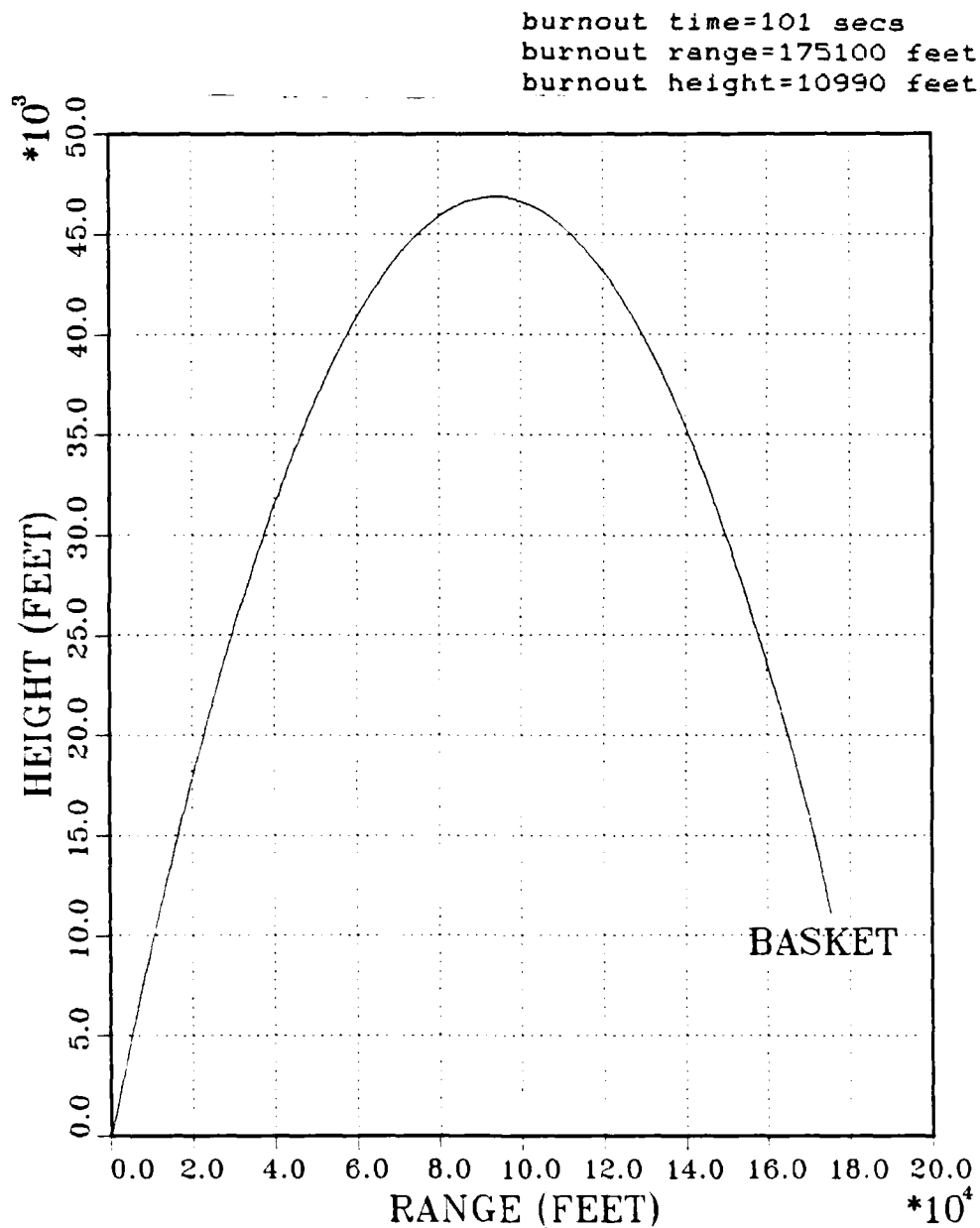
Figure 2-1 ARMT Pseudo-vacuum Trajectory

$$I\ddot{\theta} + f(Cm_q)\dot{\theta} + f(Cm_\alpha)\theta = f(Cm_\alpha)\gamma$$
$$m\ddot{x} = L\sin\gamma - D\cos\gamma$$
$$m\ddot{y} = L\cos\gamma + D\sin\gamma$$
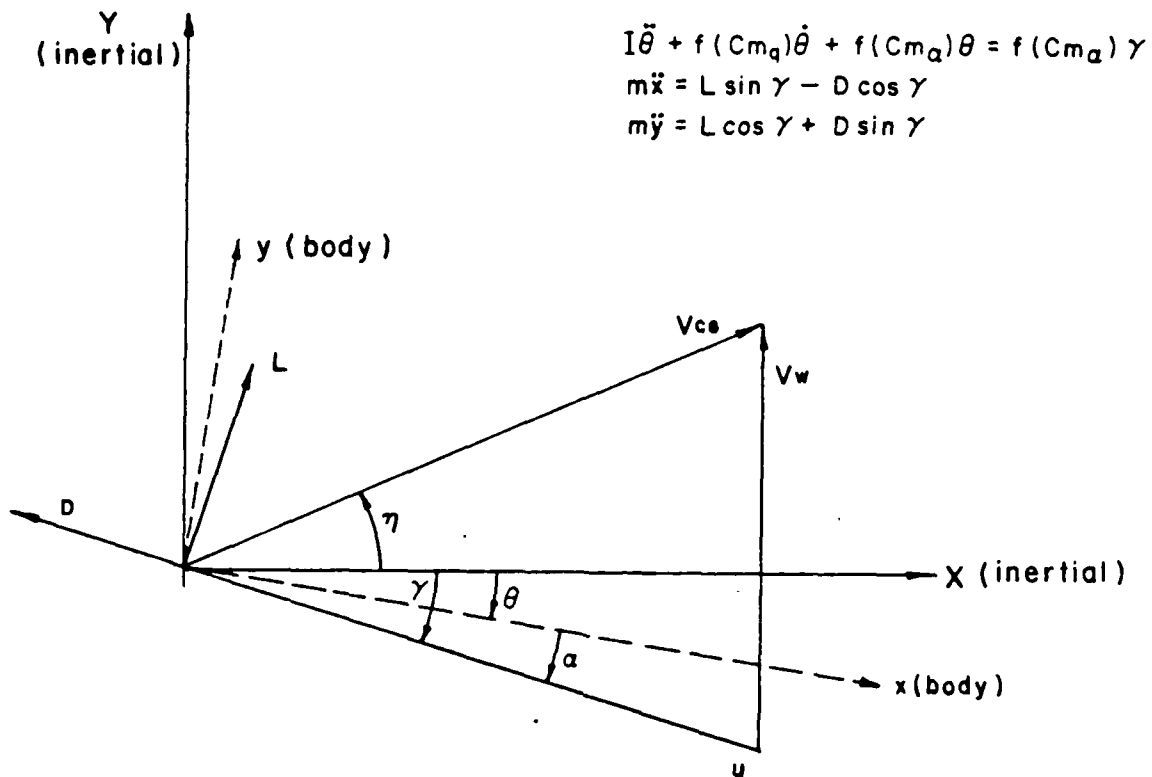
Figure 2-2   Three Degrees Freedom Model (Yaw Plane)

The crosswinds were varied in intensity and duration to
analyze crossrange dispersion.   As well thrust was varied as
a function of drag by scaling the drag. Cmq predictions were
approximately -190 to -205 by Norden Systems [Reference 2]
and an analysis was done to determine the effects of varying
this damping coefficient.   To further study the projectile
characteristics, trajectories were simulated with no thrust
or mass attenuation with varying wind profiles. Figure 2-3 ,

shows the baseline three-degrees-of-freedom trajectory of thrust equals drag with no wind.
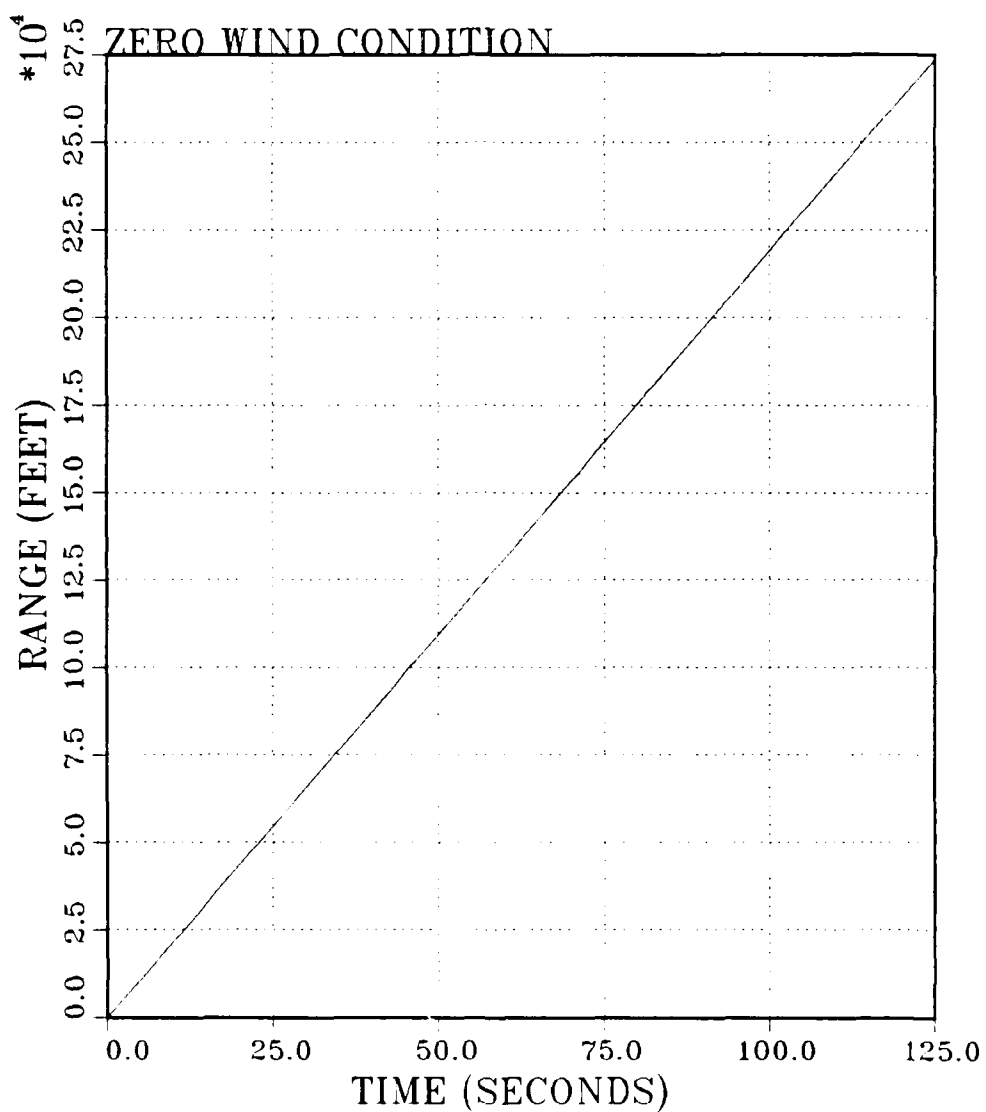
Figure 2-3   Baseline   Three-Degrees-Of-Freedom Trajectory

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C. FIVE-DEGREES-OF-FREEDOM MODEL

Again the IODE program was used to solve a five degrees of freedom system of equations. The roll plane was neglected for the following reasons:

-the program could not accept sufficient functions to define six degrees of freedom.

-the fins are expected to damp out initial spin due to gun rifling (900 RPM) in the first few seconds of flight. Sufficient spin to average projectile asymmetry errors to zero but not enough to significantly affect dynamics will remain.(ie. gyroscopic effects and Magnus effects)

-the initial spin damping dynamics are beyond the scope of this thesis.

The projectile was assumed to be axisymmetric allowing for ease of calculations in the yaw and pitch planes. Figures 2-2 and 2-4 depict the yaw and pitch planes for the model,respectively.

A listing of the equations is provided in the IODE specifications at Appendix F. Trajectory simulations were run with varying wind profiles and thrust error scenarios. Terminal guidance time (Tc) was determined by the baseline five degrees of freedom trajectory shown at Figure 2-1 as 101 seconds. This trajectory has no wind and thrust exactly equaled drag until discard of the air inlet spike and

canard deployment.All simulations assumed a 45 degree launch angle and Mach 2.2 muzzle velocity. Dispersion from the pseudo-vacuum trajectory was measured at terminal guidance time including the following variables:

-X=range at 101 seconds
-Y=crossrange at 101 seconds
-Z=height at 101 seconds
-Tb=burnout time
-Vcg=speed at time 101 seconds

Dispersion is defined as the difference between value for perturbed trajectories and the baseline trajectory.
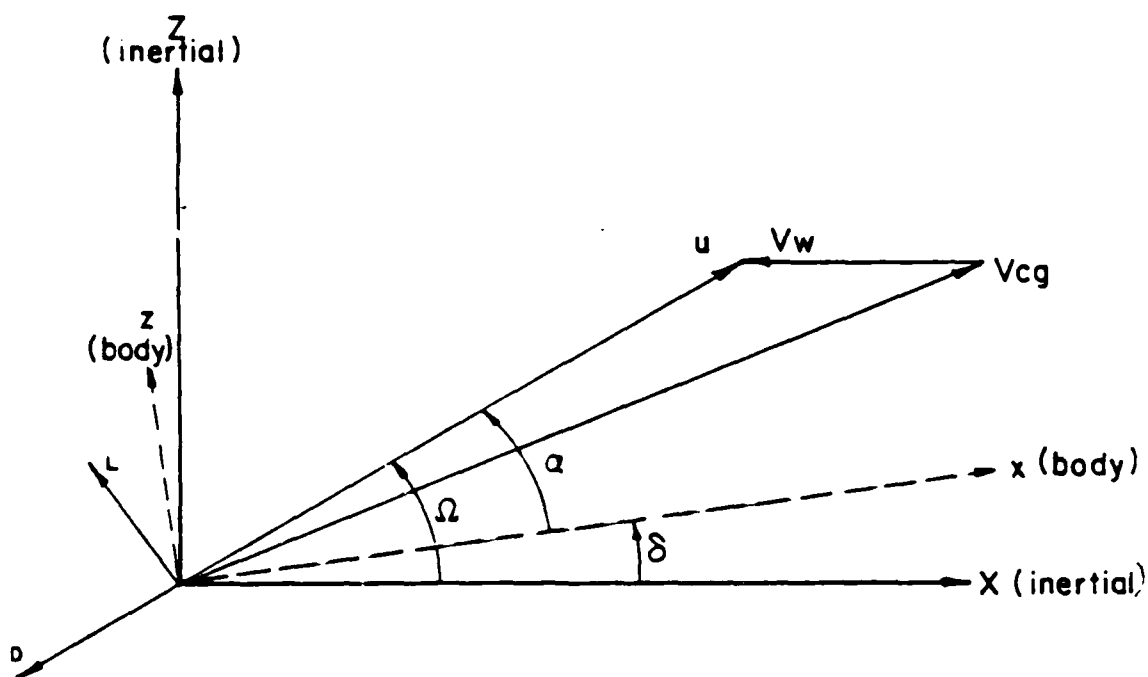
Figure 2-4 Five-Degrees-Of-Freedom Pitch Plane Model

D. SIX-DEGREES-OF-FREEDOM MODEL

The Ballistics Research Laboratories (Aberdeen) six degrees of freedom model HTRAJ was obtained and adapted for use on the NPGS IBM 370 system. The adapted listing is included as Appendix G. Program compilation was achieved but output data was not satisfactory due primarily to input data syntax problems. Further,the program requires extensive modification to be able to vary thrust as a function of drag with the ease of the previous models already described. Time was not available to correct these problems. Detailed documentation on tne program HTRAJ is available through BRL.

III. TRAJECTORY RESULTS

A. THREE DEGREES OF FREEDOM

1. Crosswind And Thrust Error Sensitivity

Figures 3-1 and 3-2 show the effects of constant thrust errors as a percentage of drag with no wind. Recall that the three-degrees-of freedom trajectory is at constant altitude. The figures therefore represent a thrust error sensitivity in terms of burn time and range variations due to drag or thrust. The trajectories all pass nearly through the 218000 foot range mark at t=100 seconds, but the burnout ranges are significantly different due to the varying burn times resulting from projectile thrust. Figure 3-2 demonstrates the obvious conclusion that the burnout time decreases as thrust increases.

Figure 3-3 combines the effects of constant crosswinds and thrust errors to demonstrate resultant cross range dispersion. The constant wind velocity lines are very nearly linear, and the pattern is essentially a shift about the zero-zero point. If thrust is less than drag, the dispersion is in the direction of the wind vector. If thrust is greater than drag then the overcompensation produces a dispersion opposite to the wind vector.
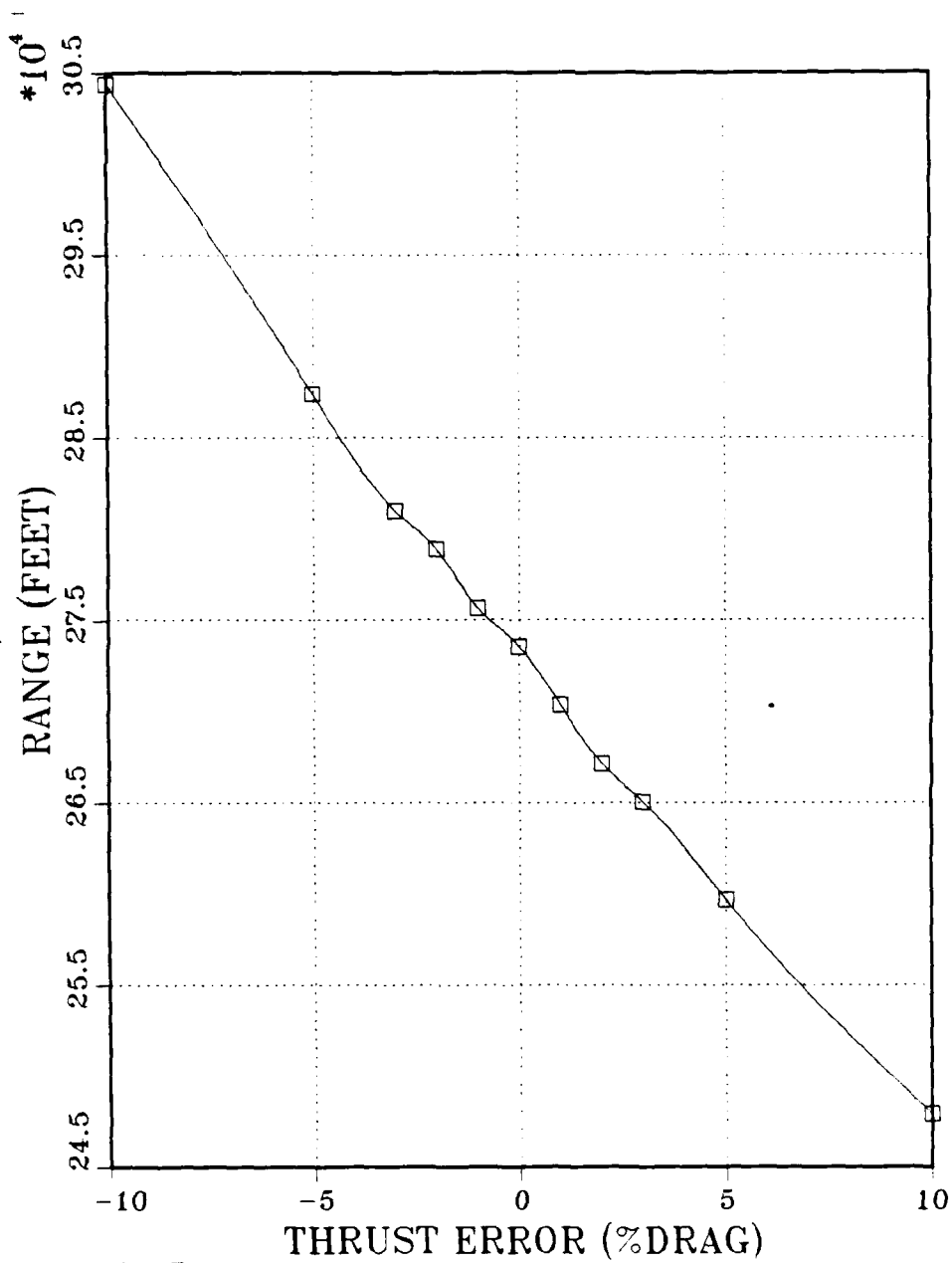
Figure 3-1 Thrust Error Sensitivity (Range)
Three Degrees Of Freedom

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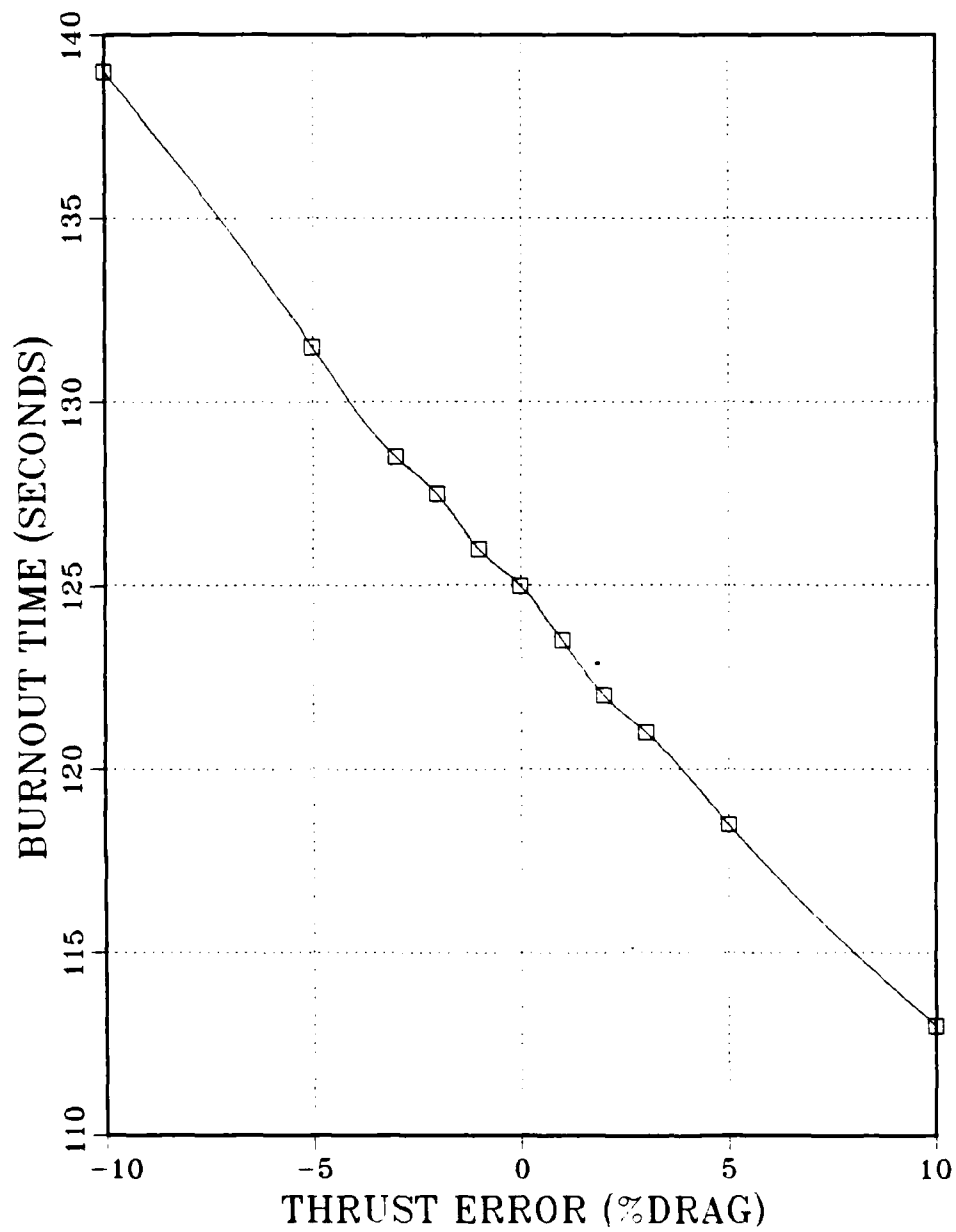
Figure 3-2 Thrust Error Sensitivity (Burntime)
Three Degrees Of Freedom

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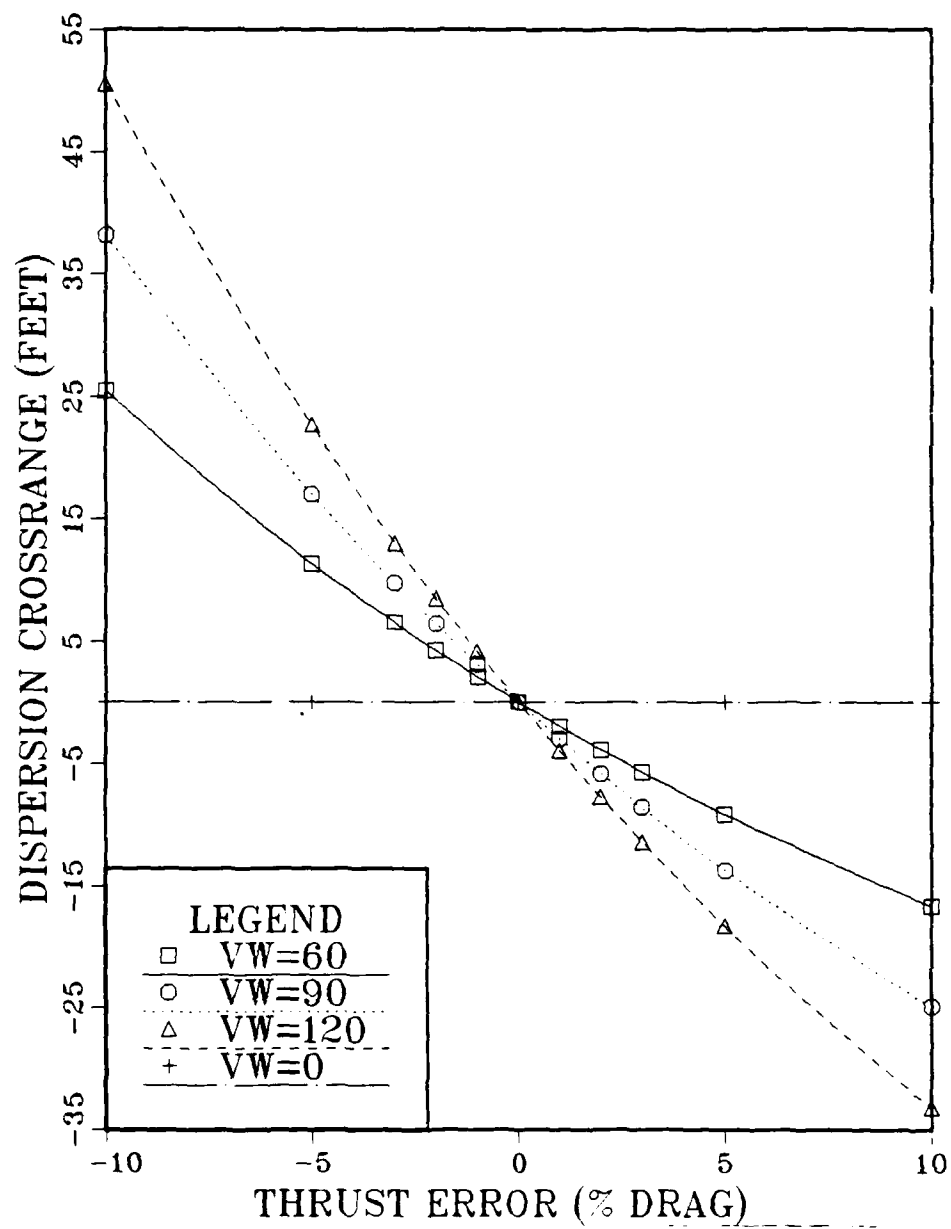
Figure 3-3 Crosswind Sensitivity Three Degrees Of
Freedom

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Of interest was the dispersion due to the same wind profiles without thrust or mass loss. This represents an absolute dispersion with a given wind profile. These results are in Table 3.1.

Table 3.1 No Thrust Crosswind Effects
Three Degrees of Freedom

Thrust=0   t=125 seconds

vw (ft/sec)	dispersion (feet) crossrange
0	0
60	195.76
90	293.80
120	392.02

The data clearly shows that crosswinds have a minimal effect in the thrusted scenarios. The dispersion in the thrust-equals- drag case is due to the transients (Lw) and is negligible as well. This is illustrated at Table 3.2.

Table 3.2 Dispersion Due to Net Lift
from Transients

Thrust=drag

vw (feet/sec)	dispersion (feet) crossrange
0	0
60	.018
90	.027
120	.036

.

Angle of attack damped to virtually zero during the trajectories (see Figure E-3) but the absolute maximum values were also recorded.Figure 3-4 demonstrates the relation between angle of attack (alpha) and the wind velocity.Thrust errors had virtually no effect on the angle of attack magnitude.
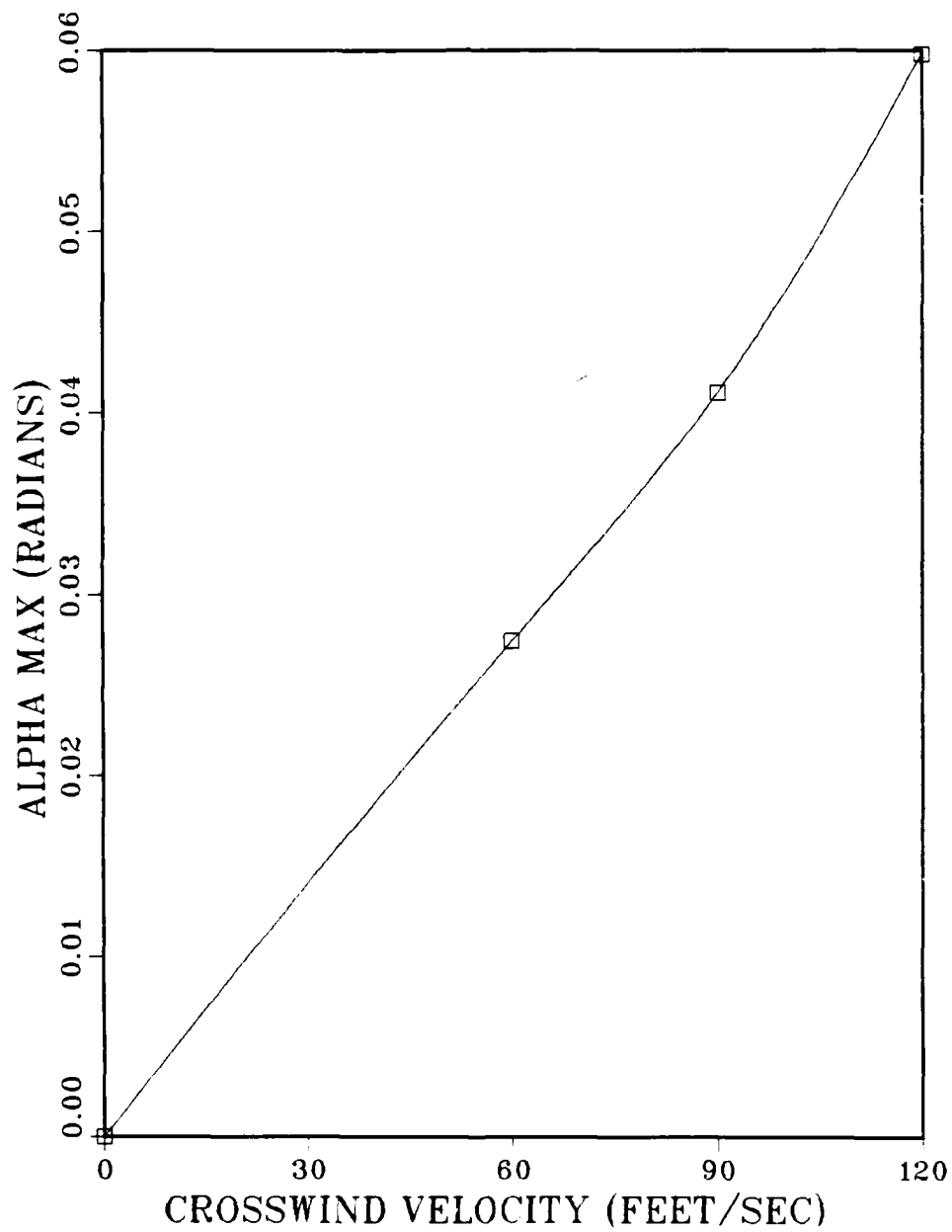
Figure 3-4 Wind Effects On Maximum Angle Of Attack

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2. Damping Coefficient Effects

The magnitude of Cmq was determined to be approximately -200 in the flight speed ranges of the ARMT projectile [Reference 4]. To determine if this coefficient significantly affected dispersion Cmq was varied from 0 to 1.9 x 10^6 and the dispersion recorded. Figure 3-5 shows the relation between Cmq and dispersion (crossrange) with a constant wind of 60 feet/second and time of 125 seconds.
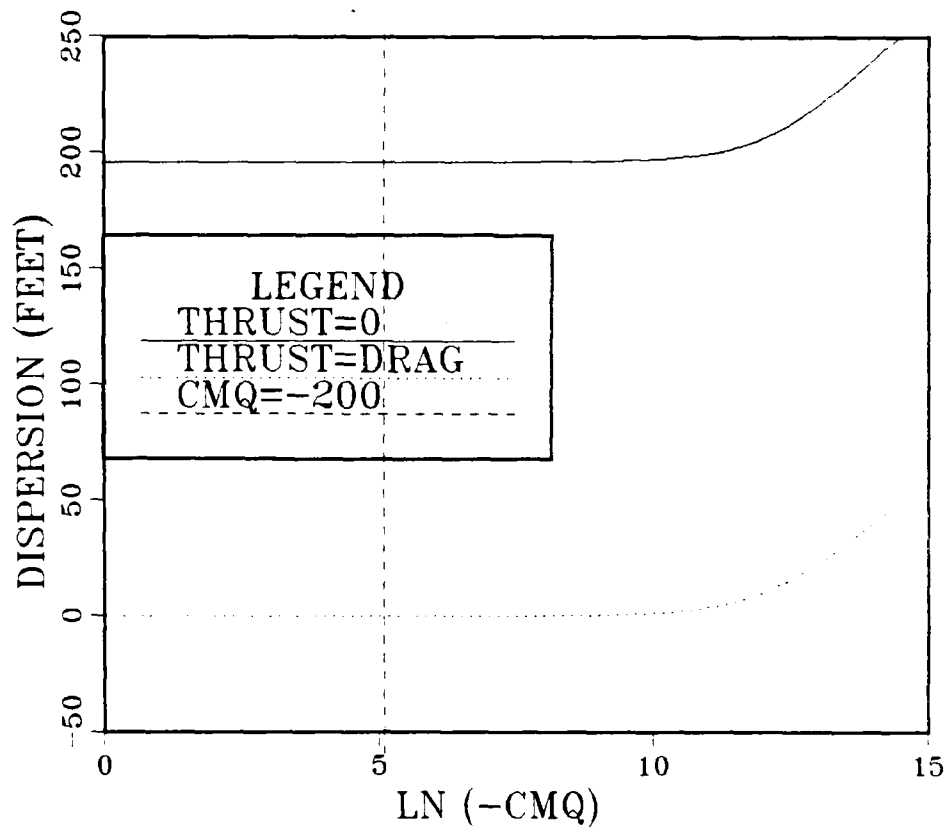
Figure 3-5 Damping Coefficient Effects

Careful examination of Figure 3-5 shows that dispersion increases slightly for realistic values of Cmq and is therefore proportional to Cmq.Due to the small sensitivity of dispersion to Cmq for all practical purposes one can conclude dispersion is independent to Cmq.(The increased dispersion proportional to Cmq can be explained as the difference in the areas under a highly damped sinusoid versus a non-damped sinusoid is considerable.)

3. Sinusoidal Wind Analysis

To test the effects of phase angles and wavelengths on the projectile dynamics a sinusoidal wind was input to test the model.The wind (Vw) was of the form Vo sin(2 PI Vo t/lambda + phase) where Vo was set at 60 feet/second.Figures 3-6 and 3-7 show the trajectories for the sine and cosine winds to burnout at thrust equal to 90% drag.(Lambda=range and lambda=.5 range)Of note is the fact that the sine wind produces a continuous dispersion while the cosine wind does not when thrust does not equal drag.This discovery led to an expanded study of different phase and wavelength sinusoidal wind inputs for various thrust scenarios.As well a simplified model was constructed as shown at Figure 3-8 and calculations confirmed the three degrees of freedom model results.Figures 3-9 and 3-10 depict the results of the calculations.
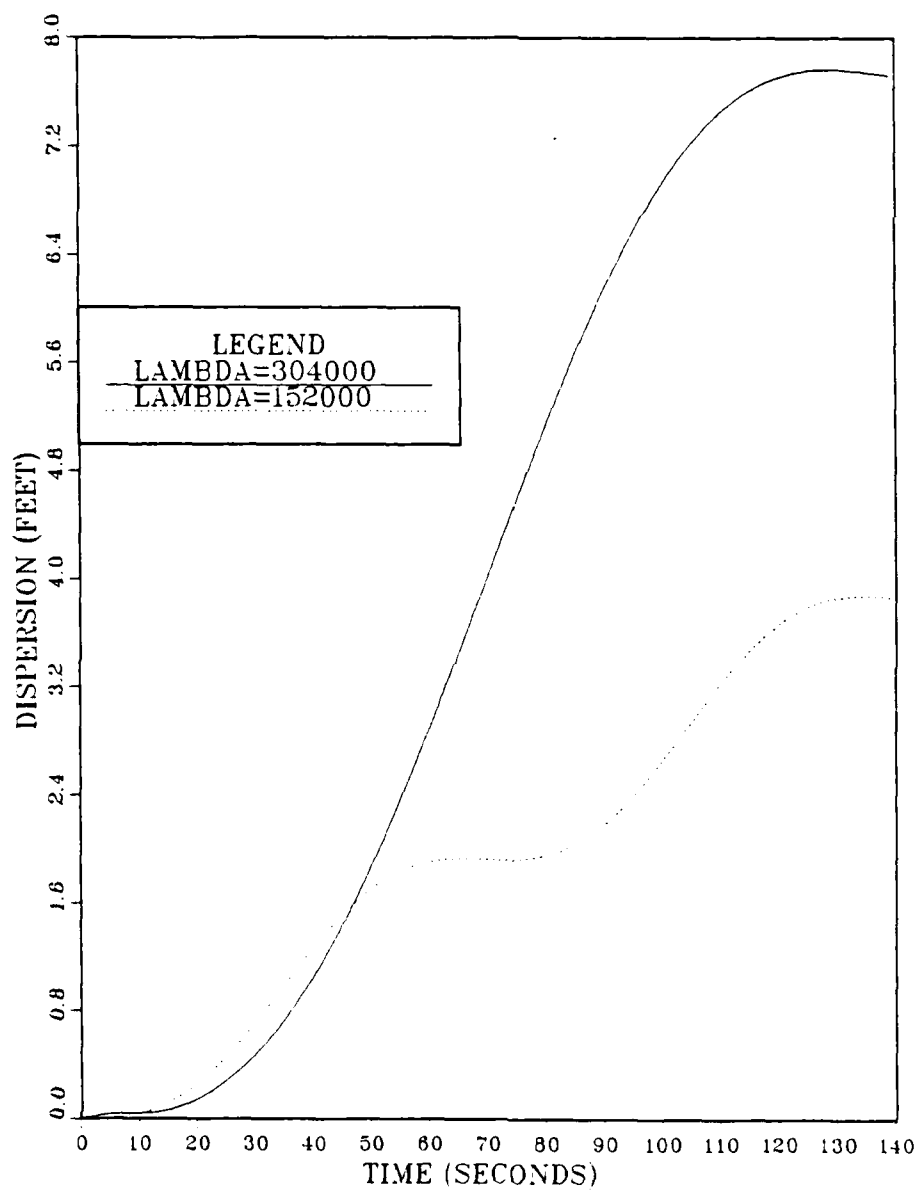
Figure 3-6 Sinusoidal Wind Effects (Sine)

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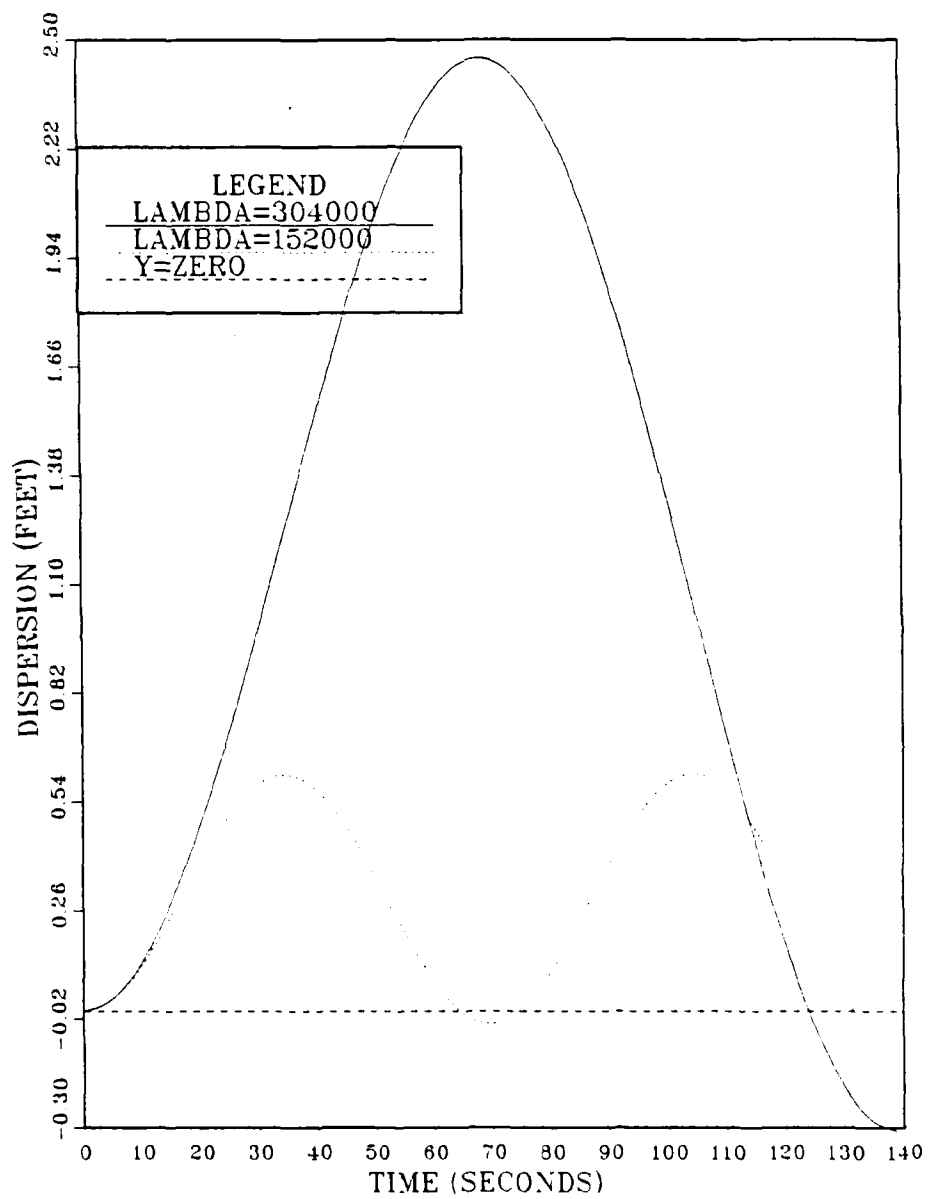
Figure 3-7 Sinusoidal Wind Effects (Cosine)

Y

Dx

Dy

D

Vcg Vw

η

X

γ

u
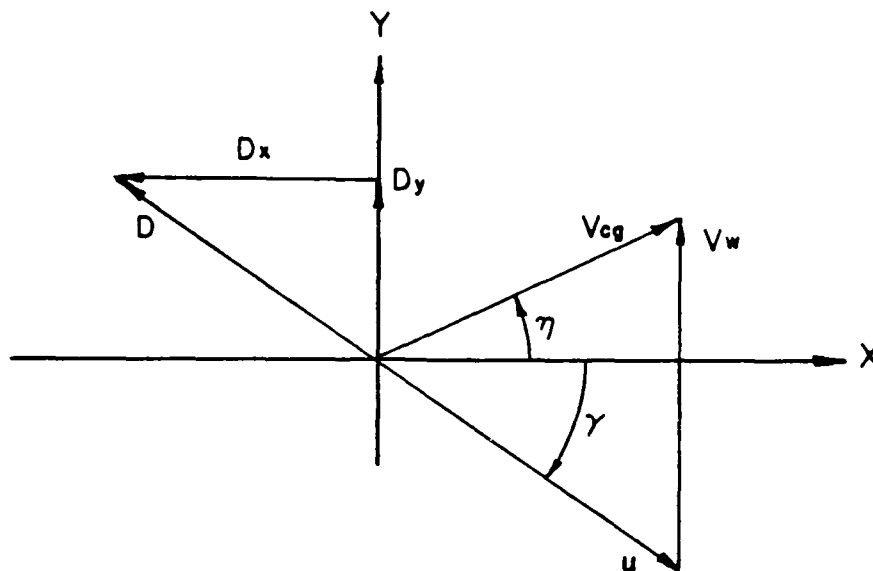
Figure 3-8 Simplified Three Degrees Of Freedom Model

The simplified model was used to analytically evaluate the crossrange dispersion (y) in the cases of sine and cosine winds to confirm the validity of the three-degrees-of-freedom model. Calculations follow:

General equations of motion in the y direction from Figure 3-8 are:

M dVy/dt =Dy which approximately equals D(Vw-Vy)/Vxo

if Vxo=Vo=constant. Then transforming the equation we get:

dVy/dt + D/(MVo)Vy = D/(MVo) Vw(t)

or in time differentiated notation:

$$\ddot{y} + B \dot{y} = B\, Vw(t) \quad \text{if } D/(MVo) = B$$

If a cosine wind $Vw(t) = Vwo \cos (2\ PI\ Vo\ t/\lambda)$ is applied and the differential equation solved we have:

$$y(t)/\lambda = K \left[e^{-Bt} - \cos(2\ PI\ Vo\ t/\lambda) + \frac{D\lambda \sin(2\ PI\ Vo\ t/\lambda)}{2\ PI\ m\ Vo^2} \right]$$

$$\text{let } K = 2\ \frac{\dfrac{1/2\ m\ Vo^2\ Vwo}{D\lambda\ Vo}}{1 + \left[\dfrac{4\ PI\ D\lambda}{1/2\ m\ Vo^2}\right]^2}$$

Figure 3-9 graphically depicts the results as t increases. A zero asymptote is observed and this conforms with model results.

Now if a sine wind $Vw(t) = Vwo \sin (2\ Pi\ Vo\ t/\lambda)$ is applied and the differential equation solved:

$$y(t)/\lambda = K \left[\frac{D\lambda}{4\ PI\ 1/2\ m\ Vo^2}(1 - \cos(2\ PI\ Vo\ t/\lambda)) - \sin(2\ PI\ VO\ t/\lambda) + \frac{4\ PI(1/2\ mVo^2)(1 - e^{-Bt})}{D\lambda} \right]$$

Figure 3-10 graphically depicts these results as t increases. The asymptote is

$$K \left[\frac{(4\ PI\ 1/2\ m\ Vo^2)}{D\lambda}(1 - e^{-Bt}) \right]$$

and this conforms to the model also.
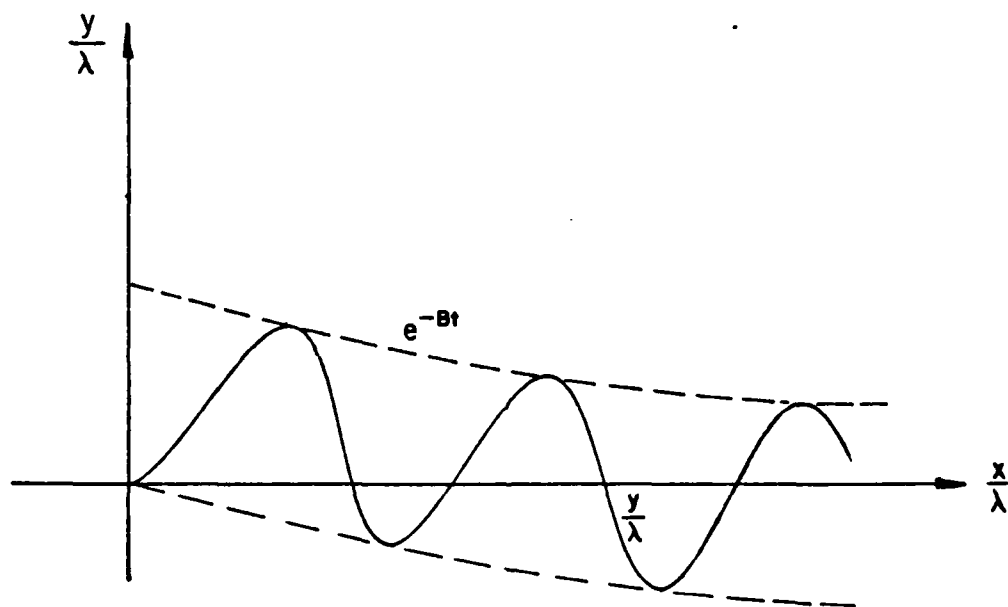
Figure 3-9 Cosine Wind Analysis Results
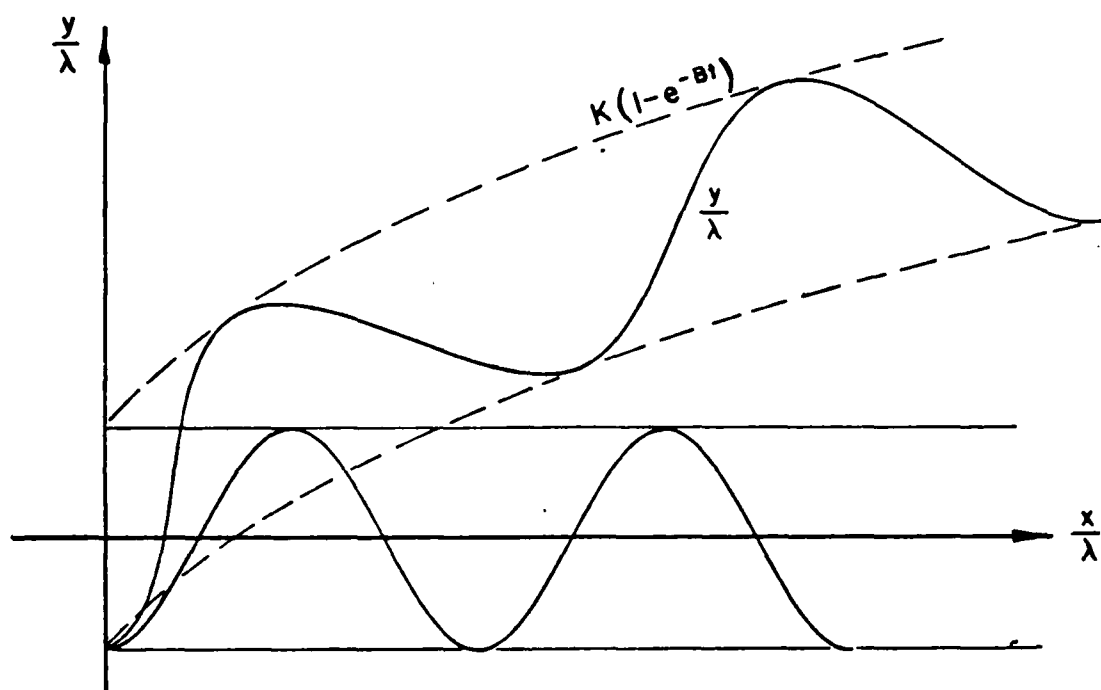
Figure 3-10   Sine Wind Analysis Results

The constant wind case was also derived:

$$V_w(t) = V_w$$ and the solved differential equation is:

$$y(t) = V_w t - V_w m V_o/D \, e^{-Bt}$$

and as t increases y approaches $V_w t$.

Specific calculations were done to confirm dispersion results at burnout. The calculations were based on:

$$y = dy/dx \; X = 1/V_o \; dy/dt \; X$$

$$V_{wo} = 60 \text{ ft/sec}$$

$$V_o = 2190 \text{ ft/sec}$$

$$\lambda = 304000 \text{ ft}$$

$$t = \lambda/V_o$$

$$D = 1/2 \; \rho \; V_o^2 \; A \; C_d \; (=226 \text{ lbf})$$

Thrust $= .9D$ therefore $D = 22.6$ lbf

$$M = 225 \text{ lbm}$$

Taking the time derivative of the cosine wind $y(t)$ dispersion formula derived earlier we get

$$dy/dt = K \left[-Be^{-Bt} + \frac{2 \; PI \; V_o}{\lambda} \sin(2 \; PI \; V_o \; t/\lambda) + \frac{D\lambda}{4 \; PI \; 1/2 \; mV_o^2} \cdot \frac{2 \; PI \; V_o}{\lambda} \cos(2 \; PI \; V_o \; t/\lambda) \right]$$

at t = λ/Vo the equation becomes:

$$dy/dt = K(-Be^{-B\lambda/Vo} + B)$$

and substituting the values into the approximationn
for y; y=0 ft.

Now, performing the same operations on the sine
wind dispersion equation :

$$dy/dt = K\left[\frac{D\lambda}{4\ PI\ 1/2\ mVo^2} \cdot \frac{2\ PI\ Vo}{\lambda}\sin(2\ PI\ Vo\ t/\lambda) \right.$$
$$\left. \frac{-2\ PI\ Vo}{\lambda}\cos(\frac{2\ PI\ Vo\ t}{\lambda}) + (\frac{4\ PI\ 1/2\ m\ Vo^2}{D\lambda}). \right.$$
$$\left. (Be^{-Bt}) \right]$$

and at t=λ/Vo

$$dy/dt = K\left[\frac{-2\ PI\ Vo}{\lambda} \frac{-4\ PI\ 1/2\ m\ Vo^2}{D\lambda}.Be^{-Bt} \right]$$

and y=20 ft approximately.

Finally, taking the constant wind dispersion
formula and taking its derivative :

$$dy/dt = Vw - Vw\ e^{-Bt}$$

and y= 10 ft approximately.

These results are consistent with the three-degrees-of-
freedom model considering the initial approximations.

To study the short period resonance phenomenom the
phase and wavelength wind variations were documented in

44

detail for a condition of thrust equal to 90% drag.Figures
3-11 to 3-13 show the crossrange dispersion effects from
wavelengths of 5000 (lambda = .016 range) to
303000(lambda=range) feet and the phase angle variations
from 0 to 2 PI.At approximately 9850 feet the dispersion
characteristics were no longer symmetric but remained under
one foot.This is demonstrated at Figure 3-14.A crossrange
dispersion contour was constructed at Figure 3-15 but this
did not emphasize the resonance phenomenon sufficiently due
to linearized aerodynamics and small dispersion
magnitudes.The parameters that varied most significantly
near resonance were angle of attack and burn time.Indeed,it
is clear that the projectile is unstable in this region with
a maximum angle of attack of 1.21 radians(70 degrees).Due to
the increased angle of attack, drag increased and burn time
decreased in the order of seven seconds (5%) compared to the
baseline trajectory. This clearly affected the range at
burnout.Due to large angle of attack the linearized
aerodynamics are not valid.Projectile performance at wind
resonance is worthy of additional analysis.It was decided to
demonstrate resonance by plotting the maximum angle of
attack (alpha) versus wavelength with different thrust/ drag
scenarios.The resonance results are at Figure 3-16.The
projectile natural frequency is estimated at 0.22 Hz.
Resonance was confirmed in the 0.22 Hz regime for thrust

errors under 10% including varying Vwo.This was necessary as the system is non-linear and Vwo could have affected resonance.It was noted that the curve shifted and increased or decreased in magnitude slightly in each case.This is due to the non-linearity of the system equations and the variations in Vo during flight.The absolute case of no thrust showed resonance at 10000 feet with a maximum angle of attack of 1.25 radians(72 degrees).
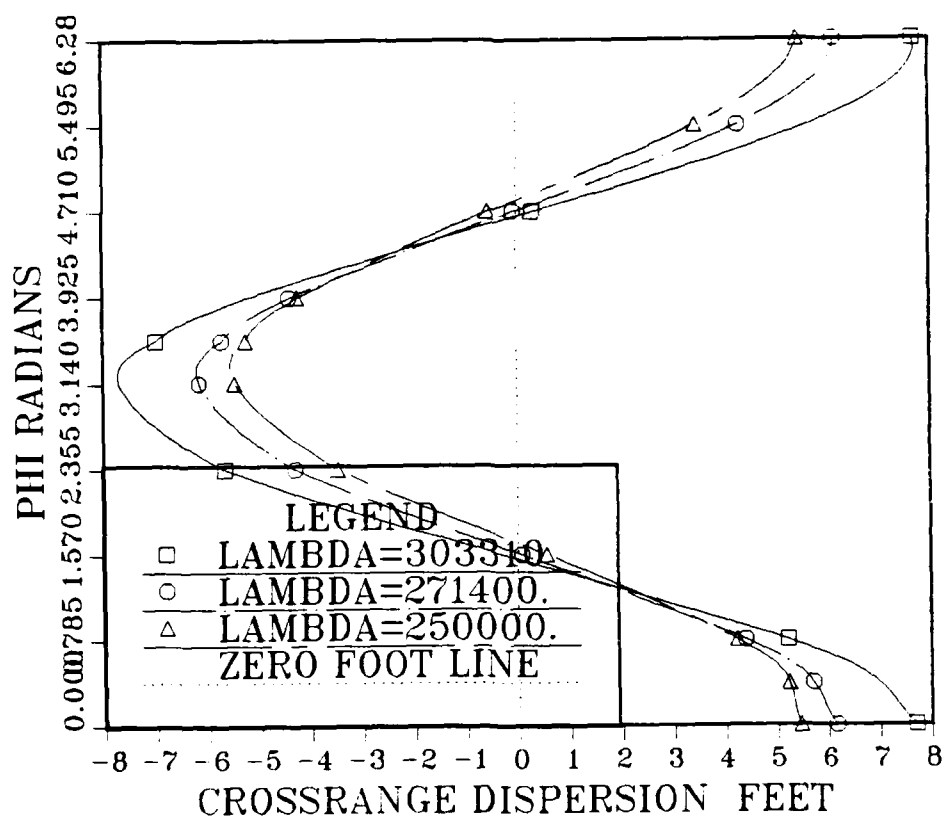
Figure 3-11 Dispersion Versus Wind Phase Angle(Large Lambda)
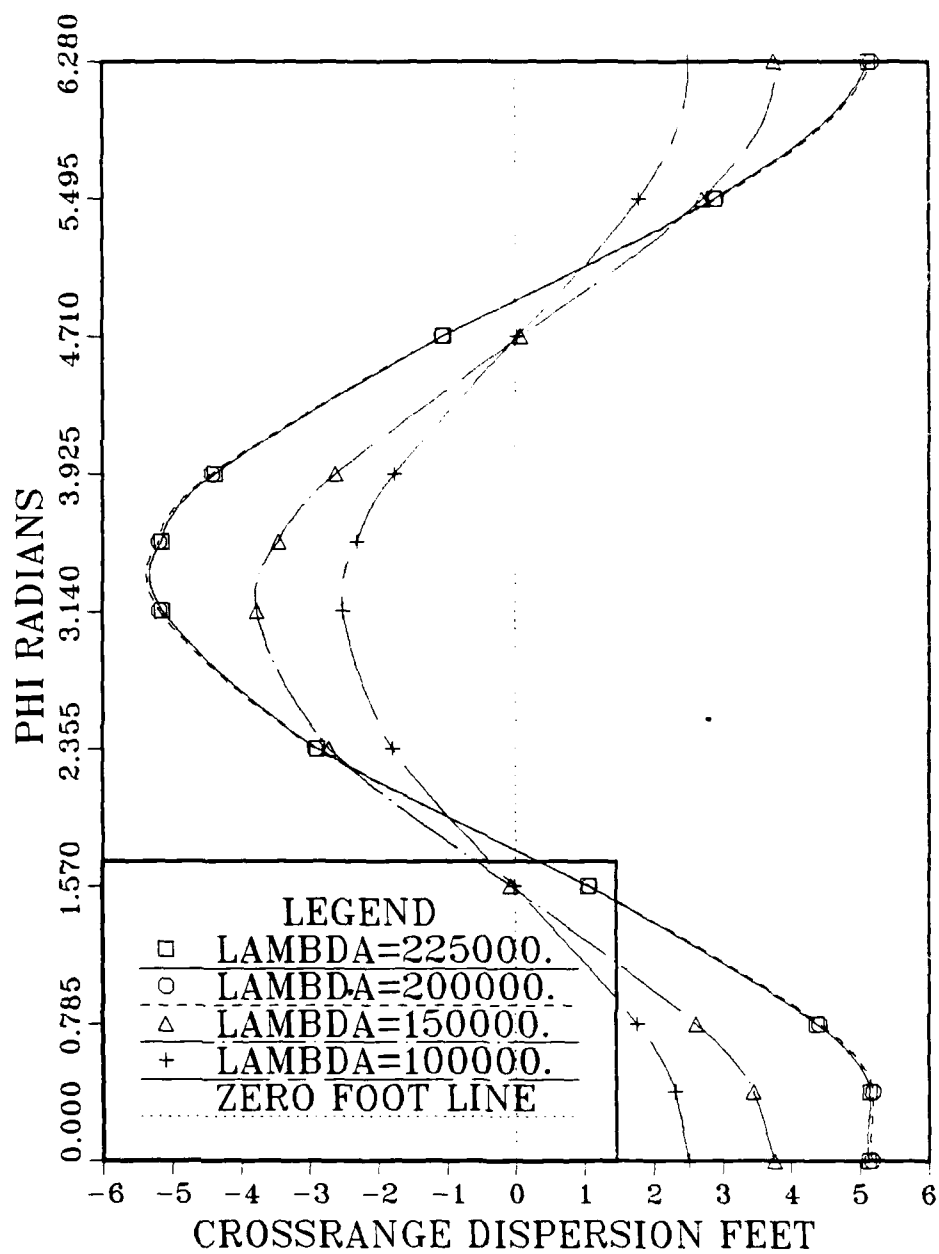
Figure 3-12 Dispersion Versus Phase Angle
(Medium Lambda)

47
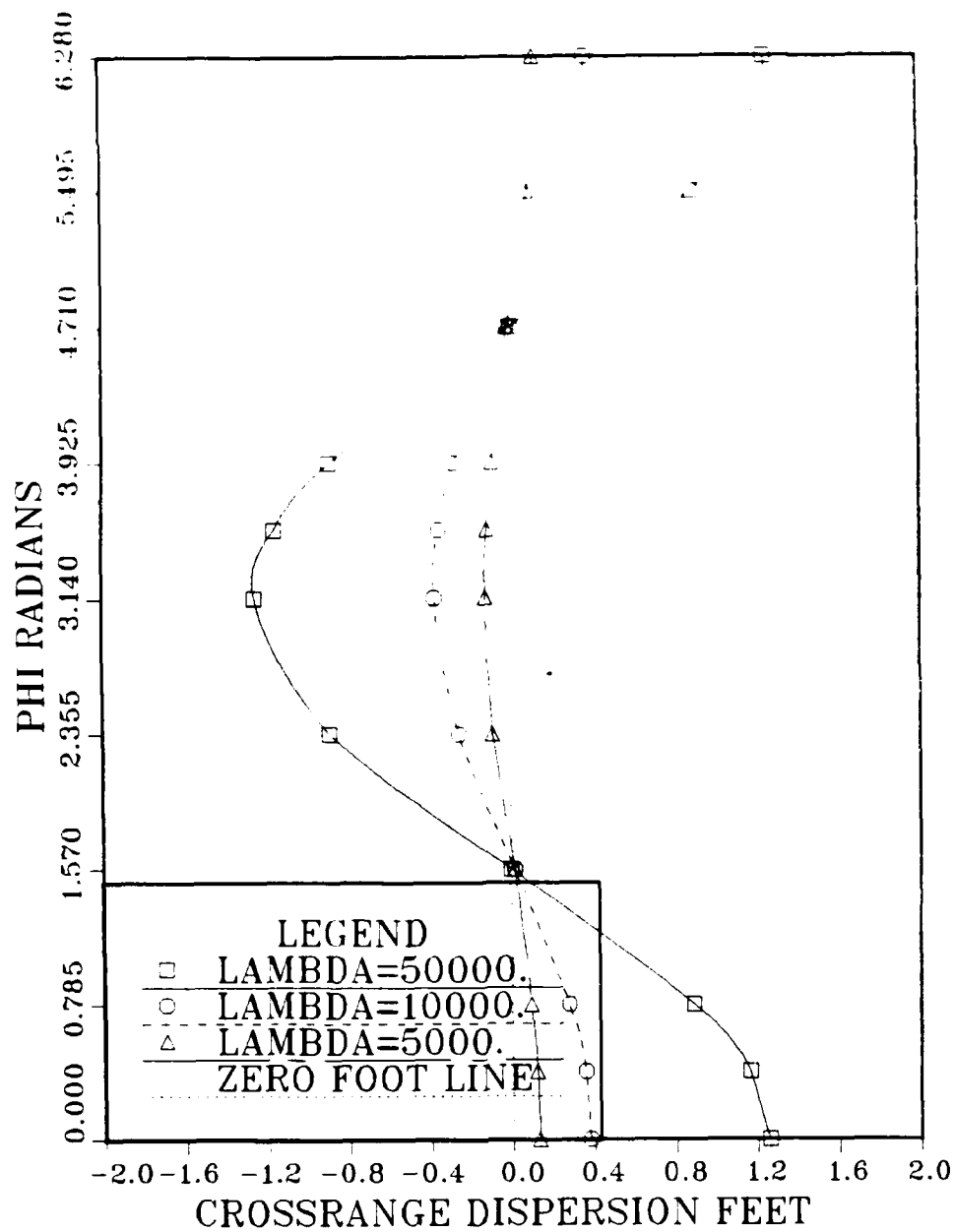
Figure 3-13 Dispersion Versus Phase Angle(Small Lambda)

48
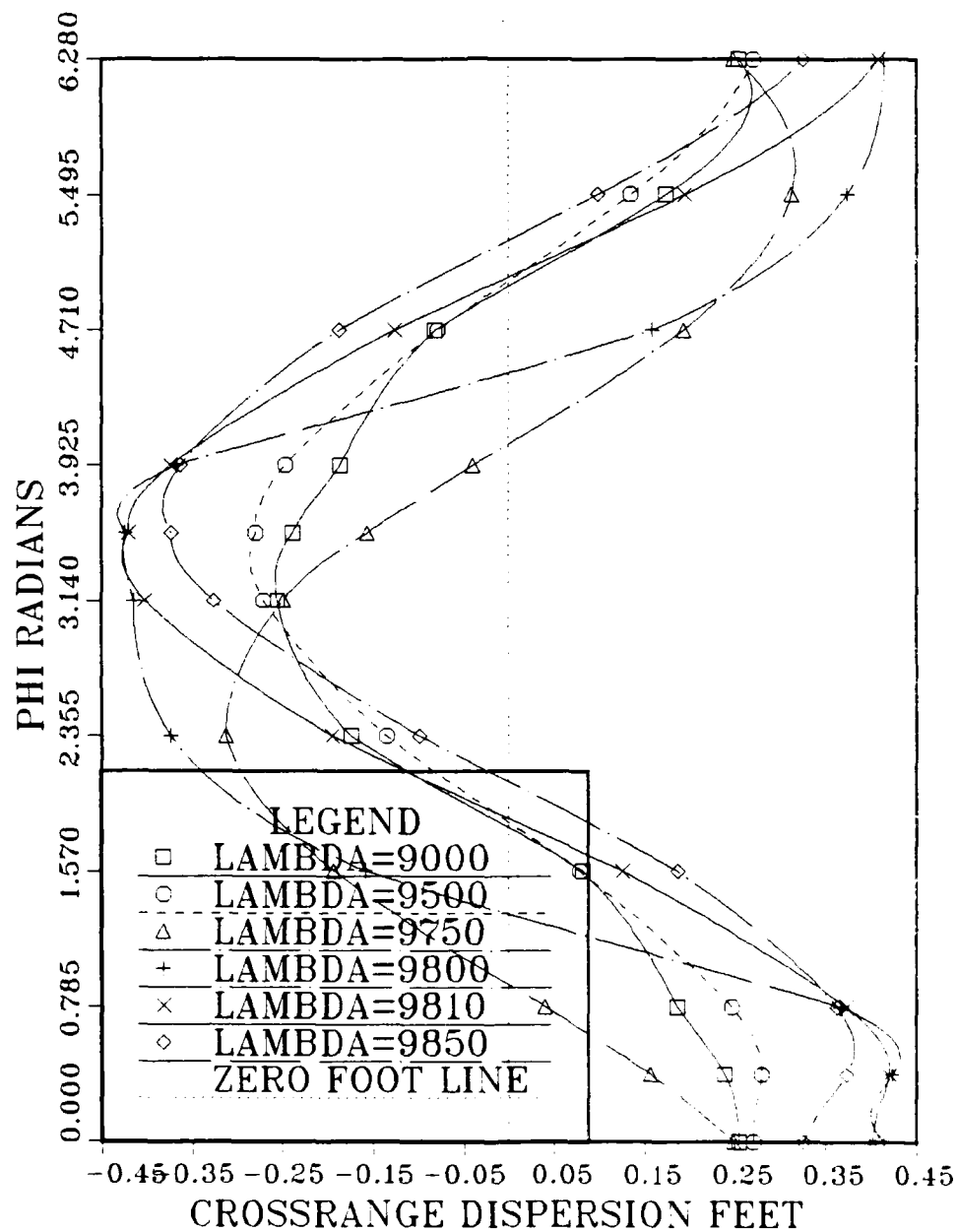
Figure 3-14 Dispersion Versus Phase Angle
Resonance Lambda
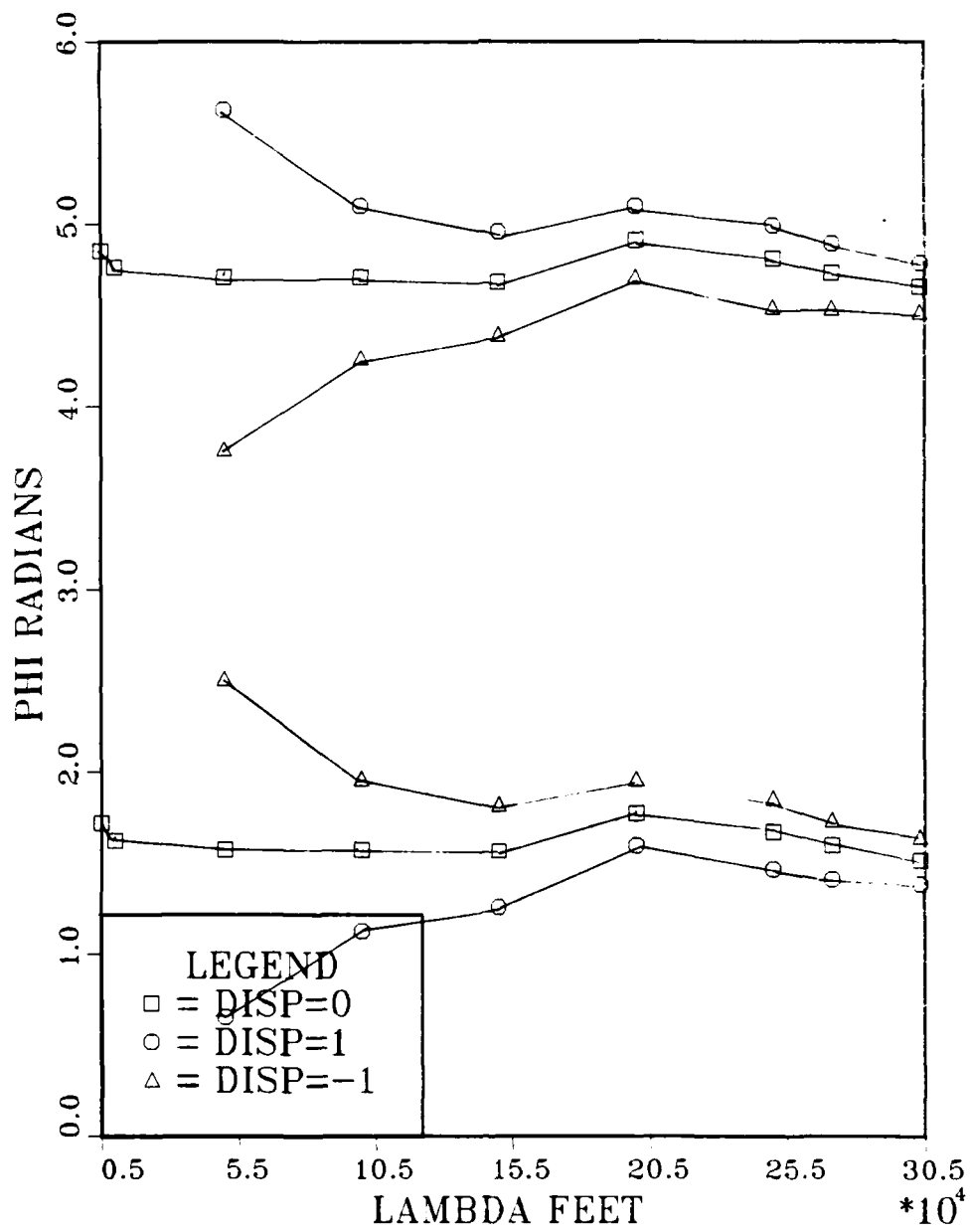
Figure 3-15 Phase Angle Versus Wavelength
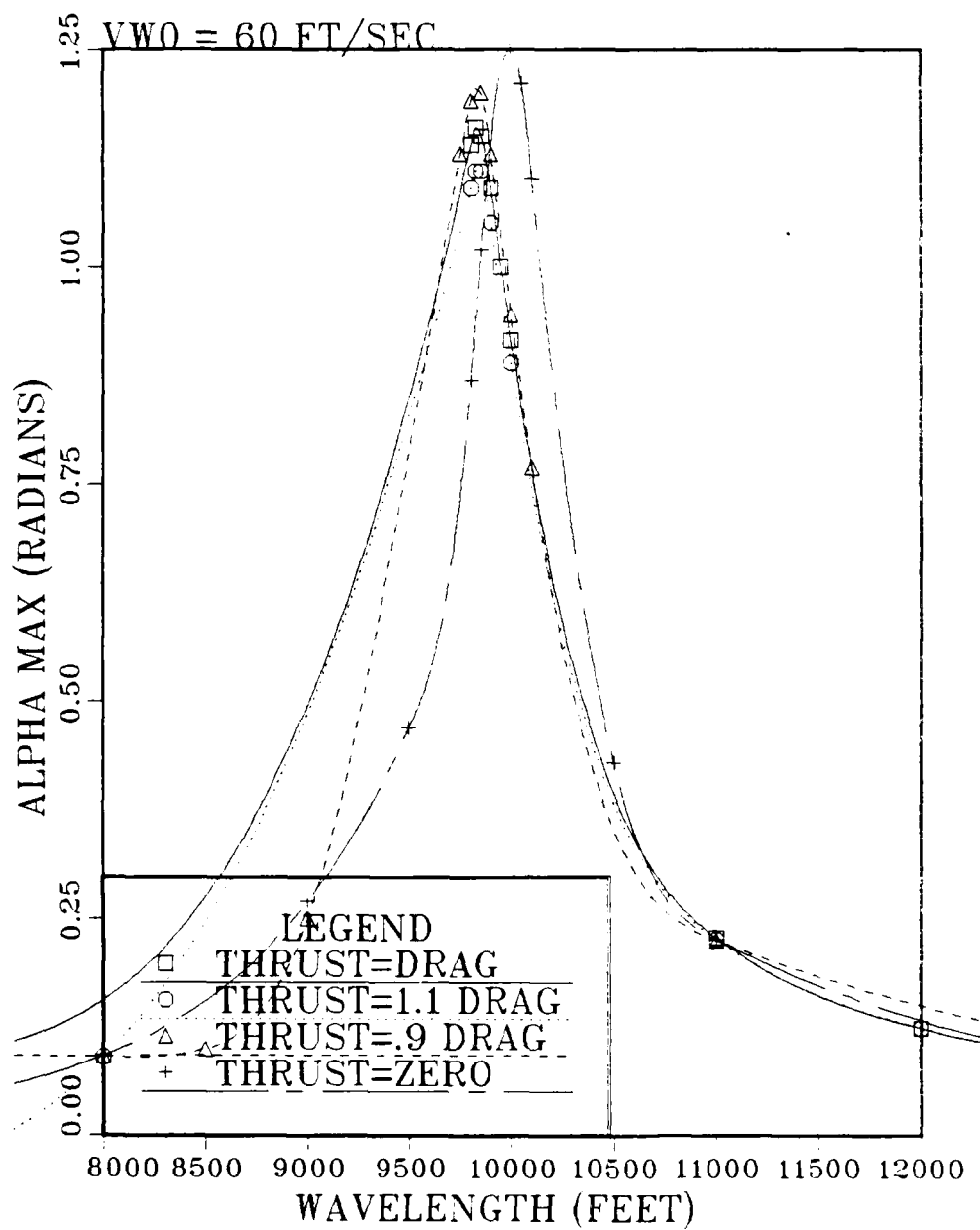
Figure 3-16 Detrimental Resonance Between Projectile
Short Period and Spatial Frequency of
Wind Profile

It is clear that if the wind profile experienced by the projectile has harmonic content near the natural frequency then the round will be unstable and/or have large dispersion at burnout. This is best illustrated by viewing the wind as Vw(t) with reference to the projectile. By a Fourier transform of the wind profile resonance with projectile natural frequency (fn) will be evident in the frequency domain.The wind oscillations need only be velocity variations with the appropriate harmonic content.Figure 3-17, which illustrates this concept, shows fn coinciding with a maximum of Vw(f). One would anticipate stability problems for this case.

FOURIER TRANSFORM (sample)
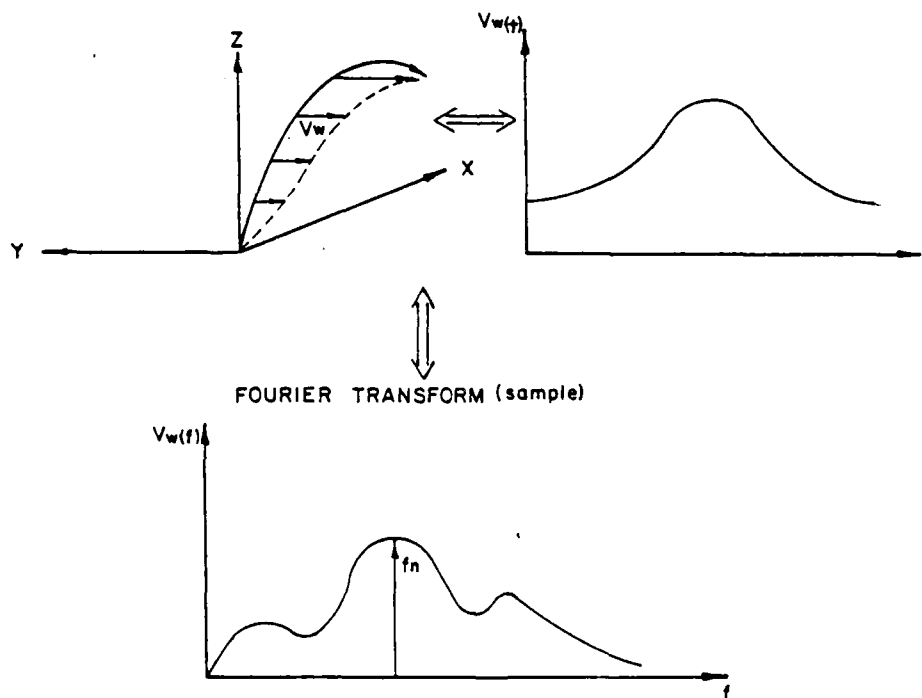
Figure 3-17 Fourier Transform Of Wind Profile Concept

Calculations for the long period resonance or phugoid show that the phugoid is irrelevant as flight time is too short:

T=4.44*Vo/g=301.8 seconds [Reference 3]

The results of the sinusoidal winds were also compared with the aerodynamic jump phenomenom outlined in BRL report 1077 [Reference 4]. At first glance the sinusoidal wind results appear consistent with aerojump,but detailed calculations show otherwise. The rate of change of initial angle of attack is critical to aerojump and is easily incorporated into the aerojump equation.The results for the sine wind are a function of wavelength and of the same form as the simplified model results but the cosine wind and constant wind both yielded a small aerojump proportional to the initial wind.The magnitudes of the aerojump dispersions were more consistent with the net lift transient effects. Further, continuous perturbations in the form of wind after time zero are not in the aerojump equations and for all practical purposes the phenomenom is not observed in the model.These results should have been apparent before calculations were performed. Aerojump equations are not appropriate for non-zero wind conditions.Clearly, when wind is included the aerojump equations cannot predict dispersion.

B. FIVE DEGREES OF FREEDOM

As previously stated dispersion was measured from the ideal pseudo-vacuum trajectory at a fixed time for initiation of terminal guidance (Tc) 101 seconds.Thrust error sensitivity in the zero wind condition is presented in Figures 3-18 and 3-19.In these two figures it is clear that thrust errors can have a significant impact on the location of the projectile at the Tc.Figure 3-18 indicates that as thrust increases the dispersion moves downrange as expected.Figure 3-19 shows that as thrust increases the height of the projectile at Tc decreases. Due to added thrust the projectile is located at a point further along the parabolic trajectory; hence the height is less.

As well Figure 3-20 shows these effects on available burn time of the ramjet.For thrust equals drag burnout at 101 seconds exactly equals the Tc.With less thrust, terminal guidance is initiated before all the propellant is burned. Conversely, when thrust exceeds drag, burnout occurs prior to initiation of terminal guidance.Assuming this fixed time for initiation of terminal guidance, the projectile may experience up to seven seconds of unpowered flight (7% error) before the guidance is deployed. The period of unpowered flight with associated high drag will cause major dispersions as shown in subsequent figures.
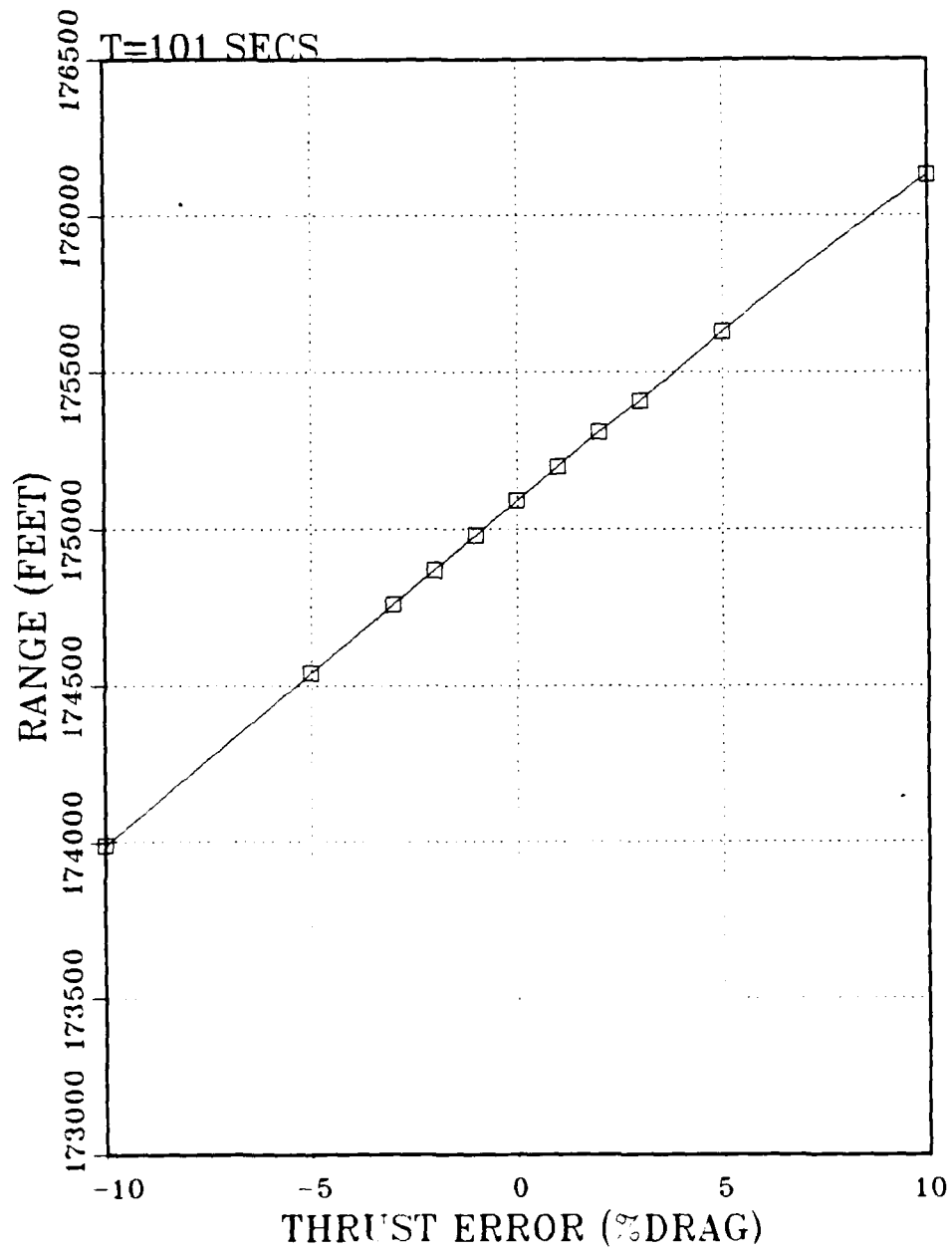
Figure 3-18 Thrust Error Effects (Range)

55
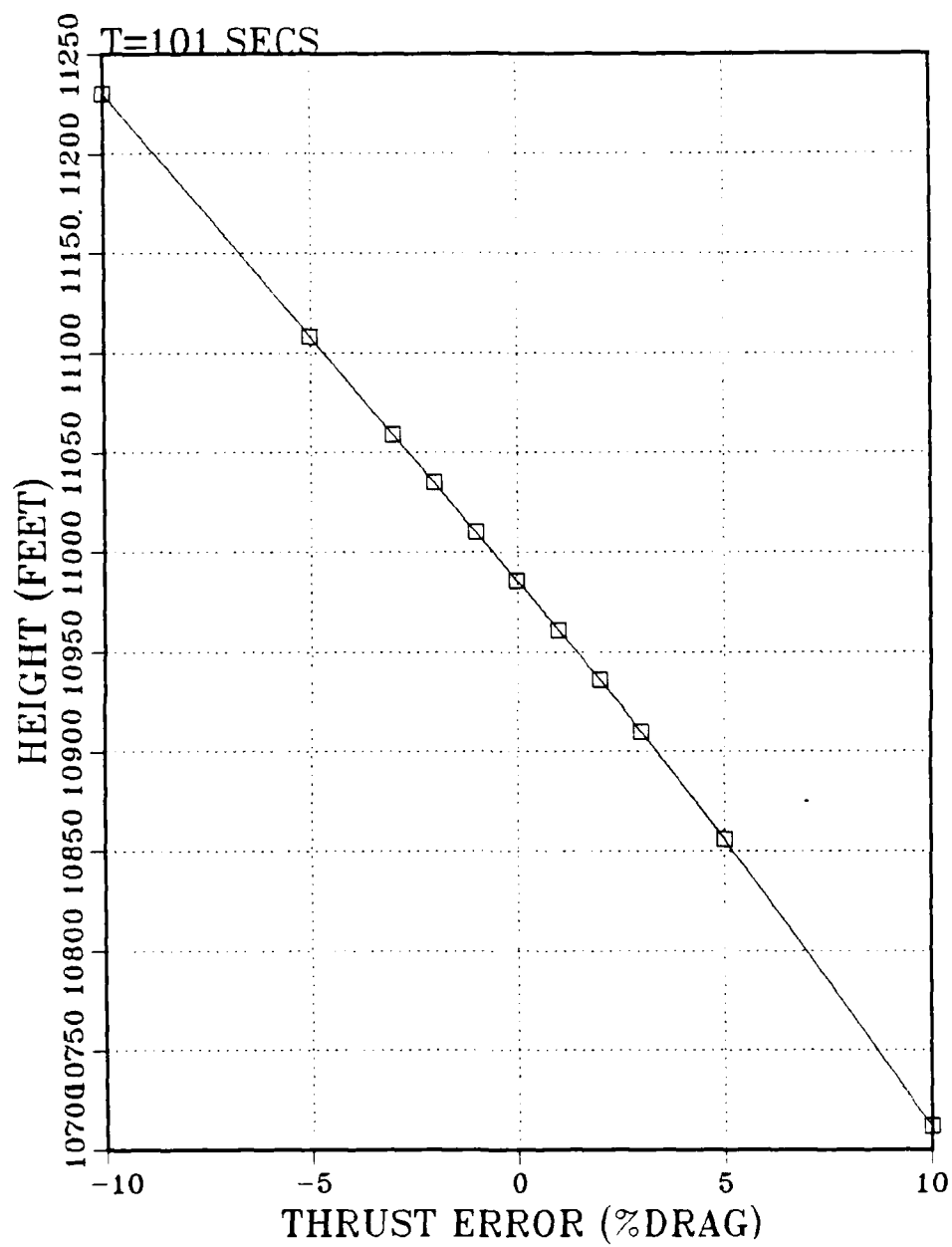
Figure 3-19 Thrust Error Effects (Height)

56
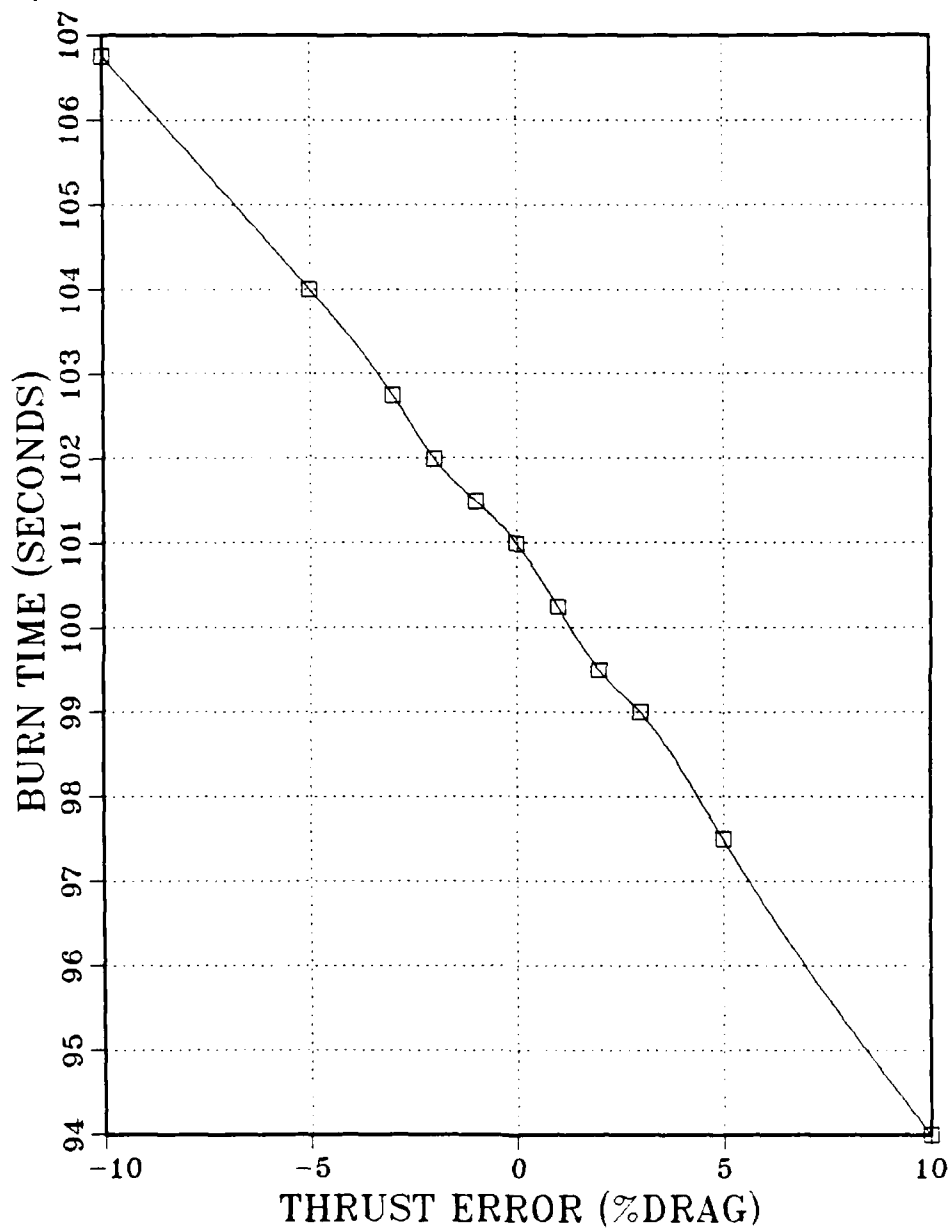
Figure 3-20 Thrust Error Effects (Burn Time)

Crosswind sensitivity results were very much the same as the three degree simulation. In fact the results appear even more linear with the same rotation about the zero zero point as in Figure 3-21. The gross features of Figure 3-3 and 3-21 are identical but Figure 3-3 shows dispersion at burnout whereas Figure 3-21 shows dispersion at Tc.

The crossrange dispersion results of a no thrust projectile with constant crosswind profiles and with thrust equal to drag (transients effects) are at Tables 3.3 and 3.4 respectively.

Table 3.3 No Thrust Wind Effects
Five Degrees

Thrust =0	time=101 seconds
Vwxy(feet/sec)	dispersion (feet) crossrange
0	0
30	92.51
60	185.11
90	272.90
120	370.97
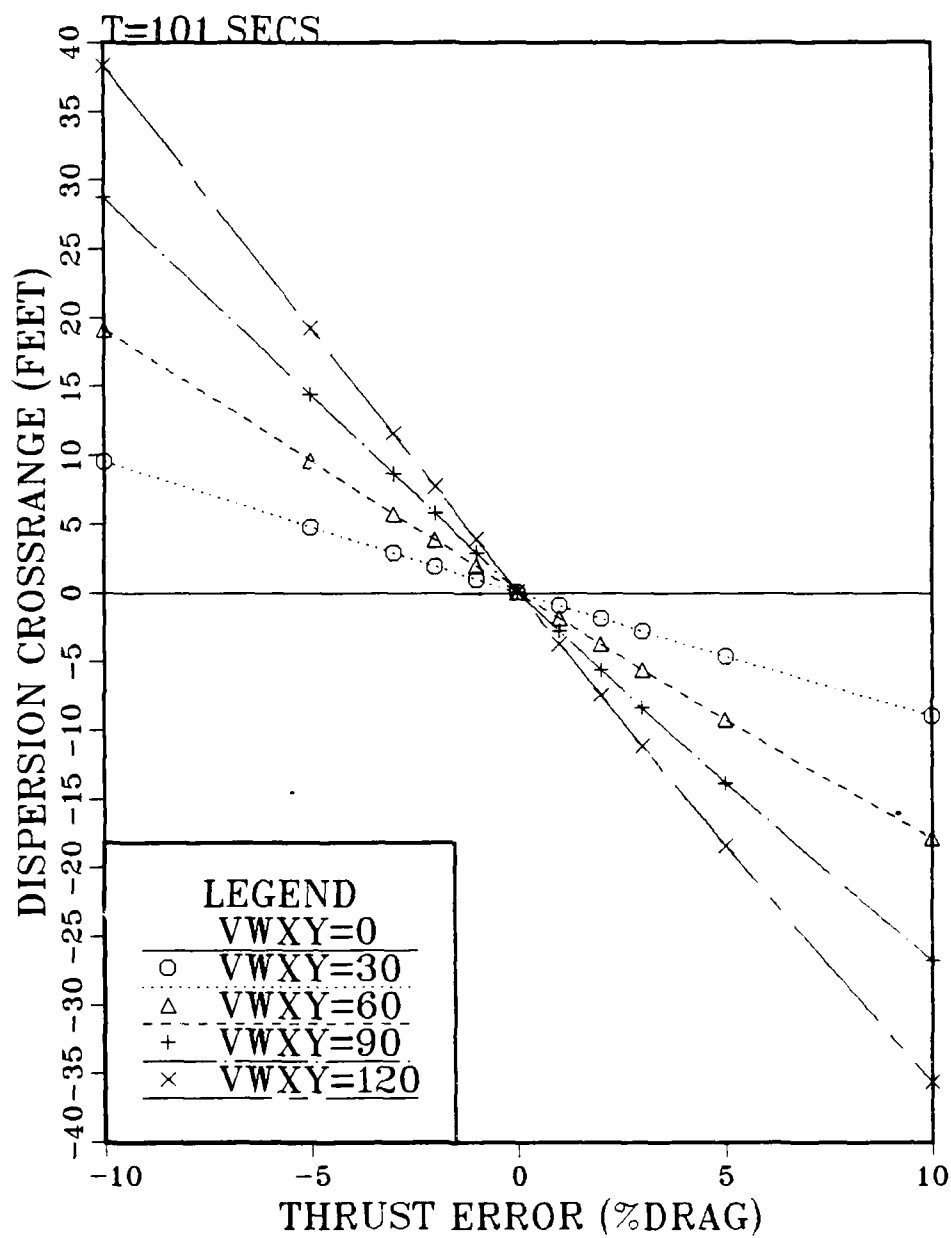
Figure 3-21 Crosswind Effects Five Degrees

Table 3.4 Dispersion Due to Net Lift
from Transients

Thrust=drag time=101 secs

Vwxy(feet/sec)	dispersion(feet)
0	0
30	.0202
60	.0413
90	.0643
120	.0919

Burn time was not significantly affected by crosswinds.

Headwind and tailwind effects on range,height and burntime in different thrust scenarios are shown in Figures 3-22 to 3-26. It is clear that dispersion from the pseudo-vacuum trajectory is minimized when thrust nearly equals drag. It is also apparent that the overthrusted trajectories involve greater dispersion as burnout occurs prior to terminal guidance and unpowered flight occurs for some time dependent on the scenario.This same error is observed in the case of headwinds and is most clear in the Figures 3-22B to 3-25B about the thrust equal to drag axis. (Note that Figure 3-22 to 3-25 inclusive have A,B and C sub-figures which are simply enlargements of key portions of the respective main figure).
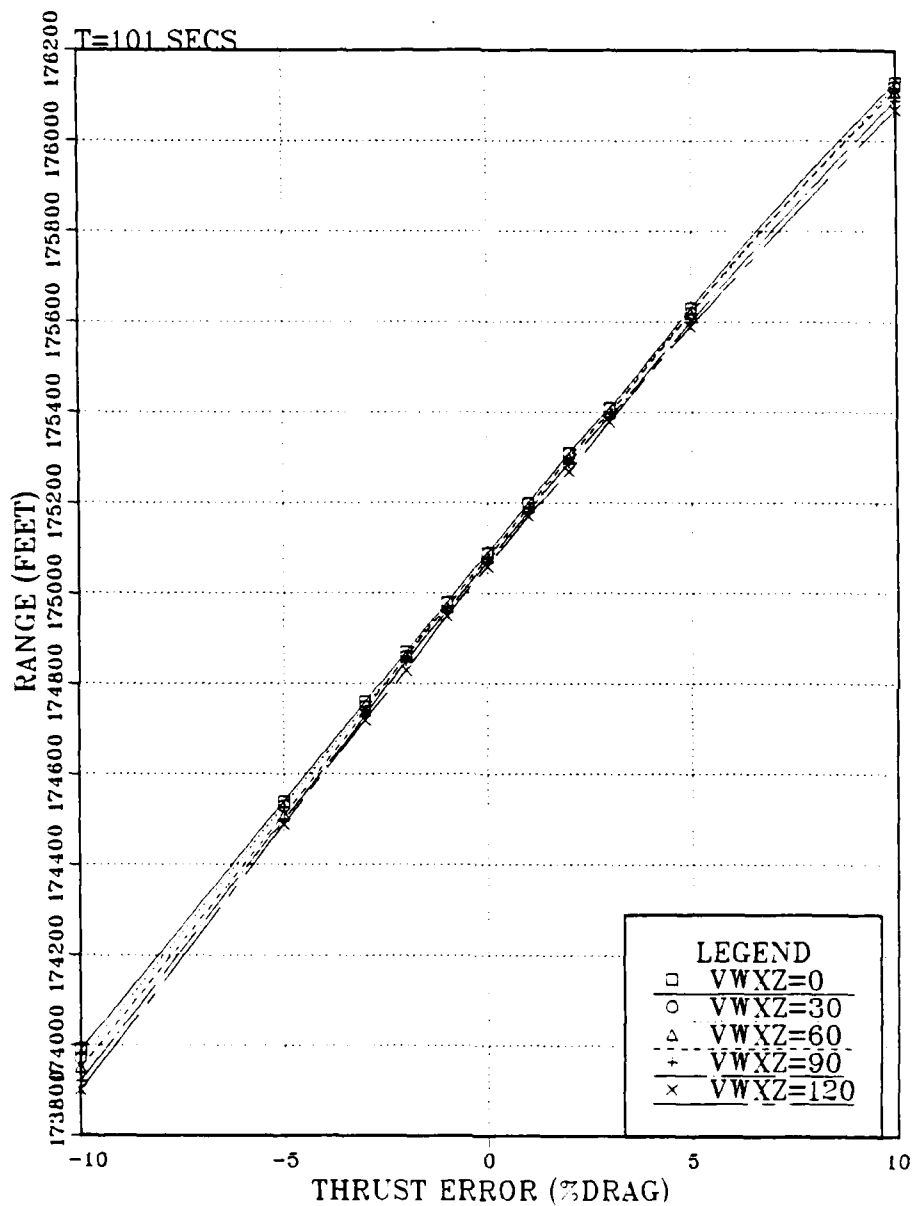
Figure 3-22   Headwind Sensitivity (Range)

61
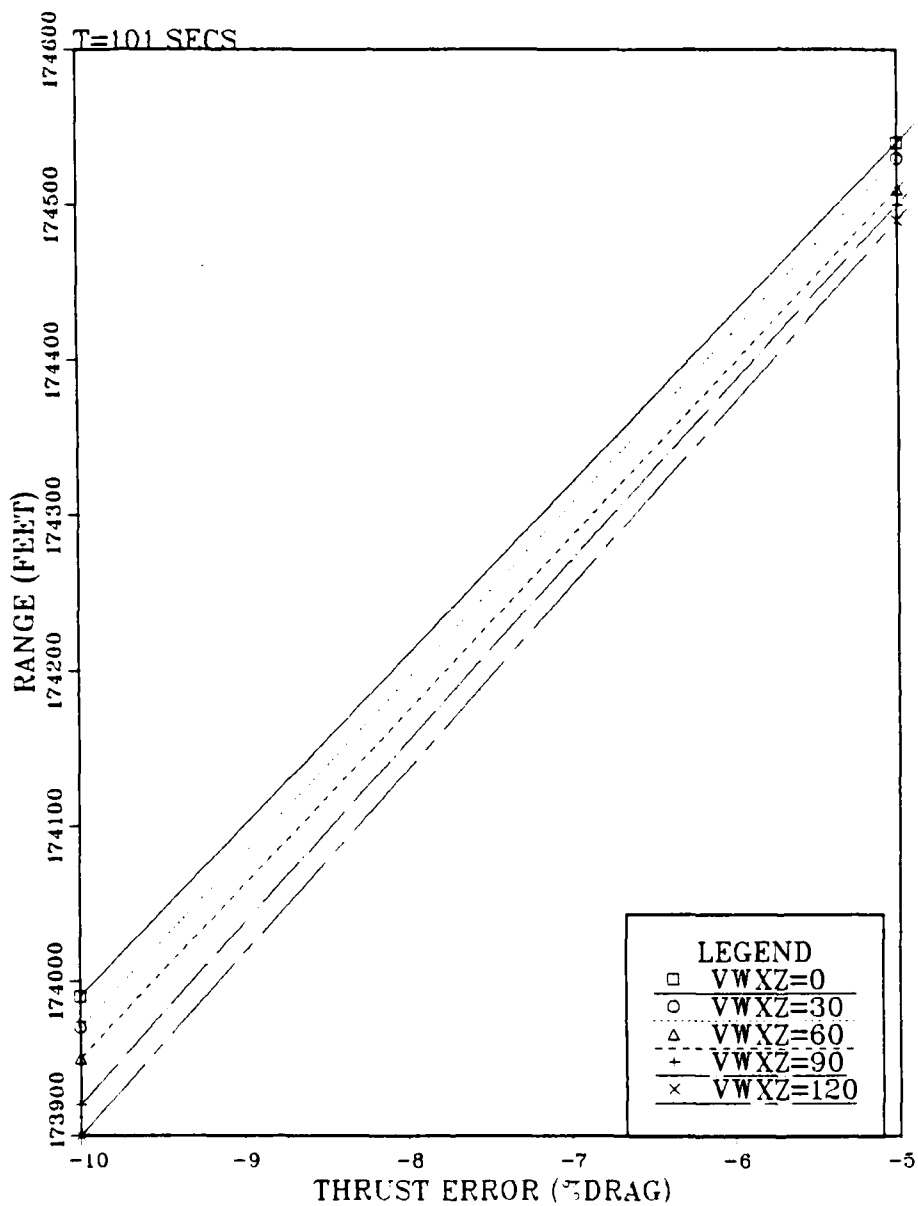
Figure 3-22A Headwind Sensitivity (Range)
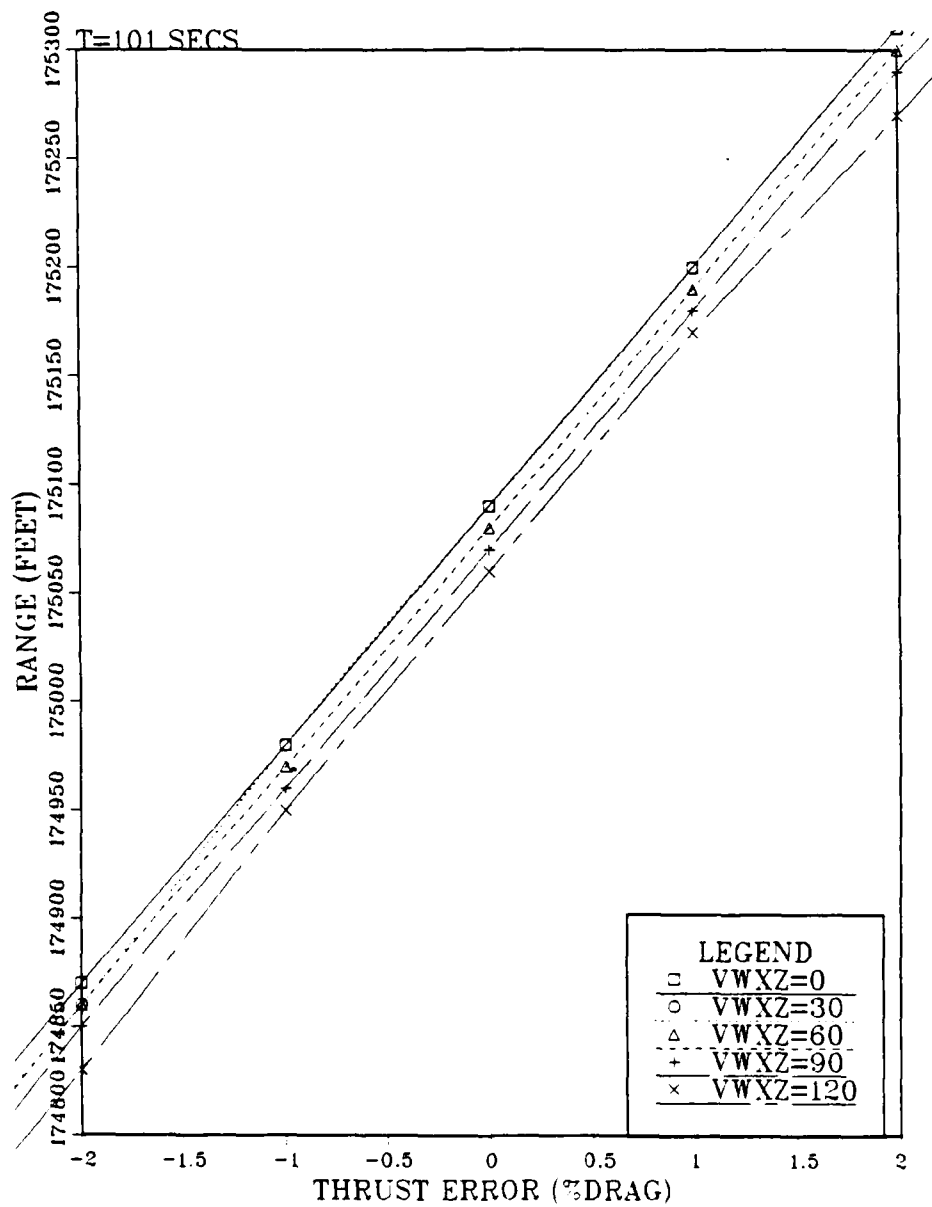
Figure 3-22B Headwind Sensitivity (Range)

63
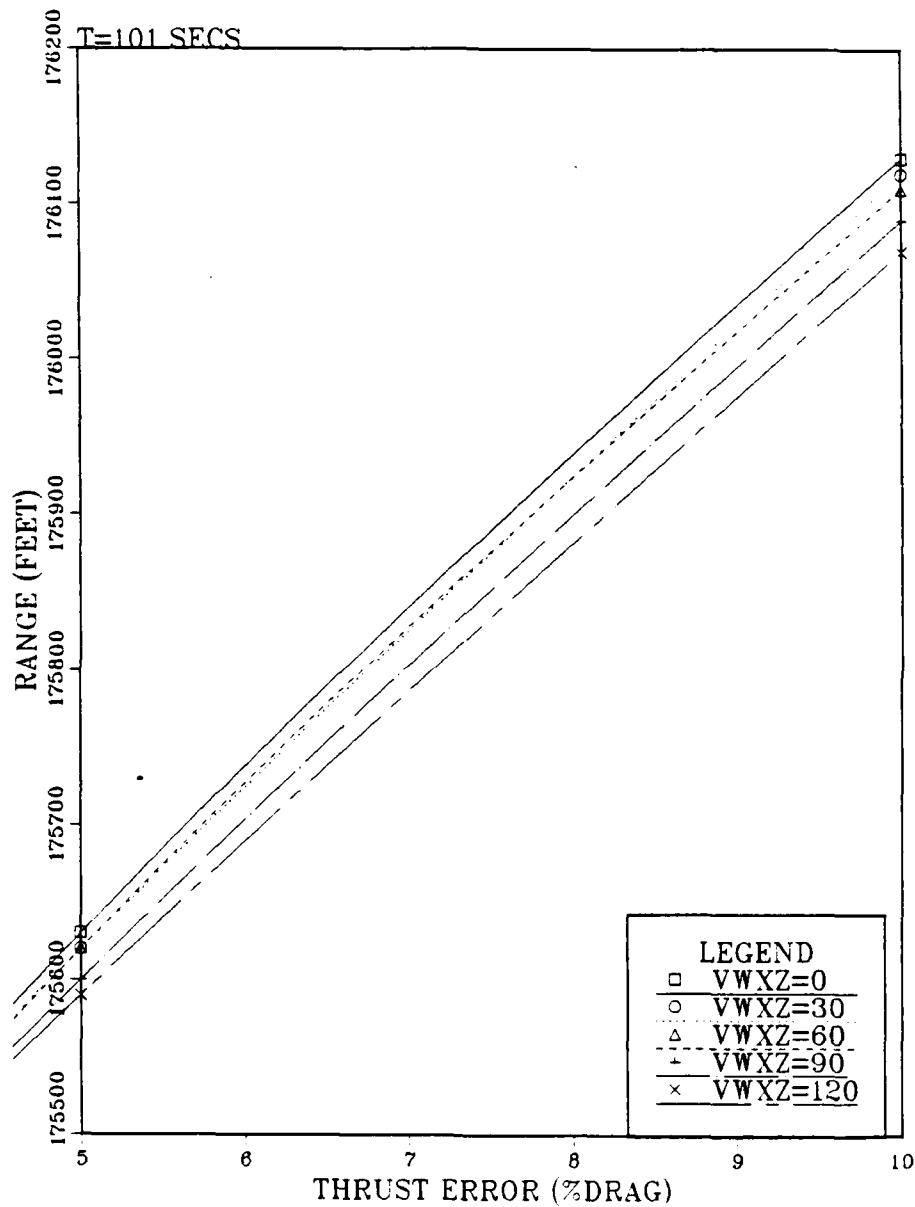
Figure 3-22C Headwind Sensitivity (Range)

64
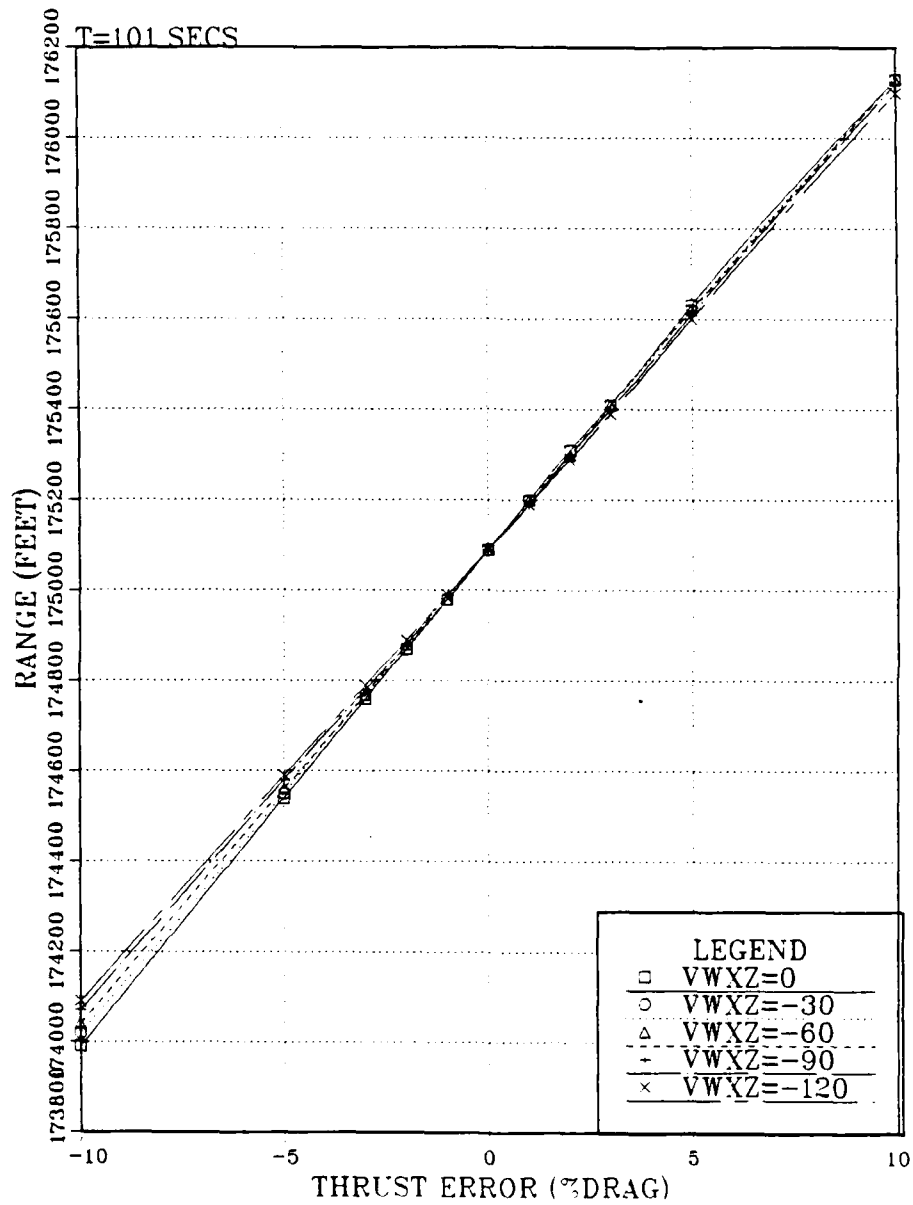
Figure 3-23 Tailwind Sensitivity (Range)
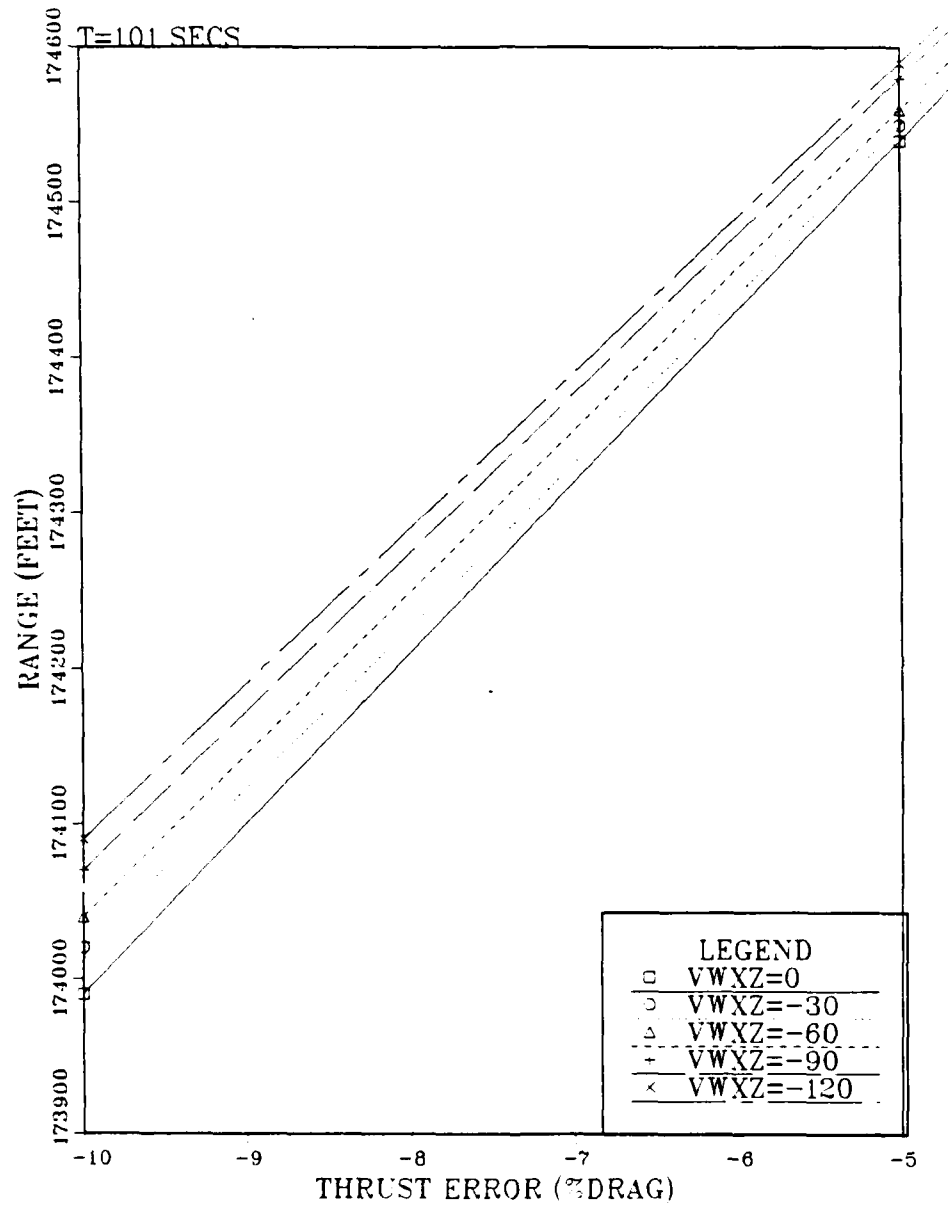
Figure 3-23A Tailwind Sensitivity (Range)
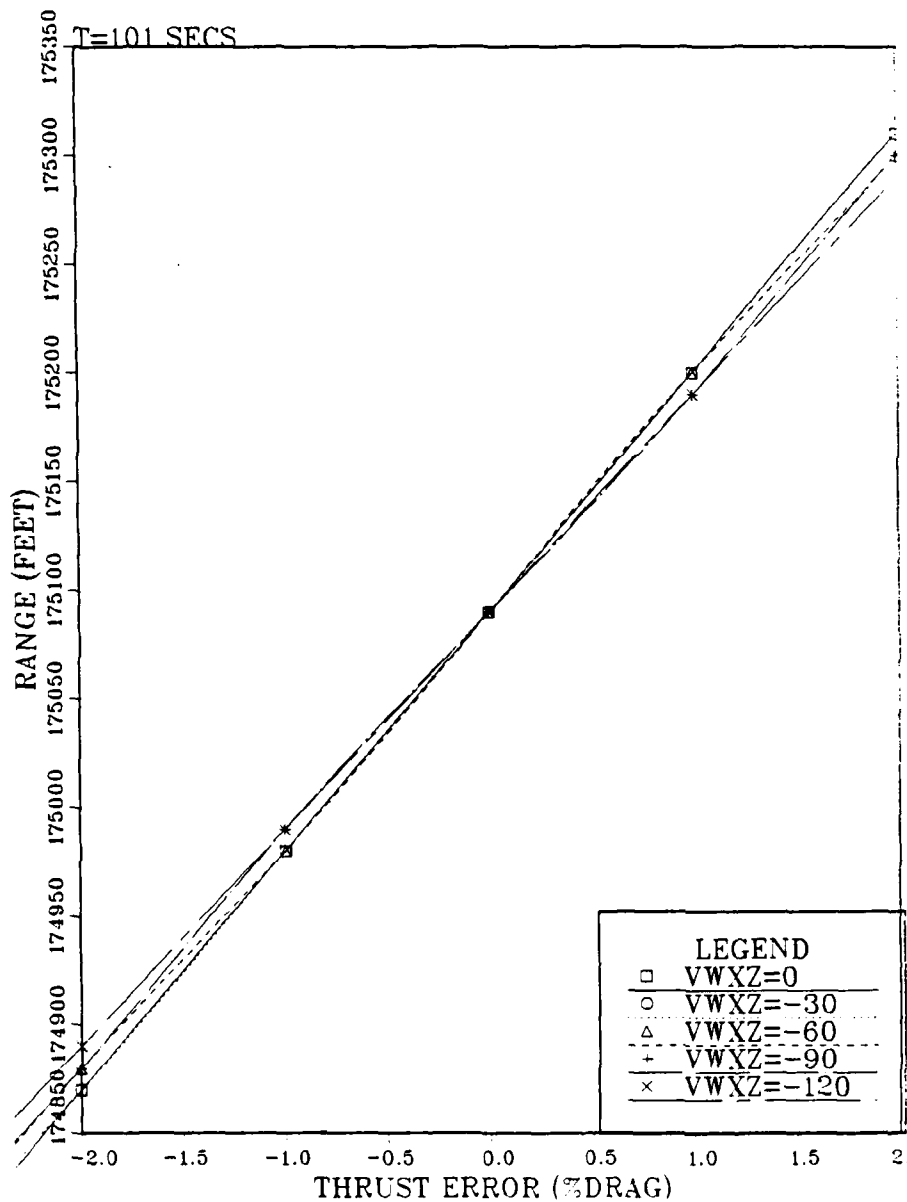
Figure 3-23B Tailwind Sensitivity (Range)

67
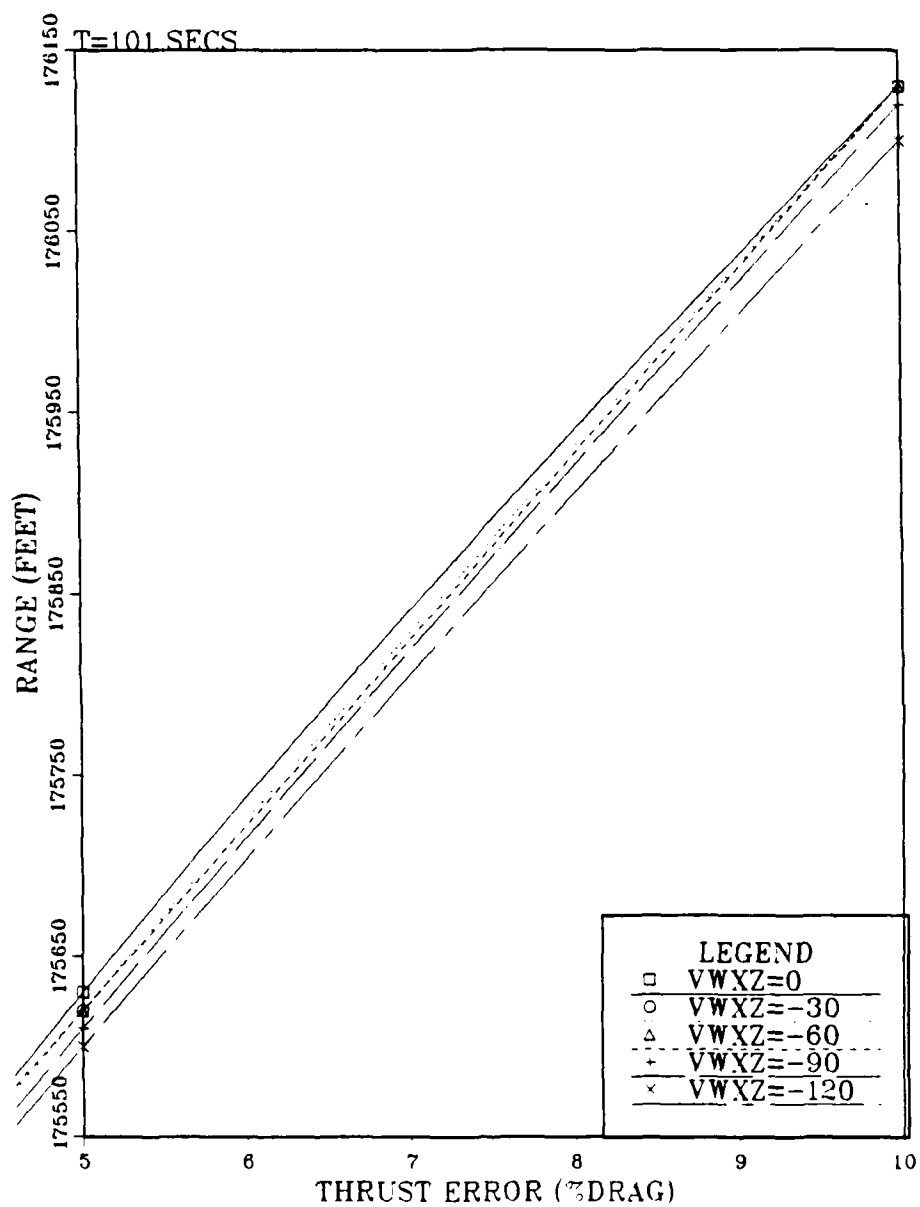
Figure 3-23C Tailwind Sensitivity (Range)

68
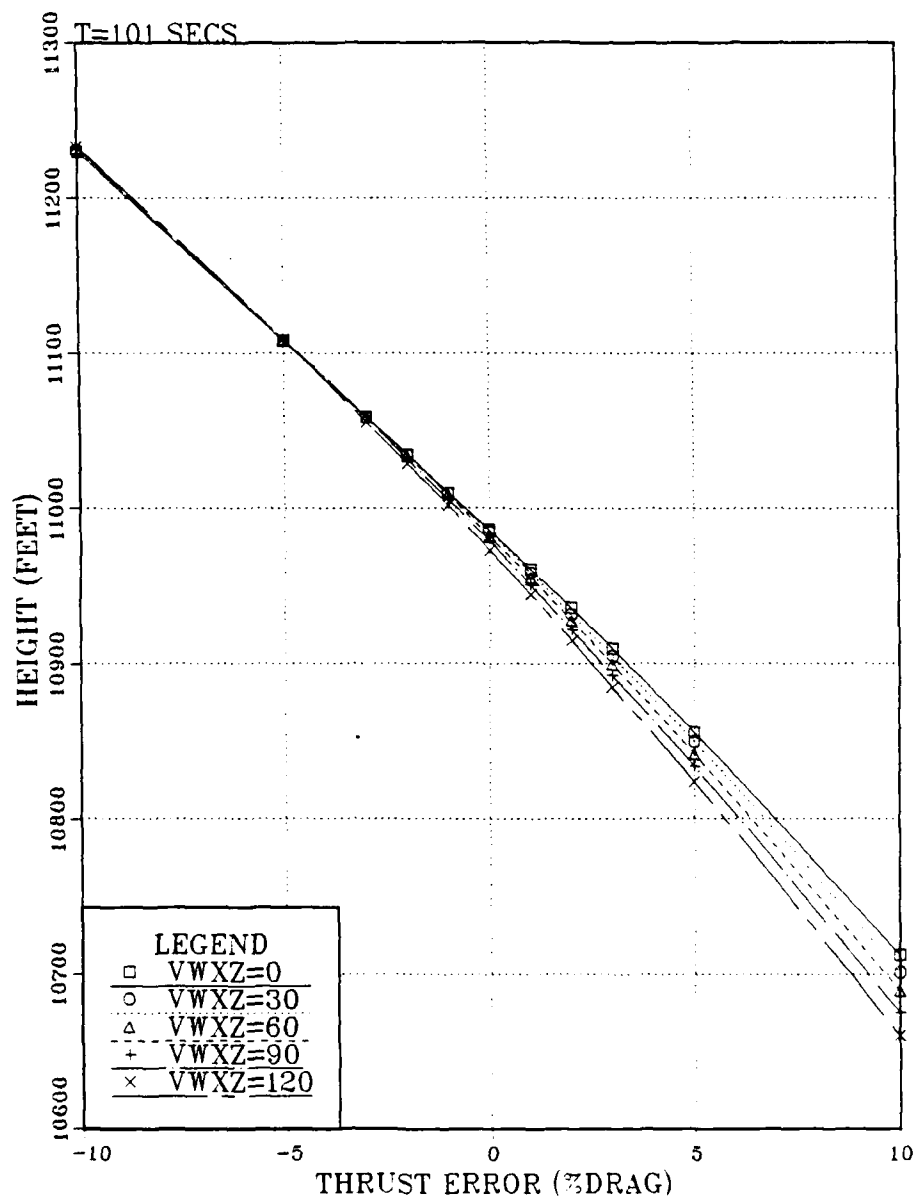
Figure 3-24 Headwind Sensitivity (Height)

69
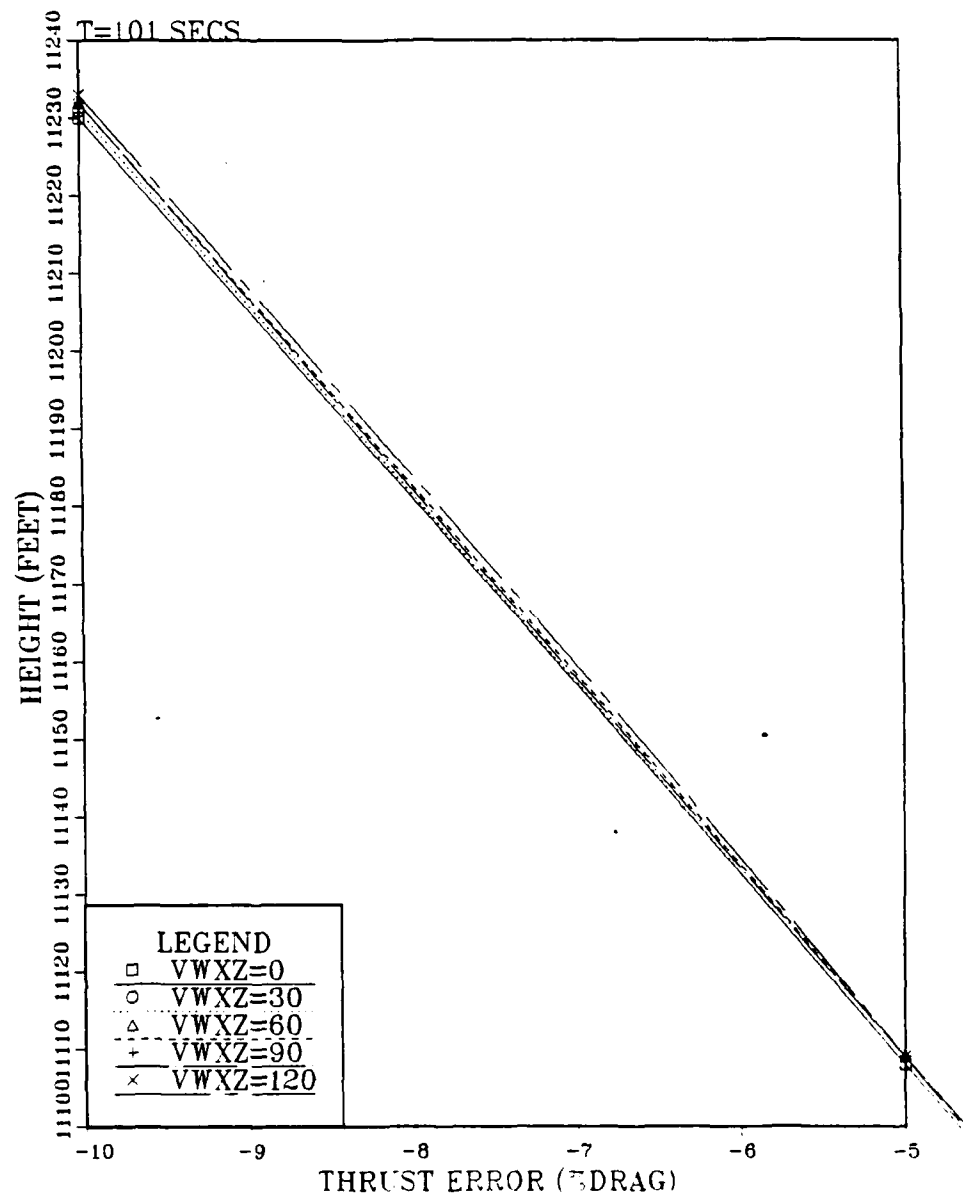
Figure 3-24A Headwind Sensitivity (Height)

70
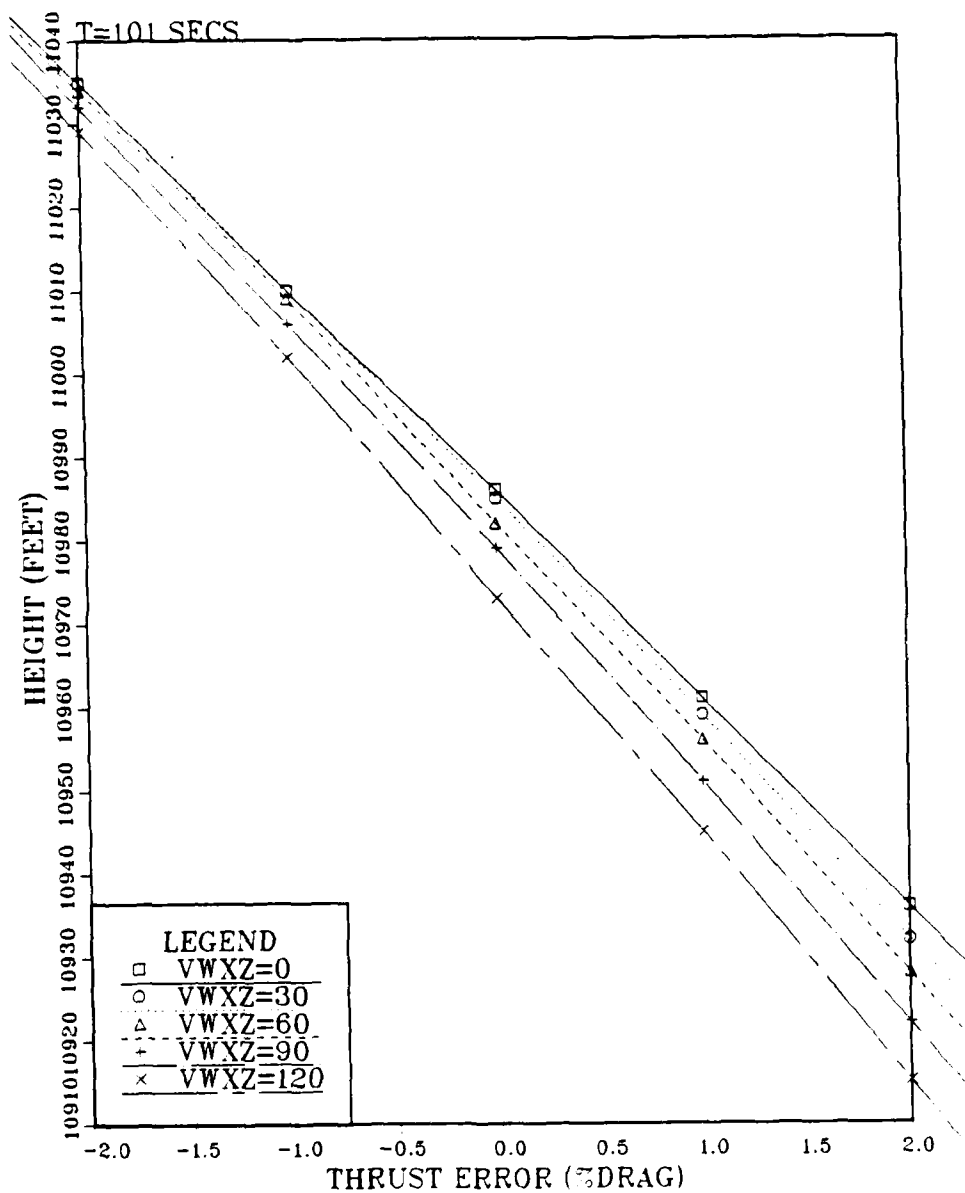
Figure 3-24B Headwind Sensitivity (Height)

71
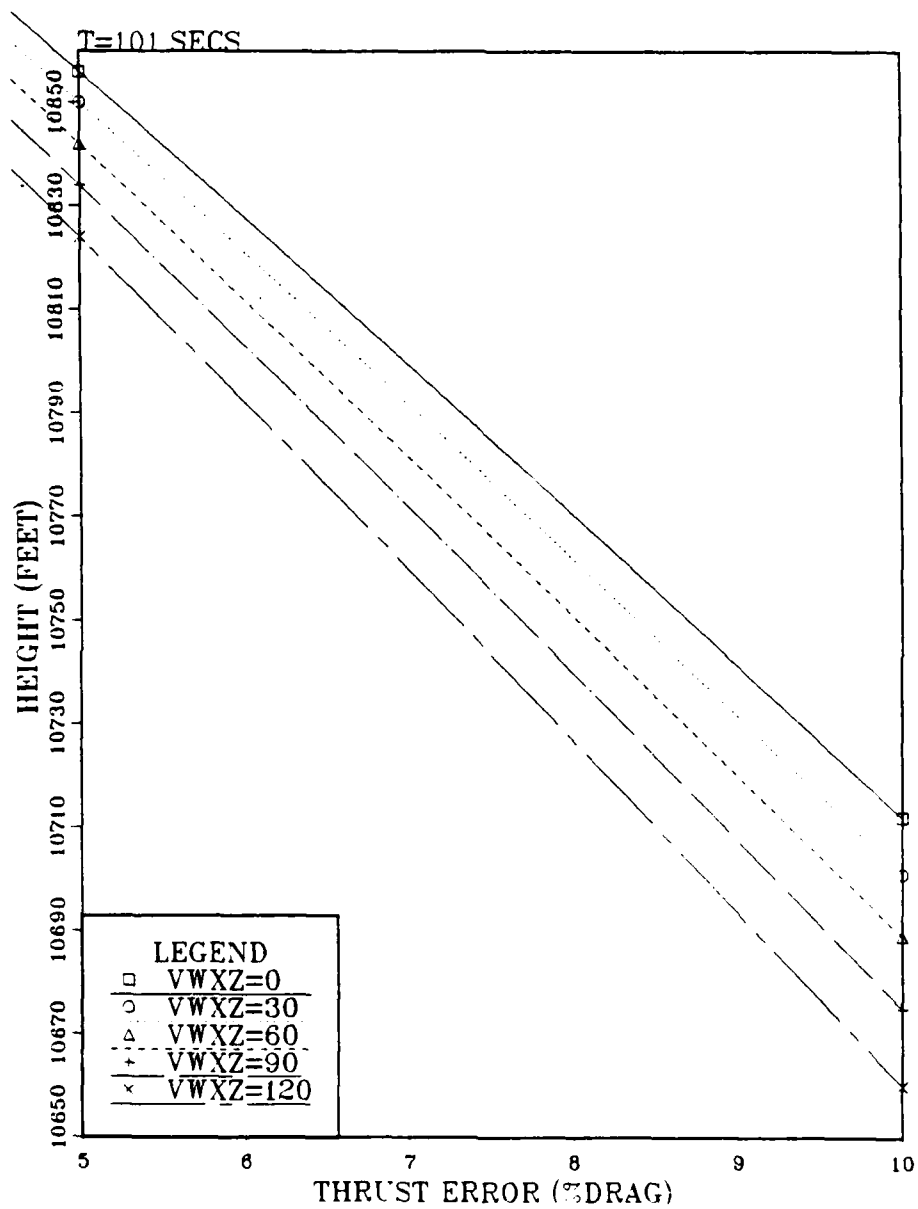
Figure 3-24C Headwind Sensitivity (Height)

72
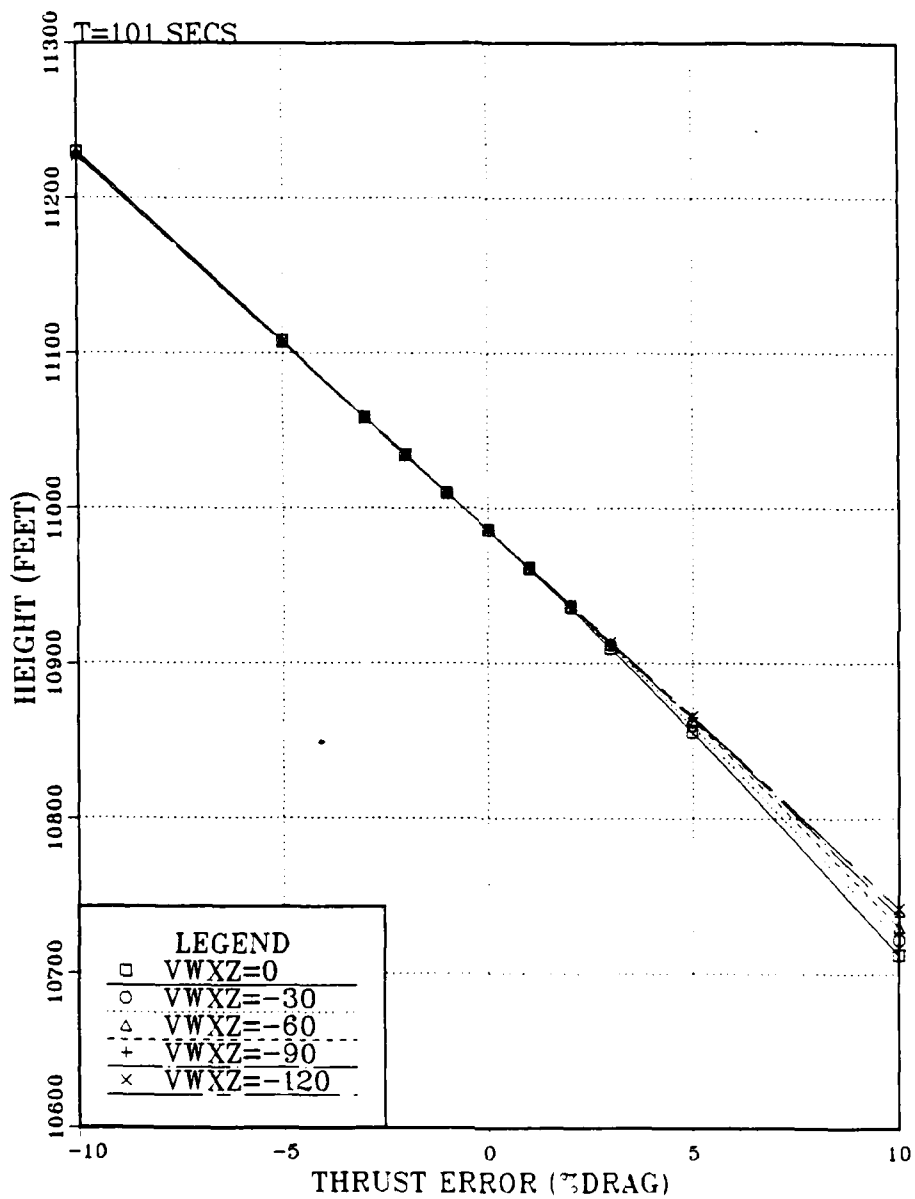
Figure 3-25 Tailwind Sensitivity (Height)

73
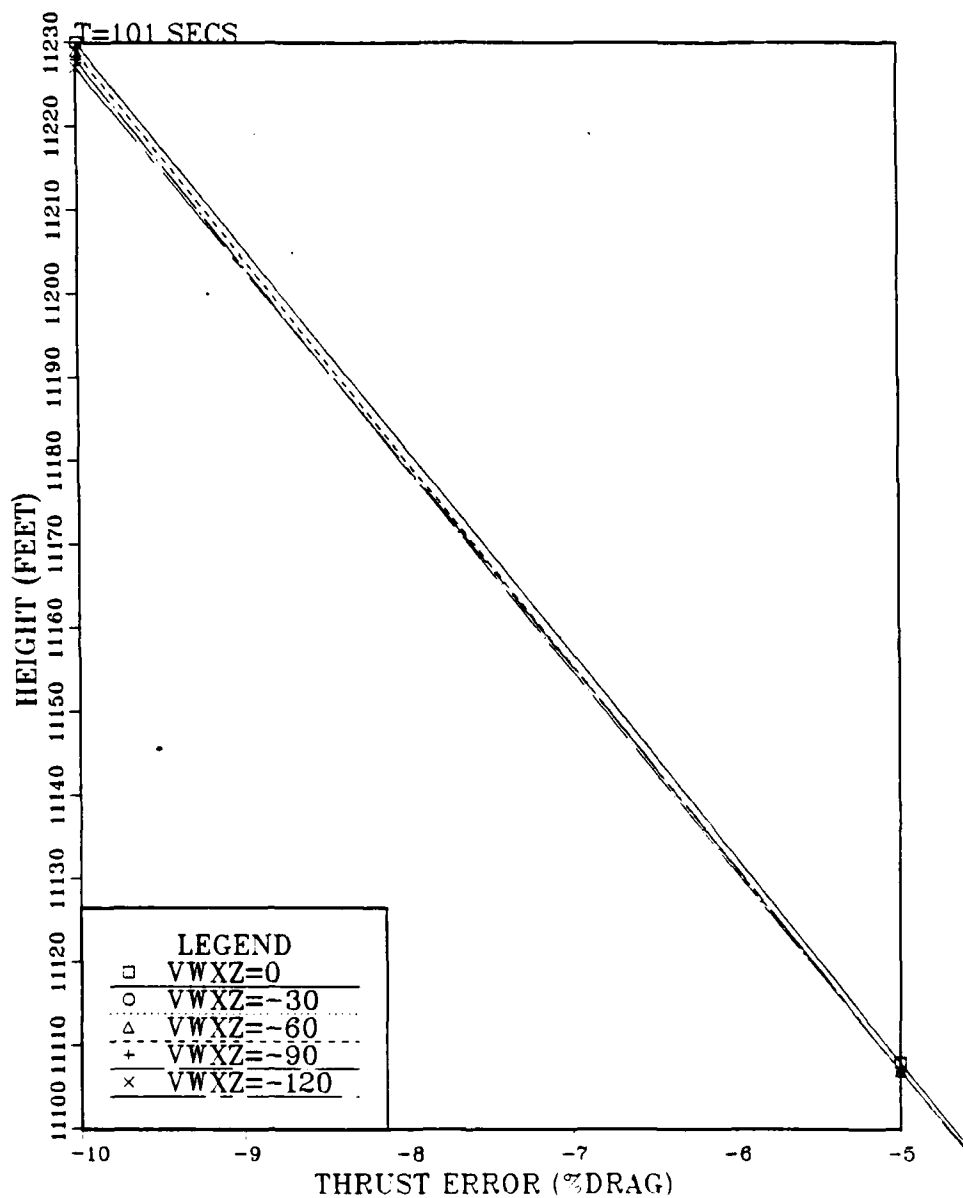
Figure 3-25A Tailwind Sensitivity (Height)

74
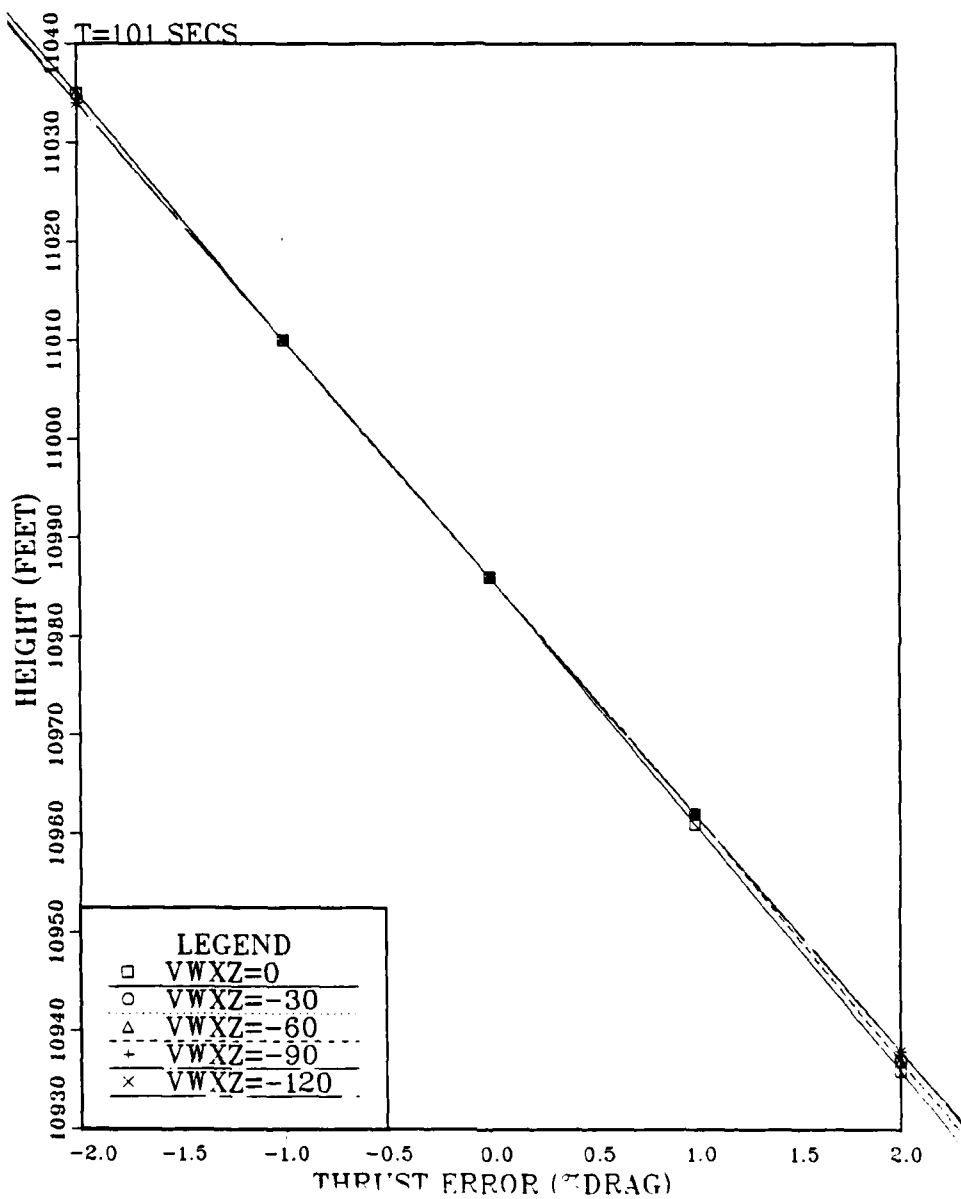
Figure 3-25B Tailwind Sensitivity (Height)
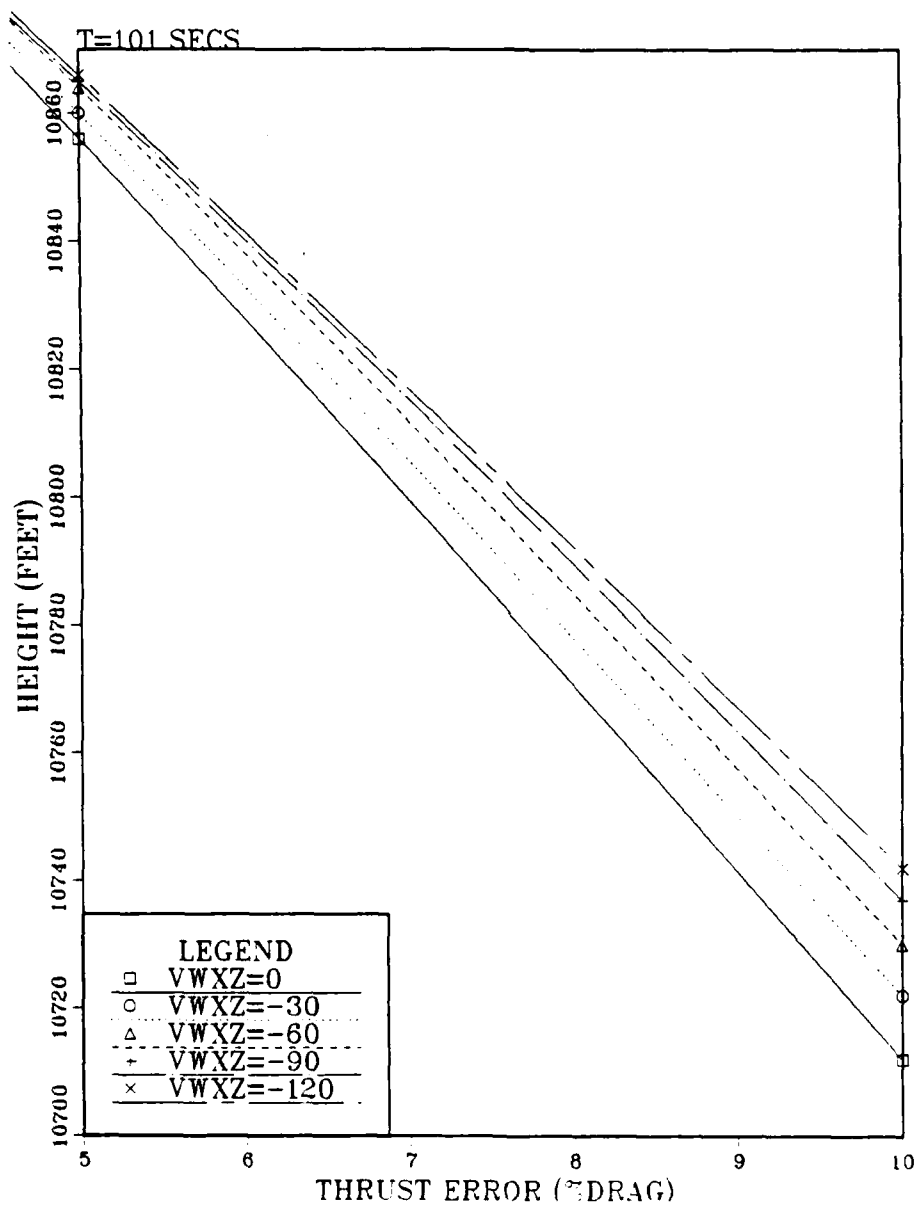
Figure 3-25C Tailwind Sensitivity (Height)
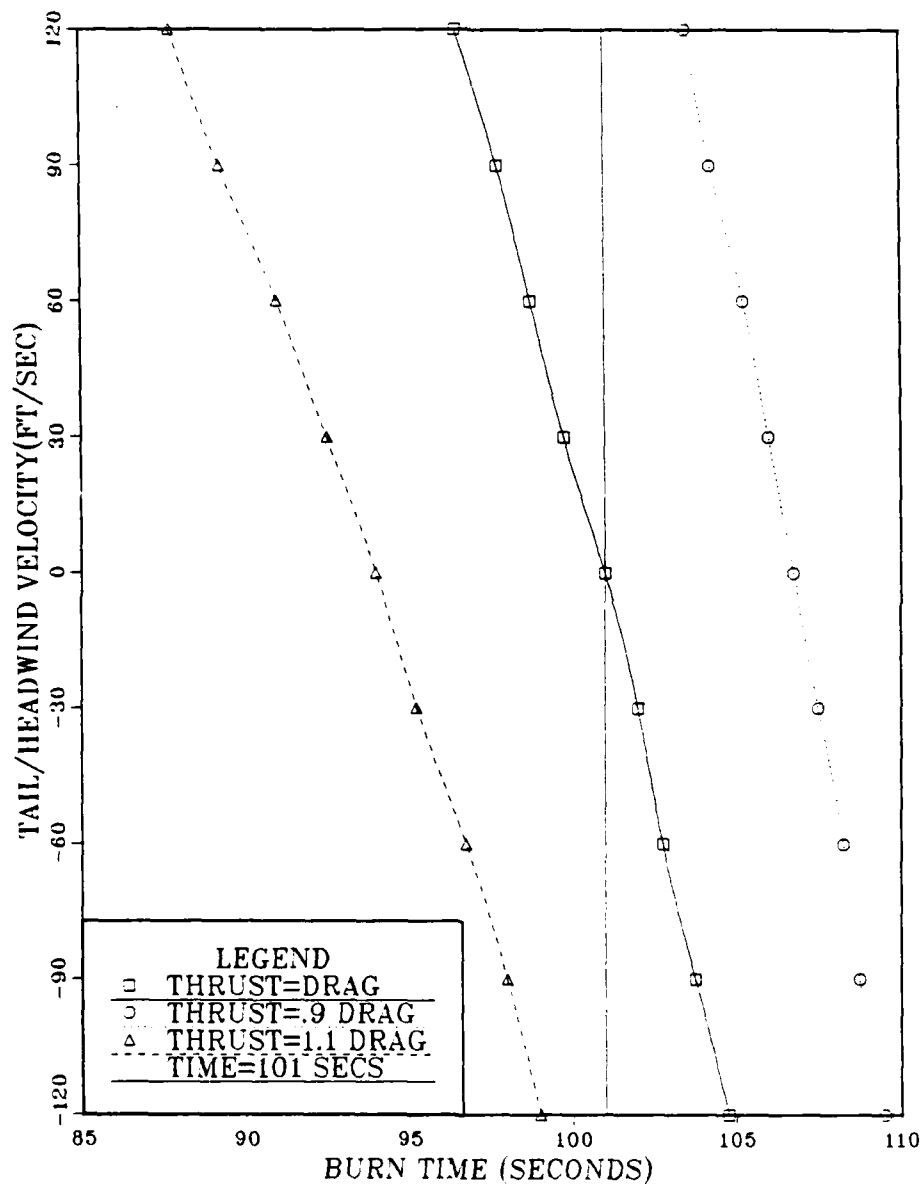
Figure 3-26 Tail/Headwind Effects (Burntime)

Deviations from the ideal trajectory were correlated and tabulated in Table 3.5.Results were conservatively linearized and are presented in that manner. Wind errors are read in addition to the thrust errors at the left of the table.For example:

```
If thrust error=-5%
   crosswind=120 ft/sec

predicted dispersion is X=-540 ft
                        Y=19 ft
                        Z=130 ft ;from ideal basket.
```

Table 3.5 Dispersion Analysis Results

| Errors | Thrust Errors | | Winds continuous 120 ft/sec | | | | |
	X	Z	Cross Y	Head X	Z	Tail X	Z
0 %	0	0	.1	30	7	.1	.1
1 %	110	25	4	30	15	10	1
2 %	220	50	8	40	20	20	2
5 %	540	130	19	50	32	50	10
10 %	1100	345	38	90	50	100	30

Velocities at time 101 seconds were measured and are shown at Figure 3-27. The total variation of extreme cases is from 2285 feet/sec to 2315 feet/sec, or only 30 feet/sec.
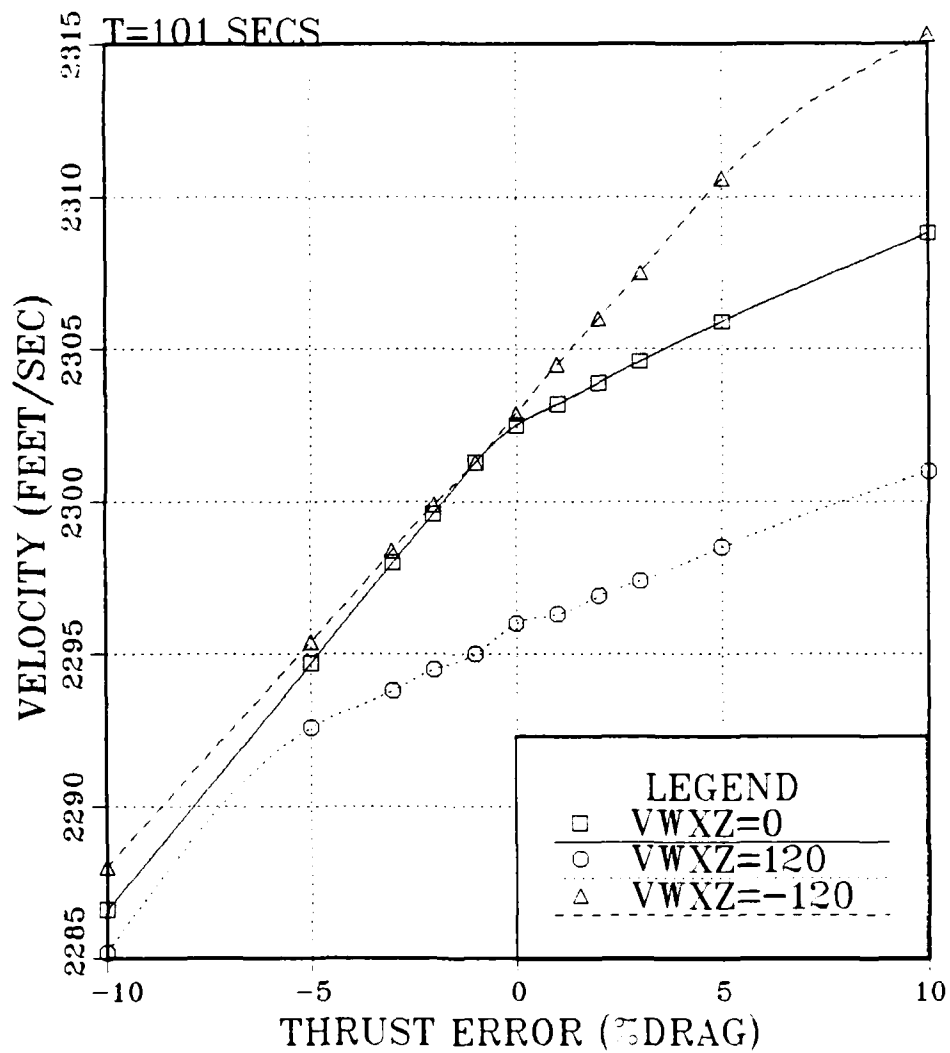
Figure 3-27 Velocity Sensitivity

Wind effects during near thrust equals drag portions of the trajectory were very small.The critical factor affecting the dispersion will be the setting of the terminal guidance clock in the projectile.This presents several options for setting initiation of terminal guidance:

-Fixed time irrespective of trajectory (ie. elevation of gun).Burn time would be shorter at less than 45 degree launch and the basket would be more sensitive to wind and thrust errors.As well the trajectory would change and so would the predicted basket.

-Fixed time for a given trajectory.This requires analysis of the sensitivity to elevation of the gun and a manual Tc setting method for gunners.

-Ramjet burnout.This would ensure that Tc occurred at an "optimum" point almost exactly on the pseudo-vacuum trajectory but the location along it at Tc would be difficult to predict.

-At given pressure for altitude [Reference 5].This would establish accurate baskets for given gun elevations assuming the altitude chosen was before ramjet burnout.

Several trajectories were simulated with a varying wind profile as a function of altitude in the Standard Atmosphere.These are shown at Figure 3-28 as compared to the pseudo-vacuum trajectory.

80
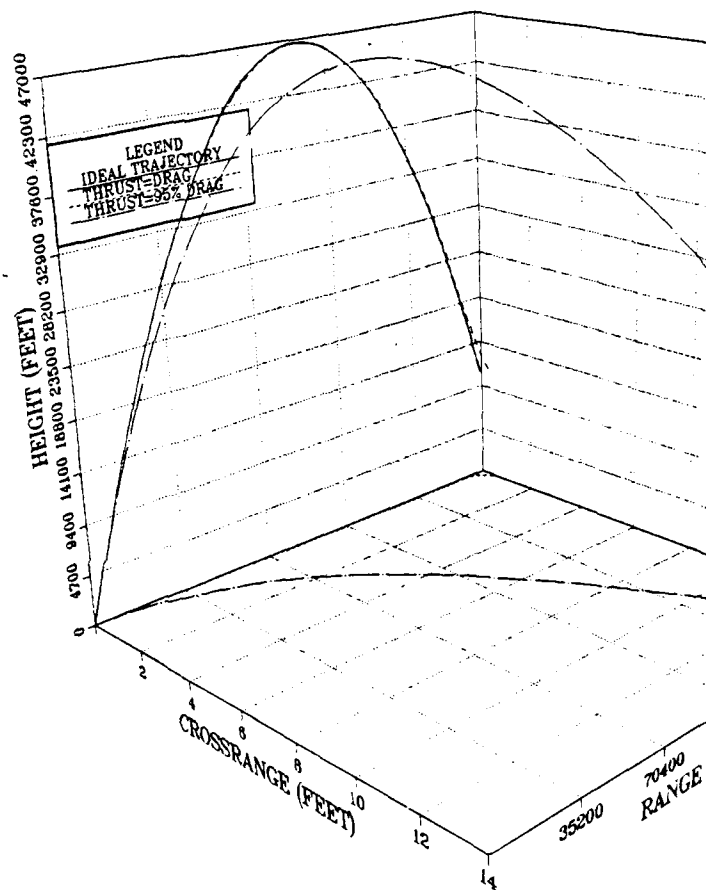
Figure 3-28 Three Dimensional Trajectory Dependent Wind Profile

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IV. CONCLUSIONS

Generally this thesis confirms the viability of th pseudo-vacuum trajectory from a thrust equals dra projectile.Indeed winds up to 120 feet per second and thrus errors up to five percent created dispersions of less tha 600 feet over a range of 175090 feet for the ARM projectile.

Specifically the following conclusions are made:

-the drag due to wind (Dw) is the aerodynami force which creates the most dispersion.

-the net lift due to transients (Lw) is a mino aerodynamic force in creating dispersion.

-the dispersion is proportional to the dampin coefficient (Cmq),although for practical values of Cm dispersion can be treated as insensitive to Cmq.

-the projectile resonance or short period is a approximately 0.22 Hz and is unstable in th resonance regime due to variable wind profiles.The phugoi is irrelevant.

-thrust errors are the most significant error contributing to dispersion.

-winds have a minor effect on dispersion durin powered flight when thrust approximates drag

except where harmonic content near resonance is contained in the wind profile.

   -headwinds create greater dispersion as ramjet burnout occurs before terminal guidance is initiated.Crosswinds and tailwinds generally will have minimal effects.

Recommendations for further study related to this thesis are:

   -Dynamics at launch including the initial spin damping, Magnus effects and aerodynamic jump.

   -Dynamics at terminal guidance including air inlet spike ejection and canard deployment.

   -Complete adaptation of BRL HTRAJ on the NPGS IBM system to use non-linear aerodynamics.

APPENDIX A-PROJECTILE CHARACTERISTICS
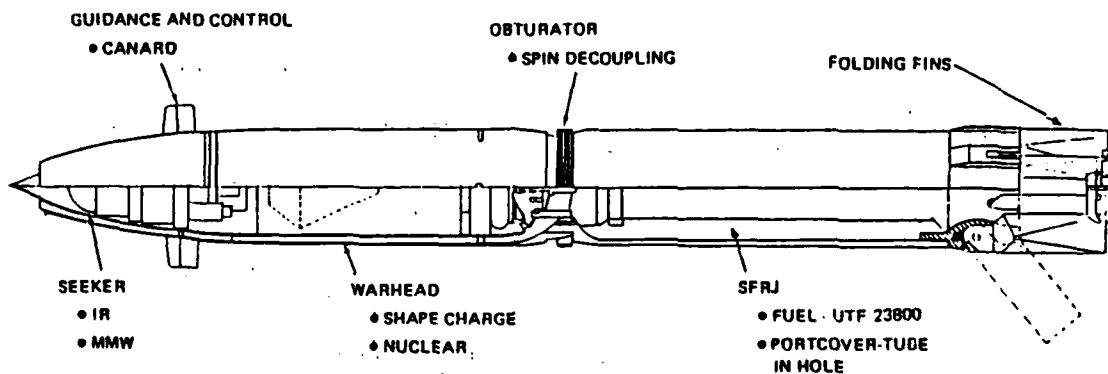
Figure A-1 ARMT Projectile Baseline Design

The following characteristics are obtained from References 2 and 6.

length=72 inches

diameter=8 inches

launch weight=225 lbm

launch CG=39.4 inches from spike apex

fuel weight=27 lbm (CG at 52.0 inches from apex)

impulse=950 "seconds"

Mass Property Equations:

CG=(225x39.4)-(52.0xfuel burned)/(225-fuel burned) in

Izz=.35-(.0019xfuel burned) in slug-ft

Ixx=Iyy=18.8-(.0423xfuel burned) in slug-ft

Aerodynamic Coefficient Equations:

Cd=Cdo +.5 x Cl x sin($\propto$)

Cdo= -.1025 x MACH + .5015   (1.8< MACH < 2.2)

Cm=Cl (Xcg-Xcp)/d

Cl=Cl$_\propto$ x $\propto$

Key Wind Tunnel Results (per degree):

MACH=1.8

        Cdo=.317   Cmq=-203

$\propto$	0	2	4	6	8	10
Cl	0	.18	.38	.62	.92	1.3
Xcp	45.4	45.6	48.2	49.7	50.2	50.0

MACH=2.2

        Cdo=.276   Cmq=-190

$\propto$	0	2	4	6	8	10
Cl	0	.19	.40	.65	.95	1.3
Xcp	42.9	42.9	44.6	45.1	46.0	44.6

Cmq=d(Cm)/d(qd/2V)

Initial Muzzle Spin Rate   30 PI radians /sec

APPENDIX B TRANSIENT ANGLE OF ATTACK CALCULATIONS

The following equation of motion applies to the dynamics of angle of attack (alpha) oscillations due to the torque equation described in the three-degrees-of-freedom model.

$$m\ddot{y} = Lw \text{ which is proportional to alpha(t)}$$

where angle of attack is of the form :

$$\alpha(t) = e^{-\delta t} \sin(wt) \text{ where } \delta \text{ is the damping constant}$$

and w is the angular velocity. Therefore:

$$my = \int_0^t \int_0^T \alpha(t) \, dt \, dT$$

$$= \int_0^t \int_0^T e^{-\delta t} \sin(wt) \, dt \, dT$$

$$= \int_0^t \left[\frac{e^{-\delta T} \left(-\delta \sin(wT) - w \cos(wT)\right) + w}{\delta^2 + w^2} \right] \, dT$$

$$= \frac{\left[\begin{array}{l} wt(\delta^2 + w^2) - 2\delta w + \\ e^{-\delta t}(\delta^2 \sin(wt) + 2\delta w \cos(wt) - w^2 \sin(wt)) \end{array} \right]}{(\delta^2 + w^2)^2}$$

When t=0, the equation reduces to:

$-2\delta w + 1(2\delta w) = 0$ which is expected if the initial condition is zero.(ie. dispersion at zero equals zero at time zero).

As t approaches infinity the equation value approaches infinite dispersion, but the oscillations of alpha have damped out. Note that the first derivative, proportional to velocity, tends to a constant value:

$(w/(\delta^2 + w^2))/m$ as t approaches infinity which is also to be expected.

APPENDIX C-PSEUDO-VACUUM TRAJECTORY CONCEPT

The basic concepts behind the pseudo-vacuum are not always readily apparent.This appendix analyzes the basic equations of motion in the following sequence of cases to illustrates the concept:

> vacuum trajectory
>
> atmosphere trajectory
>
> thrusted trajectory
>
> wind influenced trajectory
>
> thrust equal drag trajectory

In Figure C-1 (curve 1) the applicable equations of motion are:

$$m\ddot{x}_1 = 0$$

$$m\ddot{z}_1 = -mg$$

An accelometer on the projectile in the z direction would measure no acceleration as it is in free fall already. This is similar to a satellite orbit or someone on an elevator in free fall.

When atmosphere is added the key equations are:

$$m\ddot{x}_2 = -D_x = -1/2 \rho U_x^2 A C_d$$

$$m\ddot{z}_2 = -D_z - mg$$

where U is relative wind and D is atmospheric drag.In this

case Ux=Vx and Uz=Vz.This trajectory is represented by curve
2.An accelometer in the x direction measures Dx/m and Dz/m
in the z direction.

If thrust is added, the trajectory is as shown at curve
3(thrust greater than drag).The key equations are then:

$$m\ddot{x}_3 = -D_x + T_x$$

$$m\ddot{z}_3 = -D_z + T_z - mg$$

Accelerometers would measure (Tx-Dx)/m and (Ty-Dy)/m
respectively.If thrust equals drag the trajectory would be
curve 1.
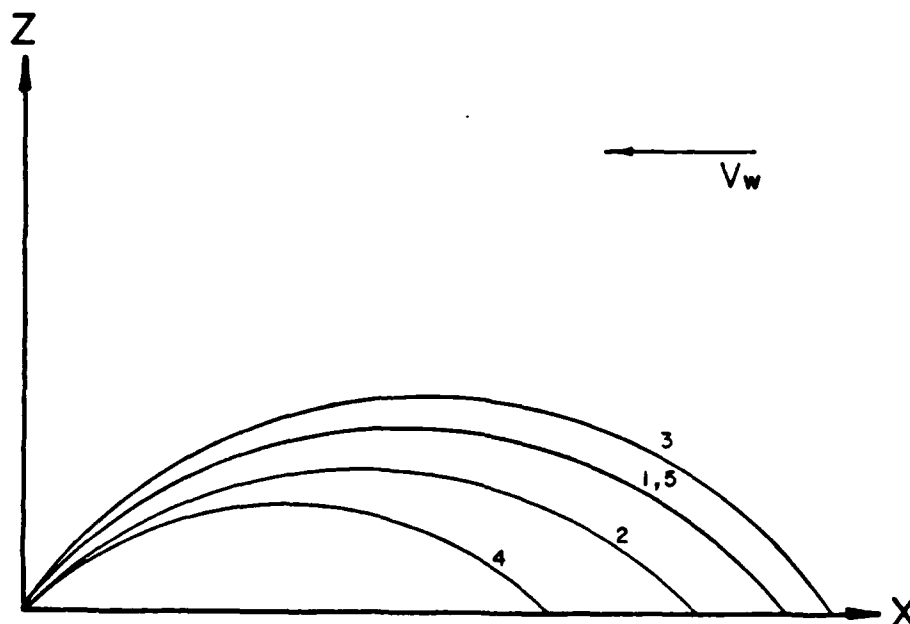
Figure C-1 Pseudo-Vacuum Trajectory Concept Curves

In Figure C-1 wind (Vw) has been added for the curve #4 in the x direction. The new equations are :

$$m\ddot{x}_4 = (-D_x + Dw) + T_x$$

$$m\ddot{z}_4 = -D_z + T_z - mg$$

where $Dx + Dw = 1/2 \, \rho \, U_x^2 \, C_d \, A$

and Ux(wind relative to the projectile) $=Vx+Vw$. With no thrust curve 4 results.

Finally, if thrust is added to equal drag the following equations are valid:

$$m\ddot{x}_5 = 0 \text{ or } T_x = D_x + Dw$$

$$m\ddot{z}_5 = -mg \text{ or } T_z = D_z$$

The accelerometer(s) read the acceleration caused by any differences in the thrust and drag forces (zero in this case).

It is clear that curves 1 and 5 are equal (and 3 if thrust=drag) but the burntime of a ramjet will not be equal in each case due to different drag profiles.

$$t = (\text{mass fuel})(\text{Isp})/\text{thrust}$$

Therefore headwinds will require more thrust and burntime will be shorter. Conversely tailwinds allow longer

burning.Burnout will occur on the vacuum trajectory but not
at the same point, as shown in Figure C-2.
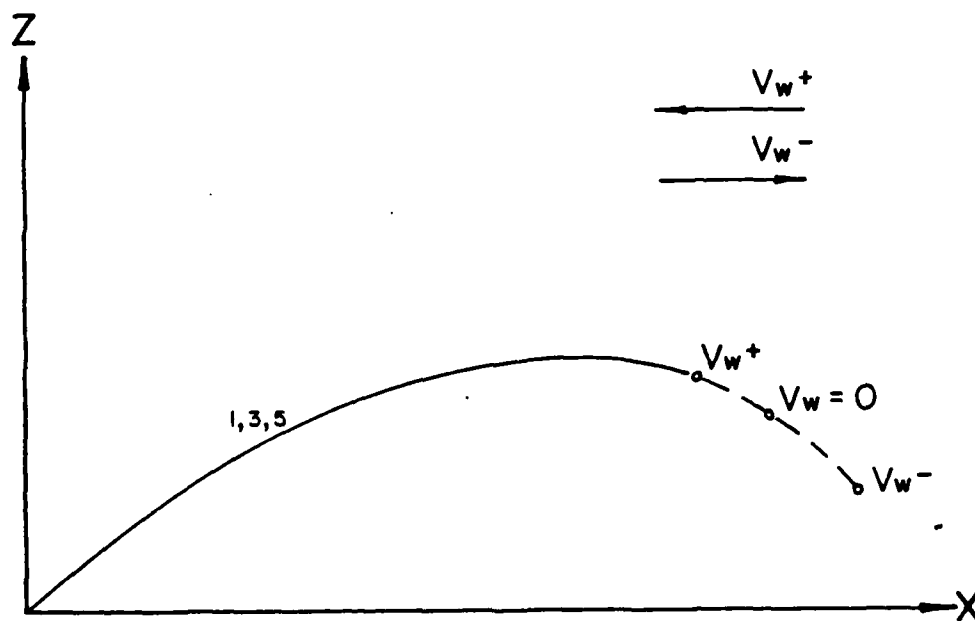
Figure C-2 Burnout Variations

APPENDIX D PSEUDO-VACUUM TRAJECTORY PROGRAM

```
10 DIM X(300),Y(300),RO(300),D(300),MDOT(300),M(300),V(300)
12 DIM CDO(300),MA(300)
15 DIM T(300)
20 MMIN=198
30 ISP=950
40 DELT=.5
50 M(1)=225
60 THETA=.7853981634000006#
70 VO=2452
75 LPRINT "TIME","X","Y","MASS","SPEED"
80 FOR I=1 TO 300
90    X(I)=VO*COS(THETA)*T(I)
100   Y(I)=(VO*SIN(THETA)*T(I))-(16.087*T(I)^2)
110   V(I)=((VO*COS(THETA))^2+(VO*SIN(THETA)-
      32.174*T(I))^2)^.5
120   TEMP =518.688-.0035662*Y(I)
150   RO(I)=(2116.22*(1-(.0035662*Y(I)/518.688))^5.256)/
      (1716.5*TEMP)
155   IF Y(I))=36089! THEN RO(I)=.001271
157 IF Y(I))=36089! THEN TEMP=389.99
158 MA(I)=V(I)/SQR(1.4*1716.3*TEMP)
159 CDO(I)=.5015-.1025*MA(I)
160   D(I)=.276*.5*RO(I)*.3491*V(I)^2
161 D(I)=D(I)/.276*CDO(I)
170   MDOT(I+1)=D(I)/ISP
180   M(I+1)=M(I)-MDOT(I)*DELT
190   T(I+1)=T(I)+DELT
195 LPRINT T(I),X(I),Y(I),M(I),V(I)
200   IF M(I+1)<=MMIN GOTO 220
210 NEXT I
220   LPRINT "RAMJET BURNOUT BETWEEN T=";T(I);"AND";T(I+1)
```

TIME	X	Y	MASS	SPEED
0	0	0	225	2452
.5	866.913	862.891	225	2440.65
1	1733.83	1717.74	224.637	2429.36
1.5	2600.74	2564.54	224.286	2418.11
2	3467.65	3403.3	223.947	2406.93
2.5	4334.57	4234.02	223.618	2395.8
3	5201.48	5056.7	223.3	2384.73
3.5	6068.39	5871.32	222.993	2373.71
4	6935.3	6677.91	222.695	2362.75
4.5	7802.22	7476.46	222.407	2351.85
5	8669.13	8266.96	222.128	2341.01
5.5	9536.04	9049.41	221.858	2330.24
6	10403	9823.82	221.597	2319.52
6.5	11269.9	10590.2	221.344	2308.86
7	12136.8	11348.5	221.099	2298.27
7.5	13003.7	12098.8	220.861	2287.74
8	13870.6	12841	220.631	2277.28
8.5	14737.5	13575.2	220.409	2266.89
9	15604.4	14301.4	220.193	2256.55
9.5	16471.3	15019.5	219.983	2246.29
10	17338.3	15729.6	219.781	2236.1
10.5	18205.2	16431.6	219.584	2225.98
11	19072.1	17125.6	219.394	2215.92
11.5	19939	17811.5	219.209	2205.94
12	20805.9	18489.4	219.03	2196.03
12.5	21672.8	19159.2	218.856	2186.2
13	22539.7	19821	218.687	2176.43
13.5	23406.7	20474.8	218.523	2166.75
14	24273.6	21120.5	218.364	2157.14
14.5	25140.5	21758.2	218.21	2147.61
15	26007.4	22387.8	218.061	2138.15
15.5	26874.3	23009.4	217.915	2128.78
16	27741.2	23622.9	217.774	2119.49
16.5	28608.1	24228.4	217.637	2110.27
17	29475	24825.9	217.504	2101.14
17.5	30342	25415.3	217.374	2092.1
18	31208.9	25996.7	217.248	2083.14
18.5	32075.8	26570	217.126	2074.27
19	32942.7	27135.3	217.007	2065.48
19.5	33809.6	27692.5	216.891	2056.78
20	34676.5	28241.7	216.778	2048.17
20.5	35543.4	28782.9	216.669	2039.65
21	36410.3	29316	216.562	2031.23
21.5	37277.3	29841	216.458	2022.89
22	38144.2	30358.1	216.357	2014.65
22.5	39011.1	30867	216.258	2006.51
23	39878	31368	216.162	1998.46
23.5	40744.9	31860.9	216.068	1990.51
24	41611.8	32345.7	215.977	1982.66
24.5	42478.7	32822.5	215.888	1974.9
25	43345.7	33291.3	215.801	1967.25
25.5	44212.6	33752	215.717	1959.7
26	45079.5	34204.7	215.634	1952.26
26.5	45946.4	34649.3	215.553	1944.91
27	46813.3	35085.9	215.474	1937.68
27.5	47680.2	35514.4	215.397	1930.55
28	48547.1	35934.9	215.322	1923.53
28.5	49414	36347.4	215.249	1916.62
29	50281	36751.8	215.177	1909.82
29.5	51147.9	37148.2	215.048	1903.13

30	52014.8	37536.5	214.921	1896.95
30.5	52881.7	37916.8	214.794	1890.09
31	53748.6	38289	214.668	1883.74
31.5	54615.5	38653.2	214.542	1877.51
32	55482.4	39009.3	214.417	1871.4
32.5	56349.3	39357.4	214.292	1865.4
33	57216.3	39697.5	214.168	1859.53
33.5	58083.2	40029.5	214.045	1853.78
34	58950.1	40353.5	213.922	1848.14
34.5	59817	40669.5	213.799	1842.64
35	60683.9	40977.3	213.677	1837.25
35.5	61550.8	41277.2	213.556	1831.99
36	62417.7	41569	213.435	1826.86
36.5	63284.6	41852.7	213.314	1821.86
37	64151.6	42128.5	213.194	1816.98
37.5	65018.5	42396.1	213.075	1812.24
38	65885.4	42655.8	212.956	1807.62
38.5	66752.3	42907.3	212.837	1803.14
39	67619.2	43150.9	212.719	1798.79
39.5	68486.1	43386.4	212.601	1794.57
40	69353	43613.8	212.483	1790.49
40.5	70220	43833.3	212.366	1786.54
41	71086.9	44044.6	212.249	1782.73
41.5	71953.8	44247.9	212.133	1779.06
42	72820.7	44443.2	212.017	1775.52
42.5	73687.6	44630.5	211.901	1772.12
43	74554.5	44809.7	211.786	1768.87
43.5	75421.4	44980.8	211.671	1765.75
44	76288.3	45143.9	211.556	1762.78
44.5	77155.3	45299	211.441	1759.95
45	78022.2	45446	211.327	1757.26
45.5	78889.1	45585	211.213	1754.71
46	79756	45715.9	211.099	1752.31
46.5	80622.9	45838.8	210.986	1750.05
47	81489.8	45953.6	210.873	1747.94
47.5	82356.7	46060.4	210.76	1745.97
48	83223.7	46159.2	210.647	1744.15
48.5	84090.6	46249.9	210.534	1742.47
49	84957.5	46332.6	210.421	1740.95
49.5	85824.4	46407.2	210.309	1739.57
50	86691.3	46473.8	210.197	1738.34
50.5	87558.2	46532.3	210.085	1737.25
51	88425.1	46582.8	209.973	1736.32
51.5	89292	46625.3	209.861	1735.53
52	90158.9	46659.7	209.749	1734.89
52.5	91025.9	46686.1	209.637	1734.4
53	91892.8	46704.4	209.526	1734.06
53.5	92759.7	46714.7	209.414	1733.87
54	93626.6	46716.9	209.302	1733.83
54.5	94493.5	46711.1	209.191	1733.94
55	95360.4	46697.3	209.079	1734.19
55.5	96227.3	46675.3	208.967	1734.6
56	97094.3	46645.5	208.856	1735.16
56.5	97961.2	46607.4	208.744	1735.86
57	98828.1	46561.4	208.632	1736.71
57.5	99695	46507.4	208.521	1777.72
58	100562	46445.2	208.409	1738.86
58.5	101429	46375.1	208.297	1740.16
59	102296	46296.9	208.185	1741.61
59.5	103163	46210.6	208.073	1743.2
60	104030	46116.4	207.96	1744.94
60.5	104896	46014	207.848	1746.82
61	105763	45903.6	207.735	1748.86
61.5	106630	45785.2	207.623	1751.03
62	107497	45658.8	207.51	1753.36
62.5	108364	45524.3	207.396	1755.83

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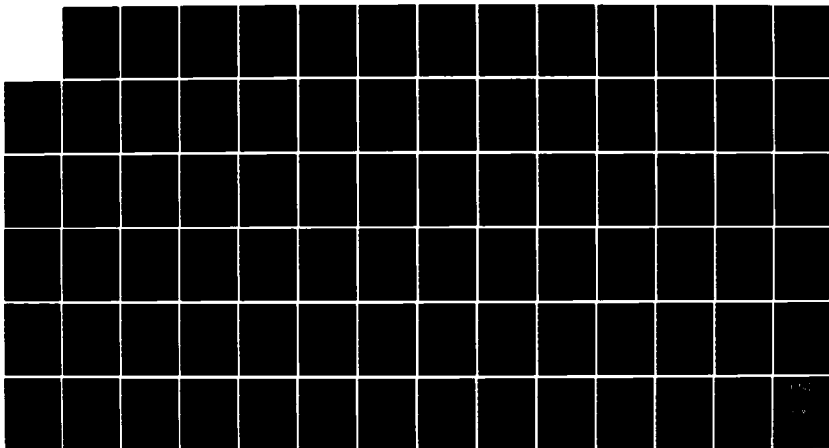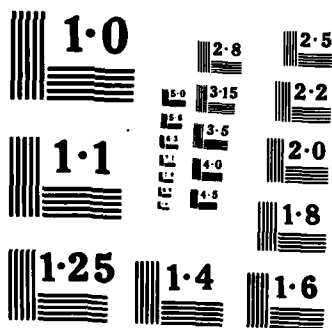
63	109231	45381.7	207.283	1758.43
63.5	110098	45231.1	207.169	1761.18
64	110965	45072.5	207.056	1764.08
64.5	111832	44905.8	206.942	1767.12
65	112699	44731.1	206.827	1770.3
65.5	113566	44548.4	206.713	1773.61
66	114433	44357.5	206.598	1777.07
66.5	115299	44158.7	206.482	1780.67
67	116166	43951.8	206.367	1784.4
67.5	117033	43736.9	206.251	1788.28
68	117900	43513.9	206.135	1792.28
68.5	118767	43282.9	206.018	1796.43
69	119634	43043.8	205.901	1800.7
69.5	120501	42796.6	205.784	1805.11
70	121368	42541.5	205.666	1809.65
70.5	122235	42278.4	205.548	1814.33
71	123102	42007.2	205.43	1819.13
71.5	123969	41727.8	205.311	1824.06
72	124835	41440.4	205.191	1829.13
72.5	125702	41145.1	205.072	1834.31
73	126569	40841.7	204.951	1839.63
73.5	127436	40530.2	204.831	1845.07
74	128303	40210.7	204.709	1850.63
74.5	129170	39883.1	204.588	1856.32
75	130037	39547.5	204.466	1862.12
75.5	130904	39204	204.343	1868.05
76	131771	38852.3	204.22	1874.1
76.5	132638	38492.6	204.096	1880.26
77	133505	38124.8	203.972	1886.55
77.5	134372	37749	203.847	1892.94
78	135238	37365.1	203.721	1899.46
78.5	136105	36973.2	203.595	1906.08
79	136972	36573.3	203.469	1912.82
79.5	137839	36165.2	203.342	1919.67
80	138706	35749.3	203.214	1926.63
80.5	139573	35325.3	203.086	1933.7
81	140440	34893.1	203.013	1940.88
81.5	141307	34453	202.939	1948.16
82	142174	34004.7	202.863	1955.55
82.5	143041	33548.5	202.785	1963.04
83	143908	33084.2	202.705	1970.63
83.5	144774	32611.9	202.624	1978.33
84	145641	32131.5	202.54	1986.13
84.5	146508	31643.2	202.454	1994.03
85	147375	31146.6	202.367	2002.02
85.5	148242	30642.1	202.277	2010.11
86	149109	30129.7	202.184	2018.3
86.5	149976	29608.9	202.09	2026.58
87	150843	29080.4	201.992	2034.96
87.5	151710	28543.7	201.893	2043.42
88	152577	27999	201.79	2051.98
88.5	153444	27446.2	201.685	2060.63
89	154311	26885.3	201.577	2069.37
89.5	155177	26316.6	201.466	2078.19
90	156044	25739.6	201.352	2087.11
90.5	156911	25154.7	201.235	2096.1
91	157778	24561.8	201.114	2105.19
91.5	158645	23960.8	200.99	2114.35
92	159512	23351.6	200.863	2123.6
92.5	160379	22734.5	200.732	2132.93
93	161246	22109.3	200.597	2142.34
93.5	162113	21476.1	200.458	2151.83
94	162980	20834.9	200.315	2161.39
94.5	163847	20185.7	200.168	2171.04
95	164713	19528.3	200.016	2180.76
95.5	165580	19862.3	199.36	2190.75

96	166447	18189.5	199.699	2200.42
96.5	167314	17508	199.533	2210.36
97	168181	16818.6	199.362	2220.38
97.5	169048	16121	199.186	2230.46
98	169915	15415.4	199.004	2240.62
98.5	170782	14701.8	198.817	2250.84
99	171649	13980	198.623	2261.13
99.5	172516	13250.3	198.424	2271.49
100	173383	12512.6	198.218	2281.92
100.5	174250	11766.9	198.006	2292.41

RAMJET BURNOUT BETWEEN T= 100.5 AND 101

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APPENDIX E- THREE CEGREES OF FREEDOM RESULTS

VARIABLES & INITIAL CONDITIONS:
```
XDOT = 2168.6700000
X = .0
YDOT = .0
Y = .0
THEDOT = .0
THETA = .0
M = 225.0000000
T = .0
```

CONSTANTS:
```
PHASE = .0
CMA = -2.3080000000
A = .3491000000000
DI = .6666670000000
CMT = .1900000000000
CDO = .2760000000000
PI = 3.1415926540
ISP = 550.0000000
LAMBCA = .1500000000
PI8 = .3526900E17
```

SPECIAL FUNCTIONS:
```
ETA = ATAN(Y(CT)/X(CT))
VCG = (XCCT**2+YDCT**2)**.5
VW = 0
GAMMA = ATAN((YCOT+VW)/XCCT)
V = (XDOT**2+(YDOT+VW)**2)**.5
Q = .5*.0008*C68*V**2
K = G*DI*A
THEDBL = (CMA*K*(THETA-GAMMA)-((CMT*K*DI*THEDCT)/(V*2)))/I
ALPHA = GAMMA-THETA
CD = CDO+.5*(CL*SIN(ALPHA)
CL = .C91*ALFFA
L = CL*Q*A
D = C*CD*G*A
XDBL = (L*SIN(GAMMA)-D*CCS(GAMMA))/M
YDBL = (L*CCS(GAMMA)+D*SIN(GAMMA))/M
C = C
MDOT = (1-C)*(CDO+.5*CL*SIN(ALPHA))*G*A/(-ISP)
DELM = 225-M
I = (18.E-.0423*CELM)*32.2
```

DERIVATIVES:
```
D(XDCT)/C(T) , = =
```

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```
D(X        )=EL
D(X   /D(T  )  = =
X=CT
D(YDCT /C(T ) ) = =
D(Y  /D(I  )  = =
Y=DCT
D(THEDOT/C(T ) = =
     THEDEL
D(THETA /D(T ) = =
     THEDCT
D(M  /D(T  )  = =
     MDOT

OUTPUTS:
   TITLE: THREE DEGREE CRCSSWIND TRIAL
   TABULATE: T                    X           Y         VCG        V         MDOT
     AT INTERVAL     .50CC000000
   PLOT: X
     AGAINST: T
   PLCT: Y
     AGAINST: T
   PLCT: ALPHA
     AGAINST: T           AT INTERVAL     .250C000C00

END CALCLLATICN WHEN M .LE. 198.000

THREE CEGREE CROSSWIND TRIAL
```

T	X	Y	VCG	V	MDOT
.0000000	1C94.3	.0000000	2188.7	2188.7	-.216237
1.000000	2188.7	.0000000	2188.7	2188.7	-.216237
1.500000	3283.0	.0000000	2188.7	2188.7	-.216237
2.000000	4377.3	.0000000	2188.7	2188.7	-.216237
2.500000	5471.7	.0000000	2188.7	2188.7	-.216237
3.000000	6566.0	.0000000	2188.7	2188.7	-.216237
3.500000	7660.3	.0000000	2188.7	2188.7	-.216237
4.000000	8754.7	.0000000	2188.7	2188.7	-.216237
4.500000	9849.0	.0000000	2188.7	2188.7	-.216237
5.000000	1C943.	.0000000	2188.7	2188.7	-.216237
5.500000	12038.	.0000000	2188.7	2188.7	-.216237
6.000000	13132.	.0000000	2188.7	2188.7	-.216237
6.500000	14226.	.0000000	2188.7	2188.7	-.216237
7.000000	15321.	.0000000	2188.7	2188.7	-.216237
7.5000C0	16415.	.0000000	2188.7	2188.7	-.216237
8.000000	17509.	.0000000	2188.7	2188.7	-.216237
8.5000C0	18604.	.00	2188.7	2188.7	-.216237

T	X	Y	VCG	V	MDOT
33.000	72226.	.0	2188.7	2188.7	-.21637
33.500	73320.	.0	2188.7	2188.7	-.21637
34.000	74415.	.0	2188.7	2188.7	-.21637
34.500	75509.	.0	2188.7	2188.7	-.21637
35.000	76603.	.0	2188.7	2188.7	-.21637
35.500	77698.	.0	2188.7	2188.7	-.21637
36.000	78792.	.0	2188.7	2188.7	-.21637
36.500	79886.	.0	2188.7	2188.7	-.21637
37.000	80981.	.0	2188.7	2188.7	-.21637
37.500	82075.	.0	2188.7	2188.7	-.21637
38.000	83169.	.0	2188.7	2188.7	-.21637
38.500	84264.	.0	2188.7	2188.7	-.21637
39.000	85358.	.0	2188.7	2188.7	-.21637
39.500	86452.	.0	2188.7	2188.7	-.21637
40.000	87547.	.0	2188.7	2188.7	-.21637
40.500	88641.	.0	2188.7	2188.7	-.21637
41.000	89735.	.0	2188.7	2188.7	-.21637
41.500	90830.	.0	2188.7	2188.7	-.21637
42.000	91924.	.0	2188.7	2188.7	-.21637
42.500	93018.	.0	2188.7	2188.7	-.21637
43.000	94113.	.0	2188.7	2188.7	-.21637
43.500	95207.	.0	2188.7	2188.7	-.21637
44.000	96301.	.0	2188.7	2188.7	-.21637
44.500	97396.	.0	2188.7	2188.7	-.21637
45.000	98490.	.0	2188.7	2188.7	-.21637
45.500	99584.	.0	2188.7	2188.7	-.21637
46.000	.100068D+06	.0	2188.7	2188.7	-.21637
46.500	.101177D+06	.0	2188.7	2188.7	-.21637
47.000	.102287D+06	.0	2188.7	2188.7	-.21637
47.500	.103396D+06	.0	2188.7	2188.7	-.21637
48.000	.104506D+06	.0	2188.7	2188.7	-.21637
48.500	.105615D+06	.0	2188.7	2188.7	-.21637
49.000	.106724D+06	.0	2188.7	2188.7	-.21637
49.500	.107834D+06	.0	2188.7	2188.7	-.21637
50.000	.108943D+06	.0	2188.7	2188.7	-.21637
50.500	.110053D+06	.0	2188.7	2188.7	-.21637
51.000	.111162D+06	.0	2188.7	2188.7	-.21637
51.500	.112272D+06	.0	2188.7	2188.7	-.21637
52.000	.113381D+06	.0	2188.7	2188.7	-.21637
52.500	.114491D+06	.0	2188.7	2188.7	-.21637
53.000	.116000D+06	.0	2188.7	2188.7	-.21637
53.500	.117109D+06	.0	2188.7	2188.7	-.21637
54.000	.118195D+06	.0	2188.7	2188.7	-.21637
54.500	.119280D+06	.0	2188.7	2188.7	-.21637
55.000	.120380D+06	.0	2188.7	2188.7	-.21637
55.500	.121470D+06	.0	2188.7	2188.7	-.21637

172900D+06
174000D+06
175090D+06
176190D+06
177280D+06
178380D+06
179470D+06
180570D+06
181660D+06
182750D+06
183850D+06
184940D+06
186040D+06
187130D+06
188230D+06
189320D+06
190410D+06
191510D+06
192600D+06
193700D+06
194790D+06
195890D+06
196980D+06
198070D+06
199170D+06
200260D+06
201360D+06
202450D+06
203550D+06
204640D+06
205730D+06
206830D+06
207920D+06
209020D+06
210110D+06
211210D+06
212300D+06
213400D+06
214490D+06
215580D+06
216680D+06
217770D+06
218870D+06
219960D+06
221060D+06
222150D+06
223240D+06
224340D+06

T	MDOT	V	VCG	Y	X
103.00	-.21637	2188.7	2188.7	.0	.225430+06
103.50	-.21637	2188.7	2188.7	.0	.226530+06
104.00	-.21637	2188.7	2188.7	.0	.227620+06
104.50	-.21637	2188.7	2188.7	.0	.228720+06
105.00	-.21637	2188.7	2188.7	.0	.229810+06
105.50	-.21637	2188.7	2188.7	.0	.230900+06
106.00	-.21637	2188.7	2188.7	.0	.232000+06
106.50	-.21637	2188.7	2188.7	.0	.233090+06
107.00	-.21637	2188.7	2188.7	.0	.234190+06
107.50	-.21637	2188.7	2188.7	.0	.235280+06
108.00	-.21637	2188.7	2188.7	.0	.236380+06
108.50	-.21637	2188.7	2188.7	.0	.237470+06
109.00	-.21637	2188.7	2188.7	.0	.238570+06
109.50	-.21637	2188.7	2188.7	.0	.239660+06
110.00	-.21637	2188.7	2188.7	.0	.240750+06
110.50	-.21637	2188.7	2188.7	.0	.241850+06
111.00	-.21637	2188.7	2188.7	.0	.242940+06
111.50	-.21637	2188.7	2188.7	.0	.244040+06
112.00	-.21637	2188.7	2188.7	.0	.245130+06
112.50	-.21637	2188.7	2188.7	.0	.246230+06
113.00	-.21637	2188.7	2188.7	.0	.247320+06
113.50	-.21637	2188.7	2188.7	.0	.248410+06
114.00	-.21637	2188.7	2188.7	.0	.249510+06
114.50	-.21637	2188.7	2188.7	.0	.250600+06
115.00	-.21637	2188.7	2188.7	.0	.251700+06
115.50	-.21637	2188.7	2188.7	.0	.252790+06
116.00	-.21637	2188.7	2188.7	.0	.253890+06
116.50	-.21637	2188.7	2188.7	.0	.254980+06
117.00	-.21637	2188.7	2188.7	.0	.256070+06
117.50	-.21637	2188.7	2188.7	.0	.257170+06
118.00	-.21637	2188.7	2188.7	.0	.258260+06
118.50	-.21637	2188.7	2188.7	.0	.259360+06
119.00	-.21637	2188.7	2188.7	.0	.260450+06
119.50	-.21637	2188.7	2188.7	.0	.261550+06
120.00	-.21637	2188.7	2188.7	.0	.262640+06
120.50	-.21637	2188.7	2188.7	.0	.263730+06
121.00	-.21637	2188.7	2188.7	.0	.264830+06
121.50	-.21637	2188.7	2188.7	.0	.265920+06
122.00	-.21637	2188.7	2188.7	.0	.267020+06
122.50	-.21637	2188.7	2188.7	.0	.268110+06
123.00	-.21637	2188.7	2188.7	.0	.269210+06
123.50	-.21637	2188.7	2188.7	.0	.270300+06
124.00	-.21637	2188.7	2188.7	.0	.271400+06
124.50	-.21637	2188.7	2188.7	.0	.272490+06
125.00	-.21637	2188.7	2188.7	.0	.273580+06

```
END OF RUN
VARIABLES & INITIAL CONDITIONS:
XDOT = 218.67000C
X = .0
YDOT = .0
Y = .0
THEDOT = .0
THETA = .0
M = 225.0000000
T = .0

CONSTANTS:
PHASE = .0
CMA = -2.308000000C
A = .349100000CC
DI = .66666670000
CMT = 190.000000000
CDO = .2760000000
PI = 3.141592654
ISP = 950.000000000
LAMBCA = 150000.00000
PI8 = .3526959E17

SPECIAL FUNCTIONS:
ETA = ATAN(YDOT/XDOT)
VCG = (XDOT**2+YDOT**2)**.5
VW = 60
GAMMA = ATAN((YDOT+VW)/XDOT)
V = (XDOT**2+(YDOT+VW)**2)**.5
Q = .5*.CCOESCEE*V**2
K = G*DI*A
THEDEL = (CMA*K*(THETA-GAMMA)-((CMT*K*DI*THEDOT)/(V*2)))/I
ALPHA = GAMMA-THETA
CD = CDO+.5*CL*SIN(ALPHA)
CL = .091*ALPHA
L = CL*Q*A
D = C*CD*C*A
XDBL = (L*SIN(GAMMA)-D*CCS(GAMMA))/M
YDBL = (L*COS(GAMMA)+D*SIN(GAMMA))/M
C = C
MDOT = (1-C)*(CDO+.5*CL*SIN(ALPHA))*Q*A/(-ISP)
DELM = 225-M
I = (18.E-.C423*DELM)*32.2

DERIVATIVES:
D(XDOT/C(T)) = =
XDBL
D(X /D(T)) = =
```

```
D(YDCT/DC(T ) = =     XDOT
D(Y /D(T ) = =        YDBL
                      YCOT
D(THEDCT/DC(T ) = =   THEDBL
D(THETA/DC(T ) = =    THEDCT
D(M /D(T ) = =        MDCT

OUTPLTS:
TITLE: THREE CEGREE CRCSSWIND TRIAL
TABULATE: T
    AT INTERVAL    .500000000
PLCT: X
    AGAINST: T
PLCT: Y
    AGAINST: T
PLOT: ALPHA
    AGAINST: T    AT INTERVAL    .250C00000CO

END CALCULATICN WHEN M .LE. 198.000

THREE CEGREE CRCSSWIND TRIAL
```

T	X	Y	VCG	V	MDOT
.C	.0	.0	2188.7	2189.5	-.21654
.50000000	1094.3	.99244D-03	2188.7	2189.5	-.21655
1.0000000	2188.7	.35210D-02	2188.7	2189.5	-.21654
1.5000000	3483.0	.64466D-02	2188.7	2189.5	-.21654
2.0000000	4377.3	.84628D-02	2188.7	2189.5	-.21654
2.5000000	5471.6	.86893D-02	2188.7	2189.5	-.21654
3.0000000	6566.0	.70662D-02	2188.7	2189.5	-.21654
3.5000000	7660.3	.43726D-02	2188.7	2189.5	-.21654
4.0000000	8154.7	.18644D-02	2188.7	2189.5	-.21655
4.5000000	9849.0	.69992D-03	2188.7	2189.5	-.21654
5.0000000	1094.3	.14154D-02	2188.7	2189.5	-.21653
5.5000000	1203.8	.36885D-02	2188.7	2189.5	-.21655
6.0000000	1313.2	.64935D-02	2188.7	2189.5	-.21655
6.5000000	1422.6	.85744D-02	2188.7	2189.5	-.21654
7.0000000	1532.1	.90176D-02	2188.7	2189.5	-.21654
7.5000000	1641.5	.76630D-02	2188.7	2189.5	-.21654
8.0000000	17509.	.51689D-02	2188.7	2189.5	-.21654
8.5000000	18604.	.27039D-02	2188.7	2189.5	-.21654
9.0000	19698.	.14109D-02	2188.7	2189.5	-.21654
9.500	2C792.	.18876D-02	2188.7	2189.5	-.21654

MDOT	V	VCG	Y	X	T
-.21653	2.2189.5	.2188.7	.97013D-02	73320.	31.500
-.21654	2.2189.5	.2188.7	-.10714D-01	74415.	32.000
-.21653	2.2189.5	.2188.7	-.10378D-02	75509.	32.500
-.21654	2.2189.5	.2188.7	.88866D-02	76603.	33.000
-.21654	2.2189.5	.2188.7	.69627D-02	77698.	33.500
-.21653	2.2189.5	.2188.7	.55195D-02	78792.	34.000
-.21654	2.2189.5	.2188.7	.52393D-02	79886.	34.500
-.21654	2.2189.5	.2188.7	.62613D-02	80981.	35.000
-.21653	2.2189.5	.2188.7	.81231D-02	82075.	35.500
-.21654	2.2189.5	.2188.7	.99824D-02	83169.	36.000
-.21654	2.2189.5	.2188.7	.11005D-01	84264.	36.500
-.21653	2.2189.5	.2188.7	.10752D-01	85358.	37.000
-.21654	2.2189.5	.2188.7	.93782D-02	86452.	37.500
-.21654	2.2189.5	.2188.7	.75553D-02	87547.	38.000
-.21653	2.2189.5	.2188.7	.61471D-02	88641.	38.500
-.21654	2.2189.5	.2188.7	.58269D-02	89735.	39.000
-.21654	2.2189.5	.2188.7	.67516D-02	90830.	39.500
-.21653	2.2189.5	.2188.7	.85039D-02	91924.	40.000
-.21654	2.2189.5	.2188.7	.11306D-01	93018.	40.500
-.21654	2.2189.5	.2188.7	.11116D-01	94113.	41.000
-.21653	2.2189.5	.2188.7	.98456D-02	95207.	41.500
-.21654	2.2189.5	.2188.7	.84171D-02	96301.	42.000
-.21654	2.2189.5	.2188.7	.64131D-02	97396.	42.500
-.21653	2.2189.5	.2188.7	.72580D-02	98490.	43.000
-.21654	2.2189.5	.2188.7	.89099D-02	99584.	43.500
-.21654	2.2189.5	.2188.7	.10619D-01	.10068D+06	44.000
-.21653	2.2189.5	.2188.7	.11618D-01	.10177D+06	44.500
-.21654	2.2189.5	.2188.7	.11474D-01	.10287D+06	45.000
-.21654	2.2189.5	.2188.7	.10293D-01	.10396D+06	45.500
-.21653	2.2189.5	.2188.7	.86544D-02	.10506D+06	46.000
-.21654	2.2189.5	.2188.7	.73472D-02	.10615D+06	46.500
-.21654	2.2189.5	.2188.7	.77771D-02	.10724D+06	47.000
-.21653	2.2189.5	.2188.7	.93383D-02	.10834D+06	47.500
-.21654	2.2189.5	.2188.7	.10971D-01	.10943D+06	48.000
-.21654	2.2189.5	.2188.7	.11941D-01	.11053D+06	48.500
-.21653	2.2189.5	.2188.7	.11828D-01	.11162D+06	49.000
-.21654	2.2189.5	.2188.7	.10722D-01	.11381D+06	49.500
-.21654	2.2189.5	.2188.7	.91705D-02	.11491D+06	50.000
-.21653	2.2189.5	.2188.7	.79215D-02	.11600D+06	50.500
-.21654	2.2189.5	.2188.7	.75755D-02	.11709D+06	51.000
-.21654	2.2189.5	.2188.7	.83064D-02	.11928D+06	51.500
-.21653	2.2189.5	.2188.7	.97861D-02	.12038D+06	52.000
-.21654	2.2189.5	.2188.7	.11342D-01	.12147D+06	52.500
-.21653	2.2189.5	.2188.7	.12274D-01	.12257D+06	53.000
				.12366D+06	

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MDOT	V	VCG	Y	X	T
-.216E+53	2189.5	2188.7	.13597D-01	.226530D+06	103.50
-.216E+53	2189.5	2188.7	.13746D-01	.227620D+06	104.00
-.216E+53	2189.5	2188.7	.14444D-01	.228720D+06	104.50
-.216E+53	2189.5	2188.7	.15377D-01	.229810D+06	105.00
-.216E+53	2189.5	2188.7	.16123D-01	.232000D+06	105.50
-.216E+53	2189.5	2188.7	.16352D-01	.233090D+06	106.00
-.216E+53	2189.5	2188.7	.15987D-01	.234190D+06	106.50
-.216E+53	2189.5	2188.7	.15231D-01	.235280D+06	107.00
-.216E+53	2189.5	2188.7	.14474D-01	.237470D+06	107.50
-.216E+53	2189.5	2188.7	.14100D-01	.238570D+06	108.00
-.216E+53	2189.5	2188.7	.14308D-01	.239660D+06	108.50
-.216E+53	2189.5	2188.7	.15015D-01	.240750D+06	109.00
-.216E+53	2189.5	2188.7	.15903D-01	.441850D+06	109.50
-.216E+53	2189.5	2188.7	.16571D-01	.442940D+06	110.00
-.216E+53	2189.5	2188.7	.16726D-01	.444040D+06	110.50
-.216E+53	2189.5	2188.7	.16125D-01	.445130D+06	111.00
-.216E+53	2189.5	2188.7	.15590D-01	.446230D+06	111.50
-.216E+53	2189.5	2188.7	.14899D-01	.447320D+06	112.00
-.216E+53	2189.5	2188.7	.14607D-01	.448410D+06	112.50
-.216E+53	2189.5	2188.7	.14872D-01	.449510D+06	113.00
-.216E+53	2189.5	2188.7	.15860D-01	.450600D+06	113.50
-.216E+53	2189.5	2188.7	.16426D-01	.251700D+06	114.00
-.216E+53	2189.5	2188.7	.17014D-01	.252790D+06	114.50
-.216E+53	2189.5	2188.7	.17095D-01	.253890D+06	115.00
-.216E+53	2189.5	2188.7	.16662D-01	.254980D+06	115.50
-.216E+53	2189.5	2188.7	.15551D-01	.256070D+06	116.00
-.216E+53	2189.5	2188.7	.15330D-01	.257170D+06	116.50
-.216E+53	2189.5	2188.7	.15120D-01	.258260D+06	117.00
-.216E+53	2189.5	2188.7	.15440D-01	.259360D+06	117.50
-.216E+53	2189.5	2188.7	.16156D-01	.260450D+06	118.00
-.216E+53	2189.5	2188.7	.16544D-01	.261550D+06	118.50
-.216E+53	2189.5	2188.7	.17450D-01	.262640D+06	119.00
-.216E+53	2189.5	2188.7	.17460D-01	.263730D+06	119.50
-.216E+53	2189.5	2188.7	.16317D-01	.264830D+06	120.00
-.216E+53	2189.5	2188.7	.15768D-01	.265920D+06	120.50
-.216E+53	2189.5	2188.7	.15639D-01	.267020D+06	121.00
-.216E+53	2189.5	2188.7	.16011D-01	.268110D+06	121.50
-.216E+53	2189.5	2188.7	.16723D-01	.269210D+06	122.00
-.216E+53	2189.5	2188.7	.17455D-01	.270300D+06	122.50
-.216E+53	2189.5	2188.7	.17878D-01	.271400D+06	123.00
-.216E+53	2189.5	2188.7	.17819D-01	.272490D+06	123.50
-.216E+53	2189.5	2188.7	.17334D-01		124.00
					124.50

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FIGURE E-1 RANGE VS TIME

FIGUR E-2 DISPERSION (Y) VS TIME

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FIGURE E-3 ALPHA VS TIME

APPENDIX F-FIVE DEGREES OF FREEDOM RESULTS

VARIABLES & INITIAL CONDITIONS:
XDOT = 1723.564000
X = .0
YDOT = .0
Y = .0
ZDOT = 1733.564000
Z = .0
THEDOT = .0
TH = .0
DELDOT = .0
DE = .7853980000
M = 225.0000000
T = .0

CONSTANTS:
CMA = -2.308000000
A = .3491009000
DI = .6666670000
ADI = .2327300000
DI2 = .4444440000
CMT = 190.000000
ISP = 950.000000
G = 32.174000000
CDO = .2760000000
K = 1.000000000
R = .0

SPECIAL FUNCTIONS:
ROT = (2116.22*(1-(.0035662*Z/518.688))**5.256)/
(1716.5*(518.688-(.0035662*Z)))
RO = CDEIF(Z,2608S,ROT,.0012711)
VWXY = 0
VWXZ = 0
GA = ATAN((YDOT+VWXY)/(XDOT+VWXZ))
O = ATAN(ZDOT/(XDOT+VWXZ))
VCG = (XDOT**2+YDOT**2+ZDOT**2)**.5
V = ((XDOT+VWXZ)**2+(YDOT+VWXY)**2+ZDOT**2)**.5
AL = C-DE
BE = GA-TH
Q = (RO*V**2)/2
LY = .091*BE*G*A
L = .091*AL*G*A
DY = D*CCS(O)/COS(GA)
D = (-.1025*V/(2402.88*(518.688-(.0035662*Z)))**.5+.5015)
+.5*(.051*AL)*SIN(AL)*G*A

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```
DRAG = D/COS(GA)
C = CDEIF(M,158,1,R)
DELM = 225-M
I = (18.8-.0423*DELM)*32.2
MDOT = (1-C)*CRAG/(-ISP)

DERIVATIVES:
D(XDCT/D(T) ) = =
D(X /D(T ) = (L*SIN(O)-C*C*COS(O)+LY*SIN(GA)-C*DY*COS(GA))/M
D(X /D(T ) = XDOT

D(YDCT /C(T ) = =
D(Y /D(T ) = (LY*CCS(GA)+C*DY*SIN(GA))/M
D(Y /D(T ) = YDCT

D(ZDCT /D(T ) = =
D(Z /C(T ) = (L*CCS(O)+C*D*SIN(O)-M*G)/M
D(Z /C(T ) = ZDOT

D(THECOT /C(T ) = =
D(TH /D(T ) = (CMA*C*ACI*(TI-GA)-((CMT*Q*ADI*DI*THECOT)/(V*2)))/I
D(TH /D(T ) = THEDCT

D(DELDCT/D(T ) = =
D(DE /D(T ) = (CMA*C*ACI*(DE-O)-((CMT*Q*ADI*DI*DELDCT)/(V*2)))/I
D(DE /D(T ) = CELDOT

D(M /D(T ) = =
D(M /D(T ) = MDCT

OUTPUTS:
TITLE:FIVE CEGREE
TABULATE: T          X           Y           Z         MDOT      VCG      M
AT INTERVAL  Z     .5000000000
PLCT: X
AGAINST: T
PLOT: AL      EE
AGAINST: T
PLCT: Y
AGAINST: T          AT INTERVAL     .2500000000

END CALCULATICN WHEN MCUT .GE. .0
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FIVE DEGREE

T	X	Y	Z	MDOT	VCG
.0	866.78	0.	862.76	-72555.5	2451.9
.5000	1733.6	0.	1717.5	-70183.4	2440.3
1.0000	2607.1	0.	2564.1	-67894.6	2429.0
1.5000	3467.5	0.	3402.8	-65666.6	2417.7
2.0000	4333.7	0.	4233.4	-63556.1	2406.6
2.5000	5207.5	0.	5055.9	-61501.9	2395.4
3.0000	6067.5	0.	5870.4	-59519.7	2384.4
3.5000	6934.2	0.	6676.9	-57607.3	2373.3
4.0000	7801.0	0.	7475.3	-55763.3	2362.4
4.5000	8667.8	0.	8265.6	-53984.4	2351.5
5.0000	9534.6	0.	9046.00	-52267.1	2340.6
5.5000	10401.	0.	9822.2	-50612.5	2329.9
6.0000	11268.	0.	10568.	-49015.1	2319.1
6.5000	12135.	0.	11347.	-47474.4	2308.5
7.0000	13002.	0.	12097.	-45988.9	2297.4
7.5000	13869.	0.	12839.	-44555.5	2287.5
8.0000	14735.	0.	13573.	-43172.2	2276.5
8.5000	15602.	0.	14299.	-41838.1	2266.2
9.0000	16469.	0.	15017.	-40551.3	2256.6
9.5000	17336.	0.	15727.	-39310.0	2245.6
10.0000	18202.	0.	16429.	-38113.7	2235.7
10.500	19069.	0.	17163.	-36957.2	2225.6
11.000	19936.	0.	17808.	-35843.3	2215.6
11.500	20808.	0.	18466.	-34769.2	2205.6
12.000	21670.	0.	19156.	-33732.2	2195.7
12.500	22536.	0.	19818.	-32732.0	2185.7
13.000	23403.	0.	20471.	-31767.6	2176.1
13.500	24270.	0.	21117.	-30836.8	2166.4
14.000	25136.	0.	21754.	-29938.6	2156.6
14.500	26003.	0.	22384.	-29072.7	2147.2
15.000	26870.	0.	23005.	-28237.1	2137.5
15.500	27737.	0.	23619.	-27431.1	2128.4
16.000	28604.	0.	24224.	-26653.3	2119.1
16.500	29471.	0.	24821.	-25903.0	2109.5
17.000	30337.	0.	25411.	-25180.0	2100.8
17.500	31204.	0.	25992.	-24482.9	2091.7
18.000	32071.	0.	26565.	-23809.0	2082.8
18.500	32938.	0.	27130.	-23159.3	2073.1
19.000	33804.	0.	27687.	-22533.2	2065.1
19.500	34671.	0.	28236.	-21928.3	2056.4
20.000	35538.	0.	28777.	-21345.3	2047.8
20.500	36405.	0.	29310.	-20782.5	2039.9
21.000	37272.	0.	29835.	-20240.7	2030.9
21.500	38138.	0.	30352.	-19717.3	2022.5
22.00	38138.	0.	30352.	-19213.	2014.3

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Data table (printed sideways). Columns, left to right: T, X, Y, Z, MDOT, VCG.

T	X	Y	Z	MDOT	VCG
45.50	78877.	0.	45573.	-2207.5	1754.4
46.00	79744.	0.	45704.	-2202.5	1752.0
46.50	80611.	0.	45826.	-2197.7	1745.7
47.00	81477.	0.	45941.	-2193.3	1747.7
47.50	82344.	0.	46048.	-2189.2	1745.9
48.00	83211.	0.	46146.	-2185.4	1743.2
48.50	84078.	0.	46237.	-2181.9	1742.2
49.00	84945.	0.	46320.	-2178.7	1740.7
49.50	85811.	0.	46354.	-2175.8	1739.3
50.00	86678.	0.	46461.	-2173.3	1738.1
50.50	87545.	0.	46519.	-2171.0	1737.0
51.00	88412.	0.	46569.	-2169.1	1736.3
51.50	89278.	0.	46612.	-2167.4	1735.3
52.00	90145.	0.	46646.	-2166.1	1734.6
52.50	91012.	0.	46672.	-2165.1	1734.1
53.00	91879.	0.	46690.	-2164.4	1733.6
53.50	92746.	0.	46700.	-2164.0	1733.6
54.00	93612.	0.	46703.	-2164.1	1733.7
54.50	94479.	0.	46697.	-2164.7	1733.9
55.00	95346.	0.	46663.	-2165.5	1734.3
55.50	96213.	0.	46661.	-2166.7	1734.9
56.00	97079.	0.	46631.	-2168.2	1735.4
56.50	97946.	0.	46552.	-2169.9	1736.1
57.00	98813.	0.	46546.	-2172.0	1737.0
57.50	99680.	0.	46452.	-2174.4	1738.1
58.00	.100550D+06	0.	46420.	-2177.2	1739.5
58.50	.101410D+06	0.	46360.	-2180.2	1741.4
59.00	.102280D+06	0.	46281.	-2183.5	1743.0
59.50	.103150D+06	0.	46195.	-2187.2	1744.7
60.00	.104010D+06	0.	46100.	-2191.1	1746.6
60.50	.104880D+06	0.	45958.	-2195.4	1748.6
61.00	.105750D+06	0.	45867.	-2200.0	1751.0
61.50	.106610D+06	0.	45769.	-2204.8	1753.1
62.00	.107480D+06	0.	45642.	-2210.0	1755.6
62.50	.108350D+06	0.	45508.	-2215.5	1758.2
63.00	.109210D+06	0.	45365.	-2221.3	1761.0
63.50	.110080D+06	0.	45214.	-2227.4	1763.9
64.00	.110950D+06	0.	45056.	-2233.9	1766.5
64.50	.111810D+06	0.	44889.	-2240.6	1770.4
65.00	.112680D+06	0.	44714.	-2247.6	1773.9
65.50	.113550D+06	0.	44531.	-2254.9	1776.9
66.00	.114420D+06	0.	44340.	-2262.6	1780.5
66.50	.115280D+06	0.	44141.	-2270.5	1784.2
67.00	.116150D+06	0.	43934.	-2278.8	1788.2
67.50	.117020D+06	0.	43719.	-2287.3	1792.1
68.00	.117880D+06	0.	43456.		

1796.2	-2.2962	43265.	0.	1.18750D+06	6E9.000
1800.5	-2.3053	43025.	0.	1.19620D+06	6E9.500
1804.5	-2.3148	42778.	0.	1.20480D+06	7C0.000
1809.5	-2.3245	42524.	0.	1.21350D+06	7C0.500
1814.2	-2.3346	42260.	0.	1.22220D+06	7C1.000
1819.0	-2.3449	41988.	0.	1.23080D+06	7C1.500
1823.9	-2.3556	41709.	0.	1.23950D+06	7C2.000
1829.0	-2.3665	41421.	0.	1.24820D+06	7C2.500
1834.1	-2.3777	41126.	0.	1.25680D+06	7C3.000
1839.5	-2.3893	40822.	0.	1.26550D+06	7C3.500
1844.5	-2.4011	40511.	0.	1.27420D+06	7C4.000
1850.5	-2.4132	40191.	0.	1.28280D+06	7C4.500
1856.2	-2.4257	39863.	0.	1.29150D+06	7C5.000
1862.0	-2.4384	39528.	0.	1.30020D+06	7C5.500
1867.9	-2.4514	39184.	0.	1.30880D+06	7C6.000
1874.0	-2.4647	38822.	0.	1.31750D+06	7C6.500
1880.1	-2.4783	38472.	0.	1.32620D+06	7C7.000
1886.4	-2.4922	38104.	0.	1.33480D+06	7C7.500
1892.8	-2.5063	37728.	0.	1.34350D+06	7C8.000
1899.3	-2.5208	37344.	0.	1.35220D+06	7C8.500
1906.7	-2.5356	36952.	0.	1.36080D+06	7C9.000
1912.5	-2.5509	36552.	0.	1.36950D+06	7C9.500
1919.5	-2.5665	36144.	0.	1.37820D+06	7D0.000
1926.6	-1.4545	35728.	0.	1.38680D+06	7D0.500
1933.0	-1.4877	35304.	0.	1.39550D+06	7D1.000
1940.8	-1.5224	34872.	0.	1.40420D+06	7D1.500
1948.4	-1.5578	34431.	0.	1.41290D+06	7D2.000
1955.9	-1.5949	33983.	0.	1.42150D+06	7D2.500
1962.5	-1.6333	33527.	0.	1.43020D+06	7D3.000
1970.5	-1.6731	33062.	0.	1.43890D+06	7D3.500
1978.9	-1.7145	32590.	0.	1.44750D+06	7D4.000
1986.9	-1.7573	32109.	0.	1.45620D+06	7D4.500
1993.9	-1.8017	31621.	0.	1.46490D+06	7D5.000
2001.0	-1.8478	31124.	0.	1.47350D+06	7D5.500
2010.6	-1.8956	30619.	0.	1.48220D+06	7D6.000
2018.2	-1.9451	30107.	0.	1.49090D+06	7D6.500
2034.9	-1.9964	29586.	0.	1.49950D+06	7D7.000
2043.5	-2.0497	29057.	0.	1.50820D+06	7D7.500
2051.5	-2.1049	28520.	0.	1.51690D+06	7D8.000
2060.6	-2.1621	27975.	0.	1.52550D+06	7D8.500
2069.3	-2.2214	27423.	0.	1.53420D+06	7D9.000
2078.7	-2.2829	26862.	0.	1.54290D+06	7D9.500
2087.0	-2.3466	26293.	0.	1.55150D+06	7E0.000
2096.0	-2.4127	25716.	0.	1.56020D+06	7E0.500
2105.1	-2.4812	25131.	0.	1.56890D+06	7E1.000
2114.3	-2.5522	24537.	0.	1.57750D+06	7E1.500
2123.5	-2.6258	23936.	0.	1.58620D+06	7E2.000
	-2.7021	23327.	0.	1.59490D+06	

```
3.40E-03+     .
 ::.=AL   I
 +++=EE   I
         I
         I
         I
         I
         I
-1.76E-04+I++++++++++++++++++++++
         I
         I
         I
         I
         I
         I
         I
-3.75E-03+I
        T=.0===+====+====33.7===+====+====67.3===+====+====101.==
```

VWXY NOW IS 60

FIVE DEGREE

T	X	Y	Z	MDOT	VCG
.0	.0	.0	.0	-.72624	2451.6
.50000	866.78	-.37852D-02	866.76	-.70250	2440.3
1.0000	1733.6	-.10021D-01	1717.5	-.67959	2429.0
1.50000	2607.3	-.10760D-01	2564.1	-.65749	2417.7
2.00000	3467.1	-.55895D-02	3402.8	-.63618	2406.6
2.50000	4333.5	.13485D-02	4233.4	-.61561	2395.4
3.00000	5200.7	.32435D-02	5050.9	-.59577	2384.4
3.50000	6067.5	.90122D-02	5870.4	-.57664	2373.3
4.00000	6934.3	-.12433D-01	6676.9	-.55818	2362.4
4.50000	7801.0	-.97417D-02	7475.3	-.54037	2351.5
5.00000	8667.8	-.46356D-02	8265.6	-.52319	2340.6
5.5000	9534.6	-.24152D-02	9044.0	-.50662	2329.9
6.0000	10401.	-.54170D-02	9822.2	-.49064	2319.1
6.5000	11268.	-.10611D-01	10588.	-.47522	2308.5
7.0000	12135.	-.13254D-01	11347.	-.46035	2297.9

T	X	Y	Z	MCOT	VCG
31.500	54607.	.16556D-01	38645.	-.24749	1877.2
32.000	55474.	.20072D-01	39001.	-.24615	1871.1
32.500	56341.	.22266D-01	39349.	-.24483	1865.1
33.000	57208.	.21999D-01	39689.	-.24354	1855.2
33.500	58074.	.20020D-01	40021.	-.24228	1853.4
34.000	58941.	.16876D-01	40345.	-.24106	1847.8
34.500	59808.	.14340D-01	40660.	-.23986	1842.3
35.000	60675.	.13662D-01	40968.	-.23869	1836.7
35.500	61541.	.15197D-01	41268.	-.23755	1831.7
36.000	62408.	.18265D-01	41559.	-.23644	1826.5
36.500	63275.	.21495D-01	41843.	-.23536	1821.5
37.000	64142.	.23475D-01	42119.	-.23431	1816.6
37.500	65009.	.23394D-01	42386.	-.23328	1811.3
38.000	65875.	.21398D-01	42646.	-.23229	1807.3
38.500	66742.	.18496D-01	42897.	-.23133	1802.8
39.000	67609.	.16080D-01	43141.	-.23040	1798.5
39.500	68476.	.15296D-01	43376.	-.22950	1794.2
40.000	69342.	.15536D-01	43603.	-.22863	1790.2
40.500	70209.	.19284D-01	43823.	-.22779	1786.2
41.000	71076.	.22365D-01	44034.	-.22698	1782.4
41.500	71943.	.24485D-01	44237.	-.22620	1776.4
42.000	72810.	.24797D-01	44432.	-.22545	1775.2
42.500	73676.	.20651D-01	44619.	-.22473	1771.8
43.000	74543.	.18185D-01	44798.	-.22408	1768.6
43.500	75410.	.16999D-01	44969.	-.22338	1762.5
44.000	76277.	.17654D-01	45132.	-.22276	1759.6
44.500	77143.	.19006D-01	45267.	-.22216	1757.0
45.000	78010.	.22828D-01	45434.	-.22160	1754.4
45.500	78877.	.25225D-01	45573.	-.22106	1752.7
46.000	79744.	.26145D-01	45704.	-.22056	1749.7
46.500	80611.	.25286D-01	45826.	-.22008	1747.6
47.000	81477.	.23108D-01	45941.	-.21964	1745.7
47.500	82344.	.20623D-01	46048.	-.21923	1743.9
48.000	83211.	.18958D-01	46146.	-.21885	1742.7
48.500	84078.	.18872D-01	46237.	-.21850	1740.7
49.000	84945.	.20447D-01	46320.	-.21818	1739.3
49.500	85811.	.23058D-01	46394.	-.21783	1738.1
50.000	86678.	.25655D-01	46461.	-.21763	1737.0
50.500	87545.	.27209D-01	46519.	-.21741	1736.0
51.000	88412.	.27145D-01	46569.	-.21721	1735.3
51.500	89278.	.25580D-01	46612.	-.21705	1734.3
52.000	90145.	.23258D-01	46646.	-.21692	1734.1
52.500	91012.	.21233D-01	46672.	-.21681	1733.8
53.000	91879.	.20420D-01	46690.	-.21674	1733.6
53.500	92746.	.21210D-01	46700.	-.21670	1733.6
54.000	93612.		46703.		

FIGURE F-1 RANGE AND HEIGHT VS TIME

125

FIGURE F-2 ALPHA AND BETA VS TIME

126

4.C8E-C2+
..=Y

2.C4E-02+

.0
T

=.0======+=======23.6========+=======67.2=======+========101.===
FIGURE F-3 DISPERSION VS TIME

```
C***********************************************************************
C*                                                                     *
C*              APPENDIX G  HTRAJ BRL PROGRAM                           *
C*                                                                     *
C***********************************************************************
      DIMENSION LE(1), C(7), QE(1), HSX(1), PY(2), DPY(2), Y(16), UV(16)
     1  QC(16), CMMT(162), CMHGT(27), T45(10), EURN(16)
     2  PR(11), CTTP(48), CT1(8), CT2(4), CT3(6), CT4(7), CT5(4)
     3  CT6(5), CT7(7), CT8(5), CT9(6), CT10(4), CT11(10), CT12(5)
      COMMON LE, RN, RK, R2TEM, RNE, L, E, LL, GO, TBMST, TEST, IST, PE,
     1  AE, MTBST, MDI, DELTB, DETFF, XIDEL, XIMAX, IH2B, IH3E, IFUB,
     2  CX1, LZ1, ETB, EPB, EUB, EX1, SRIST, TSRBST, RS, QE, IH2, TDI,
     3  IH3, TF, EC, SL, UO, SPN, IX1, IX2, IU, AZU, EU, TBM, TL, TSRI,
     4  TCE, TE, E6, TCF, PTB, PTFF, AZD, MTBP, MF, MTB, ISP, TSRI,
     5  TSRE, TSCF, CGTBP, CGTBM, ATBM, ATE, ETBM, LAT, A4, IMCB, UMCB,
     6  PHMCB, THMCB, TI, XI, YI, ZI, WSX, WS2, WEX, WBZ, DENSF, PRESF,
     7  TEMPF, SL6D
      COMMON ATM(700), IMZ1, IMZ2, ATM, J2, IDGREE(1), IROT,
     1  IREDUC, ITWT, IUPLEG, IUNIT, ISPRT, IRSET, ICURE, ISTIM, ISCCLT,
     2  I3DELF, I3DP, ISAVE6, ITONQE, IXIAYI, I5DIG, IX2N, IUN, LAM(3),
     3  B, A, ILI, SINCE, COSCE, DSQ, IKL, GOFSC, XGUT(1), YGUT, ZGUT, TOF,
     4  AA, ILI, AZUI, EUI, QEOUT, TEMP, DENSN, WX, WZ, CON, IDRN,
     5  CENS, FAR, VAS, PFI, PP1, PPFI, PPF2, ETB, CONS2, CONS, IYP,
     6  D44, GCRS, II, I2, I3, I4, I5, I6, I7, I8, I9, NEX, ILSA, IYP,
     7  IEPC, GSQ, RITB, R2TBSQ, RETE, RKI2, RK2, RNESQ2, RITE, TRCONS,
     8  LCNP, TST, IT, ITT, IFERR, ICI, HDX, CTS, TO, TI, I2, T2,
     9  T4, IRS, TALPH, THETA, ALPE, ALPQ, ALFQ2, ALPQ3, CODE, D22,
     A  IFIRST, ICC3, J7, PDTO, PMTOF, TJ(290), UA, VP, ICODE, ICCT1,
     B  ICOTZ, ICCT2, PHI, I6DP, R3, ALPHA, WT, VI, V2, V3, TSIAH, KEB,
     C  KM, KKL, KT, XDX, KH, DKDB, MACH, ISUN, SINLAT, COSLAT,
     D  SINAZ, COSAZ, SINC, CCSD, DEL
      COMMON /ERR/ IER
      COMMON /ECH/ REARIT, GC, AMTOMS, PQ, AMTOF, FTCM, ANTUM, KILD,
     1  DTOP, THCFHI, AMTCIN, AMTOKN, AMTCMH, FTG+2, CVDTCR, CVMTCR, RSG,
     2  HA(23), TM(23), ALM(22), HEAD(165)
      EXTERNAL COA, DER
      REAL LE, LL, IST, DI, IH2B, IH3B, IX3, IH2, IX3, IX1, IX2, IU, MF,
     1  MTE, ISP, LAT, LAM, MTBM, MTBST, ICL, IX2N, IUN, LZ1, KDB, KM,
     2  KL, KF, KF, MACH, ITO, IUEL, IUAZ, IARV, IARH
      DATA PI1 /.261759367/
      DATA CT1 /4HG DE, 4HG TH, 4HROUG, 4HH EN, 4HTIRE, 4HTRAJ, 4HECTO,
     14HRY /
      DATA CT2 /4H ROT, 4HATIN, 4HG EA, 4HRTH /
      DATA CT3 /4H RED, 4HUCTI, 4HON  , 4HTRAJ, 4HELTC, 4HRY  /
      DATA CT4 /4H INP, 4HUT  , 4HPIN , 4HINST, 4HEAC , 4HOF T, 4HWIST/
      DATA CT5 /4H HIT, 4H ON , 4HUP L, 4HHEG /
      DATA CT6 /4H TER, 4HMINA, 4HTE O, 4HN TI, 4HME /
      DATA CT7 /4H PRI, 4HNT V, 4HELOC, 4HITY , 4HHOR L, 4HINE /
```

```fortran
      DATA CTE /4H SUM,4HMARY,4H HAR,4HD CU,4HTPUT/
      DATA CT9 /4H 3 D,4HEG D,4HLRIN,4HG BU,4HRNIN,4HG  /
      DATA CT10 /4H ITE,4HRATE,4H UN ,4HGE  /
   14HEAD ,4H-OF T,4HHERM ,4HX2 /
      DATA CT12 /4H 5 C,4HIGIT,4H TIM,4HE PR,4HINT /
      INTEGER SYM(19)
      DATA SYM /2H10, 2HPC, 2HIM, 2HIP, 2HTS, 2HAA, 2HTC, 2HIB,
     12HRJ, 2HVC, 2HMC, 2HAC, 2HRI, 2HRT, 2HRC, 2HRS, 2HMM, 2HNA, 2HSS/
      DATA CMTGT /0.88976, 1148.29156, 2460.62592, 4101.04987,
     15741.46982, 7381.88976, 9022.30971, 10662.72966, 12303.14961,
     213543.59955, 15583.98950, 18044.61942, 21325.45932, 24606.29921,
     327887.17928, 31167.97900, 34446.81850, 37725.65879, 41010.49865,
     444291.33858, 47572.17848, 50853.01837, 54133.85827, 57414.69816,
     560695.53806, 63976.37755/
      ASSIGN 167 TO IER
C     NEXT TWC STATEMENTS ARE MINE
      INTEGER R(19),CODE,SS,TYPE,DUMMY
      DATA DUMMY/1H /
      DO 1 I=1,3833
    1 LE(I)=C.
      JBURN=1
C     START WITH AEROPACK END WITH O IN CCL 8C
    2 CALL AEFCH
      IF (IRSET.NE.O) GO TO 4
      DO 3 I=1,85C
    3 LE(I)=C.
      IST=955.55
      ISP=995.99
      TBM=.55555
      ISLN=0
      J2=1
      TSRE=.55555
      DENSF=1.
      PRESF=1.
      TEMPF=1.
      CMETM=C.
C     CONTROL CARD OPTIONS SET FOR 6DEG,SPIN,F1,STGF TRAJ ON T,FLAT TRAJ
    4 REAC (5,159) R,CODE,SS,TYPE
      IDGREE (1)=1
      IRCT=R(2)
      IREDUC=F(3)
      ITWT=1
      IUFLEG=F(5)
      IUNIT=1
      ISPRT=1
      IRSET=1
```

```
      ICLRE=1
      ISTIM=1
      ISCCUT=F(11)
      I3CBUR=R(12)
      I3CP=R(13)
      ISAVE6=F(14)
      ITONQE=R(15)
      IXIAY=R(16)
      I5CEG=R(17)
      EXTRA=R(18)
C3000 IF (EOF(5)) 3000,3001
C     STOP
    1 CECCODE (40,170,R(1),)IDGREE,IROT,IREDUC,ITM1,IUPLEG,IUNIT,ISPRT,IR
     1SET,ICLFE,ISTIM,ISCCUT,I3DBUR,I3CP,ISAVE6,ITONQE,IXIAY1,I5DIG
C     WRITE (6,220)
      READ (5,210)C,CCDE,SS,TYPE
      WRITE (6,210)C,CCDE,SS,TYPE
      IF (TYPE.EQ.SYM(1)) GO TO 8
      IF (TYPE.EQ.SYM(2)) GO TO 14
      IF (TYPE.EQ.SYM(3)) GO TO 16
      IF (TYPE.EQ.SYM(4)) GO TO 17
      IF (TYPE.EQ.SYM(5)) GO TO 18
      IF (TYPE.EQ.SYM(6)) GO TO 19
      IF (TYPE.EQ.SYM(7)) GO TO 20
      IF (TYPE.EQ.SYM(8)) GO TO 21
      IF (TYPE.EQ.SYM(9)) GO TO 22
      IF (TYPE.EQ.SYM(10)) GO TO 23
      IF (TYPE.EQ.SYM(11)) GO TO 24
      IF (TYPE.EQ.SYM(12)) GO TO 25
      IF (TYPE.EQ.SYM(13)) GO TO 26
      IF (TYPE.EQ.SYM(14)) GO TO 27
      IF (TYPE.EQ.SYM(15)) GO TO 28
      IF (TYPE.EQ.SYM(16)) GO TO 29
      IF (TYPE.EQ.SYM(17)) GO TO 31
      IF (TYPE.EQ.SYM(18)) GO TO 2
      IF (TYPE.EQ.SYM(19)) GO TO 30
      WRITE (6,200) C,CODE,SS,TYPE
      STOP
    7 CECCODE (80,171,R(1),)C
    8 GO TO (6,14,16,17,18,19,20,21,22,23,24,25,26,27,28,29,31,2,30), I
      K=1
      J2=2
      CMETM=C.
      ICN=20
      GO TO 1C
C     THIS NEXT LCOP INVCLVES MET CARD LCCPS
    9 REAC (5,171) C,CCDEM,ID
```

```fortran
      IF (IC.NE.ICN) GC TC 13                          FDU01450
      ICN=ICN+10                                       FCU01460
10    C(2)=AMICMS*C(2)                                 HDU01470
      C(3)=AMICMS*C(3)                                 FDU01480
      L=K                                              FDU01490
      DO 11 I=1,7                                      FDU01500
      ATM(L)=C(I)                                      FDU01510
11    L=L+1                                            FDU01520
      IF (L.LE.693) GC TC 12                           FCU01530
      WRITE (6,172)                                    FCU01540
      STCP                                             HDU01550
12    K=K+7                                            FDU01560
      IF (C(1).GE.0.) GO TO 9                          FDU01570
      ATM(L-7)=ABS(ATM(L-7))                           HDU01580
      NATM=K-7                                         FCU01590
      GO TO 4                                          FCU01600
13    WRITE (6,172)                                    FDU01610
      STCP                                             FDU01620
14    MTEST=C(1)                                       HDU01630
      MTB=C(2)                                         FDU01640
      D=FTOM*C(3)                                      HDU01650
      CGTE=FTCM*C(4)                                   FDU01660
      ATB=FTCM2*C(5)                                   FCU01670
      BTEM=FTCM2*C(6)                                  FDU01680
      TWIST=C(7)                                       FDU01690
15    IF (SS.EQ.CLMMY ) GO TC 4                        FCU01700
      GO TO 4                                          HDU01710
16    LO=FTGM*C(1)                                     FCU01720
      CE(1)=C(2)                                       FDU01730
      AZC=C(3)                                         FDU01740
      BC=C(4)/ANTCM**2                                 FCU01750
      SL=C(5)                                          FCU01760
      IH2=C(6)                                         FCU01770
      IH3=C(7)                                         FDU01780
      GO TO 15                                         FCU01790
17    ITC=C(1)                                         FDU01800
      IX1=FTCM*C(2)                                    HDU01810
      IX2=FTCM**C(3)                                   FDU01820
      IX3=FTCM*C(4)                                    FCU01830
      IARV=C(5)                                        FDU01840
      IARH=C(6)                                        FDU01850
      GO TO 15                                         HDU01860
18    DEIFF=C(1)                                       HDU01870
      PTFF=C(2)                                        FCU01880
      XICEL=FICM*C(3)                                  HDU01890
      AZ=C(4)                                          FDU01900
      LAT=C(5)                                         FCU01910
      GO=FTCM*C(6)                                     FCU01920
```

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```
15      GO TO 15                                      FDU01530
        Q=C(1)                                        FDU01540
        TF=C(2)                                       FDU01550
        E=C(3)                                        FDU01560
        LL=FTGM*C(4)                                  FDU01570
        SL6C=C(5)                                     FDU01580
        GO TO 15                                      FDU01590
20      TI =C(1)                                      FDU02000
        XI O=FTC**C(2)                                FDU02010
        XIMAX=FTOM*C(3)                               FDU02020
        YI=FTCM*C(4)                                  FDU02030
        ZI=FTQM*C(5)                                  FDU02040
        EX1=FTCM*C(6)                                 FDU02050
        EZ1=FTC**C(7)                                 FDU02060
        GO TO 15                                      FDU02070
21      TM CEI=FTCM*C(1)                              FDU02080
        UMCB=FTCM*C(2)                                FDU02090
        FHMCB=CTGM*C(3)                               FDU02100
        THMCB=CTCM*C(4)                               FDU02110
        EUB=FTCM*C(5)                                 FDU02120
        EPE=DTC**C(6)                                 FDU02130
        ETB=DTC**C(7)                                 FDU02140
        GO TO 15                                      FDU02150
22      R2 TEM=FTCM*C(1)                              FDU02160
        RNE=FTC**C(2)                                 FDU02170
        AE=FTCM*C(3)                                  FDU02180
        PE=C(4)/FTGM2                                 FDU02190
        RN=FTGM*C(5)                                  FDU02200
        RK=FTOM*C(6)                                  FDU02210
        GO TO 15                                      FDU02220
23      QE (1)=C(1)                                   FDU02230
        IX2=FTC**C(2)                                 FDU02240
        IU=FTCM*C(3)                                  FDU02250
        AZU=C(4)                                      FDU02260
        EU=C(5)                                       FDU02270
        XIMAX=FTGM*C(6)                               FDU02280
        XI=XIMAX                                      FDU02290
        AZC=C(7)                                      FDU02310
        GO TO 15                                      FDU02320
24      WSX(1)=AMTCMS*C(1)                            FDU02330
        WSZ=AMTCMS*C(2)                               FDU02340
        WBX=AMTCMS*C(3)                               FDU02350
        WBZ=AMTCMS*C(4)                               FDU02360
        DENSF=C(5)                                    FDU02370
        PRESF=C(6)                                    FDU02380
        TEMPF=C(7)                                    FDU02390
        CMETM=C.                                      FDU02400
        J2=1
```

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```
         GO TO 15
   25    IH2E=C(1)/DTOM
         IH3B=C(2)/DTOM
         TFUB=C(3)/FTOM
         CX1=(C(4)/ANTOM**2)/FTCM
         LZ1=C(5)/FTCM
         GO TO 15
   26    ISI=C(1)
         ISP=C(2)
         MF=C(3)
         LE(1)=FTCM*C(4)
         CGTBM=FTCM*C(5)
         ATEM=FTC(*2*C(6)
         MDI=C(7)
         GO TO 15
   27    TBWST=C(1)
         TBM=C(2)
         TBST=C(3)
         TB=C(4)
         TL=C(5)
         TDI=C(6)
         TEE=C(7)
         GO TO 15
   28    DELTB=C(1)
         PTB=C(2)
         TCE=C(3)
         TCFF=C(4)
         GO TO 15
   29    TSRIST=C(1)
         TSRI=C(2)
         TSREST=C(3)
         TSRB=C(4)
         RS=FTCM*C(5)
         TS CF=C(6)
         GU TO 15
   30    ALCNG=C(1)
         RACS=C(2)*1000.
         ADCS=C(3)*1000.
         HACA=C(4)*1000.
         TOCAY=C(5)*1000.
         ISUN=1
         GO TO 15
   31    HGTMDP=C(1)/FTOM
         CMETM=1.
         COCEM=CCE
         DO 32 I=1,162,6
         K=I+4
         READ (5,171) (CMMT(JJ),J=I,K)
```

```
+0004 2410
+0004 2420
+0004 2430
+0004 2440
+0004 2450
+0004 2460
+0004 2470
+0004 2480
+0004 2490
+0004 2500
+0004 2510
+0004 2520
+0004 2530
+0004 2540
+0004 2550
+0004 2560
+0004 2570
+0004 2580
+0004 2590
+0004 2600
+0004 2610
+0004 2620
+0004 2630
+0004 2640
+0004 2650
+0004 2660
+0004 2670
+0004 2680
+0004 2690
+0004 2700
+0004 2710
+0004 2720
+0004 2730
+0004 2740
+0004 2750
+0004 2760
+0004 2770
+0004 2780
+0004 2790
+0004 2800
+0004 2810
+0004 2820
+0004 2830
+0004 2840
+0004 2850
+0004 2860
+0004 2870
+0004 2880
```

```
      IF (CMMT(L).EQ.0..AND.CMMT(I+3).EQ.C..AND.CMMT(I+4).EQ.0.) GO TC
13    L=CMMT(L)+1.
      IF (L.NE.I+1/6) GO TO 13
      CMMT(I)=HGTMDP+CMHGT(L)
      CMMT(I+5)=.1*CMMT(I+3)
36    CMMT(I+3)=348.3676356*CMMT(I+4)/CMMT(I+5)
33    CMMT(I+5)=CMMT(I+5)-273.15
      NMET=6*L
      J2=2
      GO TO 4
34    IF (Q.EG.0.) Q=1.2
      IF (BC.EG.0.) BC=MTBST/C**2
      IF (SL.LE.EG.0.) SL6D=1.
      IF (SL.EG.0.) SL=1.
      GORSG=GC*RSG
      CSG=Q**2
      J9=2
      MTBM=0.
      IF (MF.NE.0.) MTBM=MTB+MF+MDI
      TMCB=TACBI
      IF (TMCB.EQ.0.) TMCB=TE6
      IF (IUFLEG.NE.0) J9=1
      IYP=1
      IF (ICLFE.NE.0) IYP=0
      IF (IUNIT.EC.0) GO TO 35
      PMTCF=AMTGF
      FDTCM=1.
      GO TO 36
35    PMTCF=1.
      FDTCM=LTCM
36    ITE=0
      IF (IRELUC.EQ.1) ITE=1
      IF (CMETN.EC.0.) GO TC 38
      J=1
      DO 37 I=1,NMET,6
      ATM(J)=CMMT(I)
      ATM(J+3)=CMMT(I)
      ATM(J+4)=CMMT(I+3)
      ATM(J+5)=CMMT(I+4)
      ATM(J+6)=CMMT(I+5)
      AZMHD=CVMTCR*(AZ-10.*CMMT(I+1))
      WS=.5144444444*CMMT(I+2)
      ATM(J+1)=-WS*CCS(AZMHD)
      ATM(J+2)=WS*SIN(AZMHD)
37    J=J+7
      NATM=J-1
38    SPN=TWIST
```

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```
      IF (ITWT.EQ.0) SPN=UO/(TWIST*D)
      Y(10)=TWCFHI*SPN
      IF (XIC.EQ.C.) XIO=XIDEL
      XI=XIO
      IF (XICEL.EC.0.) XI=XIMAX
      IF (IREDUC.EQ.1) TFN=-TF
      ICAP=3
      IF (IAR).EQ.0..AND.IARH.EQ.0.) GC TC 39
      IUEL=IAFV
      IUAZ=IAFH
      GO TO 4C
   39 IUEL=QE(1)
      IUAZ=AZC
   4C IF (MF.NE.0.) GO TO 41
      CGTEM=C(TE
      ATBM=ATB
   41 TALFH=0.
      ICl=11
      ICCTl=11
      ICCT2=12
      ICCT3=13
      ICCT4=14
      WRITE (6,197)
      I=1
      IF (ICCREE(1).EQ.0) GO TO 43
      DO 42 J=1,4
      CTP(I)=CTl(J)
   42 I=I+1
   43 IF (IRCT.EC.0) GC TC 45
      DO 44 J=1,4
      CTP(I)=CT2(J)
   44 I=I+1
   45 IF (IREDUC.EQ.0) GO TO 47
      CO 46 J=1,4
      CTP(I)=CT3(J)
   46 I=I+1
   47 IF (ITWT.EQ.0) GC TC 49
      DO 48 J=1,4
      CTP(I)=CT4(J)
   48 I=I+1
   49 IF (IUFLEG.EQ.0) GO TO 51
      CO 50 J=1,4
      CTP(I)=CT5(J)
   50 I=I+1
   51 IF (ISTIM.EC.0) GO TO 53
      DO 52 J=1,4
      CTP(I)=CT6(J)
   52 I=I+1
```

```
53  IF (ISFFT.EC.0) GO TO 55
    DO 54 J=1,4
    CTP(I)=CT7(J)
54  I=I+1
55  IF (ISCCLT.EQ.0) GC TC 57
    DO 56 J=1,4
    CTP(I)=CT8(J)
56  I=I+1
57  IF (I3CELR.EQ.0) GO TO 59
    DO 58 J=1,4
    CTP(I)=CT9(J)
58  I=I+1
59  IF (ITCAGE.EQ.0) GC TC 61
    DO 60 J=1,4
    CTF(I)=CT10(J)
60
61  I=I+1
    IF (IXIAYI.EQ.0) GC TO 63
    DO 62 J=1,4
    CTP(I)=CT11(J)
62  I=I+1
63  IF (I5CIG.EC.0) GO TC 65
    DO 64 J=1,4
    CTF(I)=CT12(J)
64  I=I+1
65  I=I-1
    WRITE (6,198) (CTP(J),J=1,I)
    ICOTT=C
    WRITE (6,178) CCDE
    WRITE (6,179)
    PR(1)=MIEST
    PR(2)=PTEM
    PR(3)=MJE
    PR(4)=MF
    PR(5)=ACI
    PR(6)=C/FTOM
    PR(7)=LE(1)/FTOM
    PR(8)=CCTBM/FTCM
    PR(9)=CCIB/FTOM
    PR(10)=ATBM/FTCM2
    PR(11)=AIB/FTOM2
    PR(12)=ETEM/FTOM2
    PR(13)=LL/FTOM
    WRITE (6,18C) (PR(I),I=1,13)
    IF (ITHT.EC.0) WRITE (6,181)
    IF (ITHT.EC.1) WRITE (6,177)
    PR(1)=CE(1)
    PR(2)=LC/FTCM
    PR(3)=AZ
```

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```
PR(4)=AZC                                          FDU04330
PR(5)=AZL                                          FDU04340
PR(6)=EL                                           HDU04350
PR(7)=IL/FTCM                                      FDU04360
PR(8)=IBIST                                        FDU04370
PR(9)=IT2                                          FDU04380
PR(10)=IH3                                         FDU04390
PR(11)=IUEL                                        FCU04400
PR(12)=JUAZ                                        HDU04410
PR(13)=E                                           FDU04420
WRITE (6,182) (PR(I),I=1,13)                       HDU04430
WRITE (6,183)                                      FDU04440
PR(1)=ISF                                          FCU04450
PR(2)=ISF                                          HDU04463
PR(3)=RZIBM/FTCM                                   FDU04470
PR(4)=RNE/FTOM                                      FDU04480
PR(5)=AE/FTCM2                                      HDU04490
PR(6)=PE*FTCM2                                      FDU04500
PR(7)=RN/FTCM                                       HDU04510
PR(8)=FK/FTCM                                       FDU04520
PR(9)=RACS                                          FCU04530
PR(10)=ACCS                                         FDU04540
PR(11)=ACA                                          FCU04550
PR(12)=TCDAY                                        FCU04560
WRITE (6,184) (PR(I),I=1,12)                       HDU04570
WRITE (6,185)                                      FDU04580
PR(1)=TEMST                                        FDU04590
PR(2)=TEM                                           FDU04600
PR(3)=TEST                                          FDU04610
PR(4)=TE                                            FDU04620
PR(5)=TL                                            FCU04630
PR(6)=TLI                                           FDU04640
PR(7)=TE6                                           FDU04650
PR(8)=TCRIST                                        HDU04660
PR(9)=TCRI                                          HDU04670
PR(10)=TSRBST                                       FCU04680
PR(11)=TSRB                                         FCU04690
PR(12)=FS/FTOM                                      FCU04700
PR(13)=TSCF                                         FDU04710
WRITE (6,186) (PR(I),I=1,13)                       FDU04720
WRITE (6,187)                                      HDU04730
PR(1)=CELTB                                         FDU04740
PR(2)=CLETFF                                        HDU04750
PR(3)=PIE                                           FDU04760
PR(4)=PTFF                                          FCU04770
PR(5)=TCE                                           FCU04780
PR(6)=TCFF                                          FCU04793
PR(7)=LAT                                           FCU04800
```

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```
PR(8)=ALCNG
PR(9)=BC*ANTOM**2
PR(10)=SL
PR(11)=SL60
PR(12)=G
PR(13)=TF
WRITE (6,186) (PR(I),I=1,13)
WRITE (6,185)
PR(1)=ITO
PR(2)=IX1/FTOM
PR(3)=IX2/FTOM
PR(4)=IX3/FTOM
PR(5)=TI
PR(6)=X10/FTOM
PR(7)=XIDEL/FTOM
PR(8)=XIMAX/FTOM
PR(9)=YI/FTCM
PR(10)=ZI/FTOM
PR(11)=EXL/FTOM
PR(12)=EZI/FTOM
PR(13)=GO/FTOM
WRITE (6,190) (PR(I),I=1,13)
WRITE (6,151)
PR(1)=TMCB
PR(2)=CACB/FTOM
PR(3)=PHMCB/DTOM
PR(4)=THMCB/DTOM
PR(11)=C
PR(5)=ELB/FTOM
PR(6)=ETE/CTOM
PR(7)=EFE/DTOM
PR(12)=LZ1*FTOM
PR(8)=IT2B*CTOM
PR(9)=IT3B*DTOM
PR(10)=TFUB*FTOM
PR(13)=C
PRT=CX1*FTCM*ANTOM**2
IF (ITCNCE.EQ.0) PR(11)=PRT
IF (ITCNCE.NE.0) PR(13)=PRT
WRITE (6,152) (PR(I),I=1,13)
GO TO (66,67), J2
WRITE (6,153),
PR(1)=HSX(1)/AMTOMS
PR(2)=HSZ/AMTOMS
PR(3)=HBX/AMTUMS
PR(4)=HEZ/AMTOMS
PR(5)=CEASF
PR(6)=FRESF
```

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```
      PR(7)=TEMFF
      WRITE(6,154) (PR(I),I=1,7)
      GO TO 65
   67 WRITE(6,155) CODE*
      DO 68 I=1,NATM,7
      PR(1)=ATM(I)
      PR(2)=ATM(I+1)/AMTOMS
      PR(3)=ATM(I+2)/AMTOMS
      PR(4)=ATM(I+3)
      PR(5)=ATM(I+4)
      PR(6)=ATM(I+5)
      PR(7)=ATM(I+6)
   68 WRITE(6,196) (PR(J),J=1,7)
   69 SINLAT=SIN(LAT*CVDTCR)
      COSLAT=COS(LAT*CVDTCR)
      SINAZ=SIN(A2*CVMTOR)
      COSAZ=CCS(A2*CVMTOR)
      IF(ISUN.EQ.0) GO TO 70
      WP1=AINT(RACS/10000.)
      AFP1=RACS-WP1*10000.
      FP1=AINT(AFP1/100.)
      FP2=AFP1-FP1*100.
      RASD=PI12*(WP1+FP1/60.+FP2/3600.)
      WP1=AINT(HACA/10000.)
      AFP1=HACA-WP1*10000.
      FP1=AINT(AFP1/100.)
      FP2=AFP1-FP1*100.
      HAGD=PI12*(WP1+FP1/60.+FP2/3600.)
      WP1=AINT(TOCAY/10000.)
      AFP1=TOCAY-WP1*100.
      FP1=AINT(AFP1/100.)
      FP2=AFP1-FP1*100.
      TOCAYD=FI12*(WP1+FP1/60.+FP2/3600.)
      WP1=AINT(ADCS/10000.)
      AFF1=ALCS-WP1*1000.
      FP1=AINT(AFP1/100.)
      FP2=AFP1-FP1*100.
      CECLD=CSDTCR*(WP1+FP1/60.+FP2/3600.)
      DEL=HAGC-RASD
      IF(CEL.LT.0.)DEL=DEL+TWOPHI
      DEL=DEL-CVDTOR*ALOAG+TCCAYC
C     WHAT IS SINCOS (SUBROLTINE?
      CALL SINCOS(DECLD,SINC,COSD)
      SINC=SIN(CECLD)
      COSC=CCS(CECLD)
   70 PP1=10CCO.
      IF ERR=C
      CM=0.
```

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```
      IF (IRC1.EC.1) GC TC 71
      LAM(1)=C.
      LAM(2)=C.
      LAM(3)=C.
      GO TO 72
   71 LAM(1)=-.000145858424*COSLAT*SINAZ
      LAM(2)=-.000145858424*SINLAT
      LAM(3)=.000145858424*COSLAT*CCSAZ
   72 JCGE=1
      IF (IITCNCE.EQ.0) GO TO 74
      JCGE=2
      WRITE (6,2CC)
      CALL PNEST (26,QE(1),0,T4)
      TL=(AINT((TL+.0005)*1000.5))/1000.
      ICQTT=ICQTT+1
      IF (IICQTT.NE.11) GC TO 74
   73 WRITE (6,175) UMCB,XI,CCDEM,ICCT1
      IEFC=2
      CALL SFFINT (Y,CY,1)
      GO TO 4
   74 I6 CP=0
      IF (I3CEUR.EQ.0) GC TC 75
      ICCT1=ICCT1+100
      ICCT2=ICCT2+100
      ICCT3=ICCT3+100
      ICCT4=ICCT4+100
   75 R3TEM=CCTEM-CGTB
      R3=0.
      TO=MTBM-MTB
      R1TEM=R1BM*R3TBM/TO
      RK2=RK*.5
      R1TE=R1TEM-RK2*TO
      RK12=(FK**2)/12.
      R2TESG=R2TBM**2-RK12*TC**2
      BTE=BTEM-TO*R2TBM**2-MTB*R1TBM**2+MTBM*(R1TEM-R3TBM)**2
      RETB=LE(1)-CGTB
      RITTE=RETE-RN
      CSG=D**2
      D22=MTBST/BC
      Y(1)=MTEM
      Y(2)=TEA
      Y(3)=PC
      CONS2=(TEST-TBMST)/(TB-TBM)
      SINEU=SIN(EL*CVMTUR)
      COSEU=CCS(EL*CVMTOR)
      SINAZC=SIN(AZD*CVMTCR)
      CCSAZD=CCS(AZD*CVMTGR)
      SINGE=SIN(GE(1)*CVMTGR)
```

```
      COSCE=CCS(CSE(1))*CVMTOR)
      COSAZU=CCS(AZU*CVMTOR)
      SINAZU=SIN(AZU*CVMTCR)
      B=BTBM
      TRCCNS=MF*CONS2*ISP/IST
      DO 76 I=4,9
   76 CY(I)=0.
      CY(2)=1.0
      IKL=5
      I1=1
      J5=1
      J6=1
      J7=2
      IMZ=0
      IMZ1=0
      IMZ2=0
      IF (CUO.NE.0.) GC TC 77
      IF (TBM.LT.C.) GO TO 81
      Y(4)=IX1
      Y(7)=IL*COSEU*COSAZL
      Y(8)=IL*SINEU
      Y(9)=-IL*SINAZU*COSEU
      IF (IX2.EQ.C.) GC TO 82
      Y(5)=IX2
      J8=1
      GO TO 78
   77 Y(4)=LL*CCSCE+IX1
      Y(5)=SINCE+IX2
      Y(7)=UC*COSCE*COSAZC+IU*COSAZU*COSEL
      Y(8)=UC*SINCE+IU*SINEU
      Y(9)=-IL*SINAZU*COSEU+LO*CCSQE*SINAZC
      J8=2
      DY(7)=C
      DY(8)=C
      CY(9)=0
      Y(2)=TL
      IF (ITO.NE.C.) Y(2)=ITO
   78 CELT=ICC.
      PY(1)=C.
      PY(2)=Y(3)
      DPY(1)=1.0
      INA=1
   79 WRITE (6,280)
      CALL RKC (DELT,2,DCA,PY,DPY,QQ,INN)
      INN=2
      IF (ABS(FY(1)-Y(5))).LT..00001) GO TO 8C
      IF (PY(1)-LT.Y(5)) GO TC 79
      DELT=Y(5)-PY(1)
```

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```
80   GO TO 75
     Y(2)=PY(2)
81   GO TO (82,83), J8
     DELT=DELTB
     TIME=0.
     I2=1
     I3=1
     NEC=2
     GO TO 135
82   DELT=DELTB
     TIME=TL
     Y(2)=0.
     I2=2
     I3=2
     I4=1
     I5=1
     I6=1
     NEC=8
     GO TO 135
83   I3=1
     I4=2
     I6=2
     I7=1
     I8=1
     I9=1
     NEX=1
     J6=1
     I2=2
     I5=1
     NEC=16
     KI=0
     IFIRST=1
     DELT=DELTB
     IF(TDI.LE.C.) GO TO 84
     CELT=CETFF
     I4=3
     I5=2
84   TIME=TCE+ITO
     D3=DSG*D
     C44=D3+*C
     EAR=CVPTCR*IUAZ
     EER=CVMTOR*IUEL
     SINEA=SIN(EAR)
     COSEA=CCS(EAR)
     SINEE=SIN(EER)
     COSEE=CCS(EER)
     Y(14)=CCSEE*SINEA
     Y(15)=SINEE*COSEA
```

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      Y(16)=CCSEE*SINEA
      ANX=0.
      ISFI=0
      IF (Y(1C).LE..0) GC TC 85
      A= ATBM
      ANX=Y(1C)*A
      CONS3=(ATBM-ATB)/(MTBM-MTB)
      CTS=(TSFEST-TSRIST)/(TSRB-TSRI)
      GCRS=GC*FS
      RNESQ2=RNE**2*.5
      I1=2
      I8=2
      NEC=16
   85 IF (ITCNGE.EQ.0) GC TC 86
      WRITE (6,270)
      CALL PNEST (28,QE(1),0.,IH3)
      WRITE (6,27C)
      CALL FNEST (20,QE(1),0.,BC)
      BC=BC/ANTGM**2
   86 BIH2=B*BIH2
      Y(11)=ANX*Y(14)-BIH2*SINEE*COSEA-B*IH3*SINEA
      Y(12)=ANX*Y(15)+BIH2*CCSEE*SINEA+B*IH3*COSEA
      Y(13)=ANX*Y(16)-BIH2*SINEE*SINEA+B*IH3*COSEA
      DY(7)=C..
      DY(8)=C..
      CY(9)=0.
      ALPE=0.
      ALPC1=C..
      ALPC2=C..
      ALPQ3=C..
      T45(1)=GE(1)
      T45(2)=IH2
      T45(3)=IH3
      T45(4)=TF
      T45(5)=C.
      T45(6)=SL
      T45(7)=G
      T45(8)=LQ*PMTOF
      T45(9)=CCCE
      T45(10)=1CCT4
      IF (TL.GE.TE6) GO TO 85
      CO 87 I=1,10
      J= ITTT+I+2659
   87 TJ(J)=T45(I)
      ITTT=ITTT+10
      I6DP=1
      IF (I3CEUR.EQ.0) GC TC 139
```

+DU007210
+DU007220
+DU007230
+DU007240
+DU007250
+DU007260
+DU007270
+DU007280
+DU007290
+DU007300
+DU007310
+DU007320
+DU007330
+DU007340
+DU007350
+DU007360
+DU007370
+DU007380
+DU007390
+DU007400
+DU007410
+DU007420
+DU007430
+DU007440
+DU007450
+DU007460
+DU007470
+DU007480
+DU007490
+DU007500
+DU007510
+DU007520
+DU007530
+DU007540
+DU007550
+DU007560
+DU007570
+DU007580
+DU007590
+DU007600
+DU007610
+DU007620
+DU007630
+DU007640
+DU007650
+DU007660
+DU007670
+DU007680

143

```
       D22=MTEST/BC
       I6CP=0
       IF (Y(1C).GT..0) GC TO 88
       I7=2
       I8=3
       NEG=9
       GO TO 135
88     ISPI=0
       I7=1
       I8=4
       I9=2
       NEG=10
       GO TO 135
85     ISPI=0
       IF (I3CBLR.NE.0) GC TC 90
       ICCT1=ICCT1+100
       ICCT2=ICCT2+100
       ICCT3=ICCT3+100
       ICCT4=ICCT4+100
       T45(10)=ICCT4
90     T45(5)=EC/AMTO IN**2
       DO 91 I=1,10
       J=ITTT+2659+I
       TJ(J)=T45(I)
       ITTT=ITTT+10
       Y(1)=MTE
92     BURN(I)=Y(I)
       GO TO 114
92     CONTINUE
       IEPD=5
       WRITE (6,29C)(Y,CY,1)
       CALL SFFINT (Y,CY,1)
       DELT=DELTE
       PTIME=FTE
       IPRINT=Y(2)+PTB
       TIME=TMCE
       I3=4
       J6=2
       IF (TCI.GT.0.) GC TC 94
       GO TO 140
94     DELT=DETFF
       I3=5
       TIME=TCI
       GO TO 140
95     IFIRST=0
       JBLRN=2
       INN=1
```

```
      I3=6
      I4=2
      I5=1
      DELT=DELTB
      GO TO 140
96    JBURN=1
      IEPD=5
      WRITE (6,290)
      CALL SFFINT (Y,CY,1)
      TIME=TE
      IF (ABS(TCI-TPRINT).LE..00001) GO TO 97
      GO TO 140
97    TPRINT=TPRINT+PTIME
      GO TO 140
98    I3=7
      I5=3
      DELT=DELTFF
      IF (ITB.EQ.TMCB) GO TO 100
      JBURN=3
      GO TO 135
95    JBURN=1
      IEPD=5
      WRITE (6,290)
      CALL SFFINT (Y,CY,1)
      TIME=TMCB
      I3=5
      GO TO 140
100   IFIRST=C
      JBURN=4
      GO TO 135
101   JBURN=1
      IEPC=5
      WRITE (6,290)
      CALL SFFINT (Y,CY,1)
      DELT=CELTE
      TIME=TEE
      I3=8
      J6=1
102   IF (TDI.GT.0.) GO TO 104
      IF (ITE.EQ.1) GO TO 103
      IF (TMCE.EQ.TE6) GO TO 105
      GO TO 140
103   NEX=2
      GO TO 148
104   CELT=CETFF
      GO TO 1C2
105   IF (ITCNGE.NE.0) GO TO 106
      ICCTT=0
```

145

```
106   IF (TMCE.EQ.TE6) GC TC 107
      IEPC=5
      WRITE (6,290)
      CALL SPRINT (Y,DY,1)
107   CO 108 I=1,16
108   BURN(I)=Y(I)
109   IF (I3CEUR.EQ.0.AND.ITONQE.EQ.0) GC TO 110
      GO TO 112
110   ICCTT=ICCTT+1
      IF (ICCTT.NE.11) GO TO 111
      WRITE (6,175) UMCB,XI,CCDEM,ICCT1
      IEPD=2
      WRITE (6,290)
      CALL SFFINT (Y,CY,1)
      GU TO 167
111   ICCT1=ICCT1+100
      ICCT2=ICCT2+100
      ICCT3=ICCT3+100
      ICCT4=ICCT4+100
112   T45(5)=BC/A*TO IN**2
      T45(6)=SL
      T45(10)=ICCT4
      DO 113 I=1,10
      J=I+ITTT+2659
113   TJ(J)=T45(I)
      ITTT=ITTT+1C
      DY(7)=C.
      DY(8)=C.
      CY(9)=0.
      ALPE=0.
      TALPH=C.
114   IF (I3CF.EC.0) GO TO 115
      IKL=12
115   D22=MTBST/BC
      CELT=CETFF
      PTIME=PTFF
      Y(1)=MIE
      CY(1)=0.
      TPRINT=ICFF
      IF (TPRINT.EQ.0.) TPRINT=PTFF+ITO
      I4=3
      I5=3
      J6=2
      NEX=1
      KL=0
      NEG=16
      I6DP=0
      IF (ILCREE(1).EQ.0) GO TO 116
```

+DU08650
+DU08660
+DU08670
+DU08680
+DU08690
+DU08700
+DU08710
+DU08720
+DU08730
+DU08740
+DU08750
+DU08760
+DU08770
+DU08780
+DU08790
+DU08800
+DU08810
+DU08820
+DU08830
+DU08840
+DU08850
+DU08860
+DU08870
+DU08880
+DU08890
+DU08900
+DU08910
+DU08920
+DU08930
+DU08940
+DU08950
+DU08960
+DU08970
+DU08980
+DU08990
+DU09000
+DU09010
+DU09020
+DU09030
+DU09040
+DU09050
+DU09060
+DU09070
+DU09080
+DU09090
+DU09100
+DU09110
+DU09120

146

```
      I6CF=1
      J5=2
      INA=1
      IUSA=1
      JJI=1
      TST=0.14C
      GO TO 14C
116   TST=0
      IF (Y(1C).GT.0.) GC TC 117
      I7=2
      I8=3
      NEG=9
      GO TO 118
117   IF (ISFI.EQ.1) Y(10)=HCX/A
      I7=1
      I8=4
      I9=2
      NEG=10
118   INA=1
      IF (J6.EQ.1) J6=3
      IUSA=1
      JJI=2
119   WRITE (6,28C)
      CALL RKC (DELT,NEQ,CER,Y,DY,QQ,INN)
      INA=2
      IEXIT=1
120   IF (I6CP.EQ.1) GO TC 121
      T1=Y(1C)/T*CPHI
      GO TO 122
121   T1=C
122   IF (A.GT.0.) T1=HDX/(I*CPHI*A)
      IF (T1.LT.20.) GC TO 125
      IF (VT.EC.C..OR.Y(2).LT.TL) GO TO 125
      IF (A.EC.C.) GOTO 125
      CAFM=KP*(CENS*DSQ*D33/B
      CAPP=T*CPHI*T1*D*A/(B*VT)
      T1=KDB+CKCB
      IF (I6CF.EC.1)T1=KDE+DKCBA
      T2=DENS*D33/Y(1)
      CAPT=T2*(KL-KT*(Y(1)*DSQ(A))
      CAPH=T2*(KL-T1+KH*(Y(1)*DSC/B))
      T1=2.*CAPP*(2.*CAPT-CAPH)
      T2=4.*CAFM+CAPh**2-CAPP**2
      T3=SIN(.5*ATAN2(T1,T2))
      T1=SQRT(SQRT(T1**2+T2**2))
      PP1=.5*(CAPF+T1*T3)
      PP2=.5*(CAPP-T1*T3)
      IF (AES(FFI).GE.ABS(PP2)) GO TO 123
```

147

```
      T1=PP1
      PP1=PP2
      PP2=T1
123   IF(Y(2).NE.TL) GO TO 124
      PRPP1=FF1
      PRPP2=PP2
      FF1=10000.
      PP1=PP1
      PPF1=PP1
      PPF2=PF1
      GO TO 125
124   T1=DELT*T1/D
      PPF1=(FF1-PRPP1)/T1
      PKPP1=(PP1)
      PPF2=(FF2-PRPP2)/T1
      PRFF2=FF2
125   GO TO (126,141),IEXIT
126   IF(ISTIM.EQ.0) GO TO 128
      IF(ABS(TI-Y(2)).LE..00001) GO TO 130
      IF(K1.EQ.1) GO TO 127
      IF(Y(2).GT.TI) GO TO 127
      GO TO 145
127   DELT=TI-Y(2)
      K1=1
      GO TO (140,119),JJ1
128   IF(IXIAYI.EQ.0) GO TO 131
      IF(ABS(XI-Y(4)).LE..00001) GO TO 130
      IF(K1.EQ.1) GO TO 129
      IF(Y(4).GT.XI) GO TO 129
      GO TO 145
129   DELT=(XI-Y(4))/Y(7)
      K1=1
130   GO TO (140,119),JJ1
      IF(XIEL.EC.0.) GO TO 137
      IF(ABS(XIMAX-XI).LT.(XIDEL/10.).OR.XI.GT.XIMAX) GO TO 137
      IEFC=5
      WRITE (6,290)
      CALL SPRINT(Y,DY,1)
      XI=XICEL+XI
      DELT=DELTB
      K1=0
      IF(I5.EC.4) GO TO 145
      DELT=DETFF
      GO TO 145
131   YP=Y(5)
      IF(IYP.GT.0) YP=EC
      IF(Y(2).EQ.0.) GO TO 132
      IF(ABS(YP-YI).LE..000001) GO TC 137
```

```
132  IF (K1.EQ.1) GO TO 136
     GO TO (133,135), J5
133  IF (Y(6).GE.0.) GO TO 134
     WRITE (6,178) CODE,ICO#1
     IEPC=3
     WRITE (6,25C)
     CALL SFFINT (Y,DY,1)
     GO TO 4
134  IF (YP.LT.YI) GO TC 145
     GO TO 136
135  IF (Y(6).GT.0.) GO TO 145
     IF (YP.GT.YI) GO TO 145
136  DELT=(YI-YPJ)/Y(8)
     K1=1
     GO TO (140,119), JJ1
137  IEFC=5
     NEX=4
     J7=2
     IF (JITE.EG.1) GC TC 138
     WRITE (6,25C)
     CALL SFFINT (Y,DY,1)
     GO TO 4
138  NEX=5
     J7=2
     WRITE (6,25C)
     CALL SFFINT (Y,CY,1)
     GO TO 152
139  INN=1
     IUSA=2
     JJ1=1
140  WRITE (6,280)
     CALL RKG (DELT,NEQ,CER,Y,DY,QQ,INN)
     INN=2
     IEXIT=2
     GO TO (120,142,56,55,1C1), JBURN
141  GO TO (142,126),J5
142  GO TO (143,128),J5
143  IF (ABS((Y(2)-TIME).LE..00001)GOTC(82,83,53,100,95,98,100,105,
    110)1113
     IF (Y(2)+DELT.GT.TIME) GCTO 1443
     IF (Y(2)+DELT.LT.TIME+.00001) GCTO 144
1443 DELT=TIME-Y(2)-10.E-15*TIME
     GOTC (14C,119) JJ1
144  IF (NEC.GT.9) GO TO 126
     GO TO (140,146,119),J6
145  IF (ABS(Y(2)-TPRINT).LE..00001) GC TC 147
     K2=0
     IF (Y(2)+DELT.LT.TPRINT) GC TO (140,119), JJ1
```

149

```
      K2=1
      SCC=DELT
      DELT=TFRINT-Y(2)
      GO TO (140,119), JJ1
147   IEPO=5
      WRITE (6,290)
      CALL SFFINT (Y,DY,1)
      TPRINT=TPRINT+PTIME
      IF (K2.EC.0) GO TO (140,119), JJ1
      DELT=SCC
      K2=0
      GO TO (140,119), JJ1
148   LN=LN/FNTOF
      PHI=PHI*CTGM/PDTGM
      THETA=TFETA*DTOM/PCTCM
      TO=UMCE-LN
      T1=PHMCE-PFI
      T2=THMCE-THETA
      IF (TFN.LT.0.) GO TO 149
      T3=TO*(IFN-TF)/(UNA-UN)
      T4=T1*(TFN-IH3)/(PHIN-PHI)
      T5=T2*(TFN-IH2)/(TFETAN-THETA)
      GO TO 16C
149   T3=TO*TFLB
      T4=T1*IF3B
      T5=T2*IF2B
16C   TFN=ABS(TFN)
150   IF (ABS(TO).LT.EUB.ANC.ABS(T1).LT.EFB.AND.AES(T2).LT.ETB) GO TO 15
11    TFN=TF
      H2N=IH2
      H3N=IH3
      UNA=UN
      PHIN=PF+I
      THETAN=Tr-ETA
      TF=TFN+13
      IH2=H2N+T5
      IH3=H3N+T4
      ICCTT=ICCTT+1
      IF (ICCTT.EQ.10) GO TO 73
      ICOT2=ICOT2+10
      ICCT3=ICCT3+10
      ICCT4=ICCT4+10
      GO TO 72
151   NEX=1
      IF (TMCE.EC.TE6) GC TC 105
      GO TO (14C,119), JJ1
```

```
152 IF (IXIAVI.EQ.0) GO TO 154
    YP=EC
    IF (IYF.EC.0) YP=Y(5)
    IF (ABS(IYI-YP).LE.EX1) GO TC 165
153 YP=Y(5)
    IF (IYF.NE.0) YP=EC
    TO=YI-YP
    XYI=YP
    GO TO 156
154 IF (ABS(Y(4)-XI).LE.EX1) GC TO 165
155 TO=XI-Y(4)
    XYI=Y(4)
156 T2=ZI-Y(6)
    IF (CM.NE.0.) GC TC 164
    T1=TO*CXI
    T3=T2*L2I
157 XM=Y(4)
    IF (IXIAVI.EQ.0) GO TO 158
    YP=EC
    IF (IYP.EQ.C) YP=Y(5)
    XM=YP
158 IF (JCCE-1) 159,159,160
159 CM=BC
    BC=BC+T1
    GO TO 161
160 CM=CE(1)
    CE(1)=CE(1)+T1
    IUEL=QE(1)
161 SLM=SL
    ZM=Y(6)
    SL=SL+T3
    IF (T3CEUR.EQ.0.ANC.ITCNQE.EQ.0) GO TO 162
    TFN=-TF
    Y(10)=SFN*TWOPHI
    GO TO 72
162 DO 163 I=1,16
163 Y(I)=ELFN(I)
    GO TO 1C5
164 CQE=QE(1)
    IF (JCCE.EQ.1) CQE=BC
    T1=TO*(CM-CQE)/(XM-XYI)
    T3=0.
    IF (ABS(ZM-Y(6)).LT..00000001) GO TC 157
    T3=T2*(SLM-SL)/(ZM-Y(6))
    GO TO 157
165 IF (ABS(Y(6)-ZI).LT.EZI) GC TO 166
    IF (IXIAVI.EQ.0) GO TO 155
    GO TO 153
```

151

```
166   NEX=4
      J7=1
      IEFD=4
      WRITE (6,125C)
      CALL SFFINT (Y,CY,1)
      GO TO 4
167   CALL SFFINI (Y,CY,2)
      GO TO 4
98765 IFERR=1
      IEPC=5
      WRITE (6,174)
      WRITE (6,165)
      J7=1
      NEX=4
      J1=4
      WRITE (6,290)
      CALL SPRINT (Y,DY,1)
      STCP
165   FORMAT (38H RUNNING TCO LONG OR HAC TO EE STOPPED)
170   FORMAT (1EI2)
171   FORMAT (7F10.6,2X,A5,I3)
172   FORMAT (29H METRC CARDS ARE OUT CF CRDEF)
173   FORMAT (33H ERROR IN METRO ENLARGE ATM ARRAY)
174   FORMAT (2H1 )
175   FORMAT (20H ITERATED TEN TIMES ,2F10.2,A5,I5)
176   FORMAT (38H TRAJECTCRY UPLEG WILL NCT REACH BURST,A5,I5)
177   FORMAT (51H     UO VEH      GE     SPIN    CMEGAY O OMEGAZ O INIT.L EUE,20H
     1EL  VEH      UO VEH         AZ CF FIRE CELTA AZ AZ WRT VEH,60H
     2NIT'L ELA FIN CANT/31H      CMEGAY O OMEGAZ O INIT.L EUE,26H
     3   MILS     MILS       FT/SEC    REV/SEC  RAD/SEC ,40H RAD/SEC  ,6H MILS
     4   MILS     MILS       RAD                                 RAD/SEC )
178   FORMAT (//55X,15H INPUT FOR CODE ,A5//)
179   FORMAT (51H REF  WT   WT TBM    CG (TB)      IX TBM    IX  FUEL WT  DE WT
     1 DIA MISS LGTH MISS CG TBM  WT IM(TE)        WT I(TB)       ,28H IX TBM
     2Y (TBM) LGTH LCHR/31H      LB      LB       FT          LE    ,60H    LB
     3   LE-FT2      LB-FT2                    FT          FT   ,40H LB-FT2 )
180   FORMAT (5F10.3,4F10.5,3F10.2,F10.5//)
181   FORMAT (51H      UO VEH      GE     TWIST    CMEGAY O OMEGAZ O INIT.L EUE,20H
     1EL  VEH      UO VEH         AZ CF FIRE CELTA AZ AZ WRT VEH,60H
     2NIT'L ELA FIN CANT/31H      MILS      ISP   CAL/REV   RAD/SEC ,60H
     3   MILS     MILS       FT/SEC    CAL/REV   RAD/SEC ,40H RAD/SEC )
182   FORMAT (2F10.3,4F10.4,F10.3,3F10.3,3F 10.5,2F1C.4,F10.6//)
183   FORMAT (51H    IST     IST RATIO  T-I RATIO    ISP   RAD CY F RAD NOZ EX A JET EX,60H
     1 JET OF EAY-2/41H   PRESS DIST FL/WT RT ASCEN   APP DECL HR ANG,24H FP
     2A T OF          LBF-SEC LBF-SEC/LBM                FT          FT   ,60H
     3FT2        LE/FT2         FT/LB    HR/MIN/S   CEG/MIN/,24HS     HR )
```

```
    4MIN/S  ,FR/MIN/S/)
184 FORMAT (2F10.2,F10.4,2F10.6,F10.2,2F10.5,4F11.3//)
185 FORMAT (51H ... )
186 FORMAT (13F10.5//)
187 FORMAT (51H ... )
188 FORMAT (13F10.5//)
189 FORMAT (51H ... )
190 FORMAT (F10.5,3F10.3,F10.5,5F10.3,F10.5,1PE10.3,0PF10.5//)
191 FORMAT (51H ... )
192 FORMAT (F10.5,8F10.3,2F10.5,3F10.2,4F10.5//)
193 FORMAT (30X,56HRWIND TST CWIND TST FF CWIND FF AIR DENSIT,
    2                                                            )
194 FORMAT (20X,4F10.5,3F10.7)
195 FORMAT (1H1,56X,13HMET FOR CODE )
196 FORMAT (30X,F10.3,2F10.5,F10.3,2F10.4,F10.5)
197 FORMAT (1H1,61X,8HCONTROLS//)
198 FORMAT (4A10,5X,4A10,5X,4A10)
200 FORMAT (7A10,A7,A1,A2)
210 FORMAT (27H ERROR CONTROL IN 75 AND 80)
220 FORMAT (7F10.5,A7,A1,A2)
250 FORMAT (15H GO TO DO READ)
260 FORMAT (19H CHECKPOINT REACHED)
270 FORMAT (25H GONE TO PNEST FM 72 MAIN)
280 FORMAT (20H GONE TO PNEST FM 85 MAIN)
290 FORMAT (20H GONE TO RKG FM MAIN)
    FORMAT (23H GONE TO SPRINT FM MAIN)
    END
    SUBROUTINE CER (Y,CY)
    DIMENSION Y(16), JY(16), LE(1), QE(1), WSX(1)
```

```
      COMMON LE, FN, RK, R2TEM, RNE, D, XICEL, LL, GO, TBMST, TBST, IST, PE,    +DU12490
     1 AE, MTBST, MDI, DELIB, DETFF, XICEL, XIMAX, IH2B, IH3B, TFUB,            +DU12500
     2 CXI, LZI, ETE, EPB, EUB, SPN, EXI, SRIST, ISRBST, RS, UE, IH2,           +DU12510
     3 IH3, TF, BC, SL, UO, SPN, IX1, IX2, IU, AZU, EU, TBM, TSRI,              +DU12520
     4 TCE, TB, TE6, TCFF, PTB, PTFF, AZD, MTB, MF, MTB, ISP, TSRI,             +DU12530
     5 TSRE, TSCF, CGTBM, ATBM, ATE, BTBM, LAT, AZ, TMCB, UMCB,                 +DU12540
     6 FHMCE, IHMCB, TI, XI, YI, ZI, WSX, WSZ, WEX, WBZ, DENSF, PRESF,          +DU12550
     7 TEMPF, SLED                                                              +DU12560
      COMMON ITM(700), IMZ1, IMZ2, NATM, JZ, IDGREE(1), IROT                    HDU12560
     1 IREDLC, ITWT, IUPLEG, IUNIT, ISPRT, IRSET, ISTIM, ISCOUT,                +DU12560
     2 I3DBUF, I3DP, ISAVE6, ITONQE, IXIAYI, ISDIG, IX2N, LAM(3),               +DU12590
     3 E, A, SINCE, CCSCE, LSQ, IKL, GORSC, YOUT, ZCUT, TOF,                    +DU12600
     4 AA, IL, AZU1, ELI, PPI, QEOUT, TEMPA, DEASN, WX, CON, ICNN,              +DU12610
     5 CENS, PA, VAS, EC, PPI, PP2, PPP1, PPP2, BTB, CONS2, CONS3, D33,         HDU12620
     6 C44, CCRS, R1TB, R2TBSQ, RETB, RK12, RK2, RNES, IYP,                     +DU12640
     7 IEPD, CSR, R1TB, R2TBSQ, RETB, RK12, RK2, RNES2, KITE, TRCLNS,           +DU12650
     8 ICNP, TST, IT, ITTT, IFERR, ICI, HDX, CTS, IO, I1, I2, T3,               +DU12660
     9 T4, IE, TALPH, THETA, ALPE, ALPG1, ALPG2, ALPG3, CODE, D22,              +DU12670
     A IFIRST, JI, J7, PHI, PDTCM, PMTUF, TJ(250), LN, YP, ICODE, ICCT1,        +DU12680
     B ICOT2, ICCT3, PHI, I6LP, R3, ALPA, VT, V1, V2, V3, TSTAR, KDB,           HDU12690
     C KM, KL, KT, XDX, KH, DKDB, MACH, SINLAT, COSLAT,                         +DU12700
     D SINAZ, COSAZ, SINC, COSD, DEL                                            +DU12710
      COMMON /ERR/ IER                                                          +DU12720
      COMMON /BCH/ REARTH, GC, AMTOMS, PQ, AMTOF, FTGM, ANTUM, RTOD,            +DU12730
     1 CTOM, INCFHI, AMTCIN, AMTOKN, FTOR2, CVDTGR, CVMTGR, RSQ,                +DU12740
     2 HA(25), TM(25), ALV(25), HEAD(169)                                       +DU12750
      REAL LE, LSF, LAT, MDI, IH2B, IH3B, IU1, IX2, IH3, IX1, IX2, IU, MF, MTB  HDU12760
     1 ISF, LAT, LAM, MTB, MTBST, IU1, IX2N, IUN, LZI                           +DU12770
      REAL NLJ, NL2, NU3                                                        +DU12780
      REAL MACH, KM, KCB, KL, KH, KF, KTA, KT, KLA, KA, KE, KHA, KMA, KSH       HDU12790
    1 GO TO (35,1), IUSA                                                        +DU12800
    1 AM=CONS2*(Y(2),-TBM)+TEMST                                               +DU12810
      WRITE (657)                                                               +DU12820
      CALL PNEST (1,AM,TALPH,TST)                                              +DU12830
      TR=TRCLNS*TST                                                             +DU12840
      TO=Y(1)-MTB                                                               HDU12850
      R1=R1TE+RK2*TO                                                            +DU12860
      R2SQ=R2TBSQ+RK12*TO**2                                                    +DU12870
      R3=TO*F1/Y(1)+ISP                                                         HDU12880
      CY(1)=-1F/ISP                                                             +DU12890
      B=BTB+((Y(1)-MTB)*R2SQ+MTB*R1**2-Y(1)*(R1-R3)**2                          +DU12900
      GO TO (22,3), I1                                                          +DU12910
   (2) GO TO (24,35), I2                                                        +DU12920
   (3) A=ATB+CCNS3*(Y(1)-MTB)                                                   +DU12930
      GO TO 2                                                                   +DU12540
    4 V1=Y(7)                                                                   +DU12550
      V3=Y(9)                                                                   +DU12560
```

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```
 5    IF (TST).LE.0.) GO TO 12
      TSTAR=TR*TF+(PE-PA)*AE
 6    V2=Y(8)
      VTSQ=V1**2+V2**2+V3**2
      VT=SQRT(VTSQ)
      MACH=V1/VAS
      IF (16CF.EQ.1) GO TO 7
      VDCTX=(15,19,20,13),I5
      COSA=VDCTX/VT
 7    IF (ABS(CGSA).LE.1.0005) GO TO 8
      WRITE (6,55) Y(2),CCSA,CODE,ICCT1
      GO TO IER, (56)
 8    IF (ABS(CCSA).LE.1.0.) GO TO 9
      IF (COSA.LT.0.) GO TO 10
      COSA=1.
      ALPHA=C.
      GO TO 11
 9    COSA=-1.
      ALPHA=3.14526535
      GO TO 11
10    ARCCS=WAS AFCCCS
11    ALPHA=ARCGS(COSA)
      ALFSQ=ALPHA**2
      TALFH=ALPSC
      GO TO (15,15,20,13), I5
12    TSTAR=0.
      DY(1)=0.
      GO TO 6
13    V1=Y(7)-WSX(1)
      V3=Y(5)-WSZ
      GO TO 5
14    V1=Y(7)-WBX
      V3=Y(5)-WBZ
      GU TO 5
15    WRITE (6,57)
      CALL PNEST (2,MACH,TALPH,KDB)
      GO TO (16,21), I6
16    WRITE (6,57)
      CALL PNEST (9,MACH,TALPH,F)
      F=F*FTCM
      TO=(GC*TSTAR-DENS*C22*KDB*VTSQ)/Y(1)-GO*SINGE-F*COSGE
      CY(9)=0.
      IF (TC.G1.0.) GO TO 17
      DY(7)=C.
      CY(8)=C.
      GO TO 18
17    CY(7)=TC*CUSQE
```

C

```
      DY(8)=TC*SINUE
18    DY(4)=Y(7)
      DY(5)=Y(8)
      DY(6)=Y(9)
      GO TO 23
19    DY(1)=MCI/(TL-TDI)
20    WRITE (6,57)
21    CALL PREST (4,MACH,TALPH,KCB)
      TO=Y(5)+REARTH
      R=SQRT(Y(4)**2+TO**2+Y(6)**2)
      T1=GOR*C/R**3
      G1=T1*Y(4)
      G2=T1*TC
      G3=T1*Y(6)
      NU1=-LAM(1)*Y(8)-LAM(2)*Y(5)
      NU2=LAM(1)*Y(7)+LAM(3)*Y(9)
      NU3=LAM(2)*Y(7)-LAM(3)*Y(8)
      T4=GC*TSTAR
      GO TO (22,27), I7
22    WRITE (6,57)
      CALL PREST (3,MACH,TALPH,DKDB)
      DKDBA=DKDB*ALPSQ
      T1=CENS*C22
      T1G=DENS*C32
      T2=DENS*DSQ
      WRITE (6,57)
      CALL PREST (IKL,MACH,TALPH,KL)
      CALL PREST (10,MACH,TALPH,KM)
      RE=RETE-R3
      XCG=LE(1)-RE
      TO=(CGTE-XCG)/D
      KM=KM-TC*(KL+KDB)
      GO TO (23,27), IS
23    T1=-T1*(KLB+DKDBA)*VT
      WRITE (6,57)
      CALL PREST (6,MACH,TALPH,KS)
      T3=T1O*KS*VT/B
      X1CH1=Y(15)*Y(13)-Y(16)*Y(12)
      X2CH2=Y(16)*Y(11)-Y(14)*Y(13)
      X3CH3=Y(14)*Y(12)-Y(15)*Y(11)
      RT=RTTE-R3
      CALL PREST (8,MACH,TALPH,KH)
      T11=DENS*D44
      T7=-DY(1)*RE*RT
      DY(10)=C.
      HDX=0.
      V1CX1=V2*Y(16)-V3*Y(15)
      V2CX2=V3*Y(14)-V1*Y(16)
```

```
      V3CX3=V1*Y(15)-V2*Y(14)                                      HDU13930
      DO 24 I=7,9                                                  HDU13940
      DY(I)=C.                                                     HDU13950
24    DY(I+4)=0.                                                   HDU13960
      XDX=Y(14)**2+Y(15)**2+Y(16)**2                              HDU13970
      IF (XCX.LE.1.0005) GO TO (25,26,28,30), 18                  HDU13980
      WRITE (6,54) Y(2),XCX,CCDE,ICOTI                            HDU13990
      GO TO (56) IER                                               HDU14000
25    T2=T2*KL*SL6D                                                HDU14010
      T5=TIO*KM*VT                                                 HDU14020
      T6=TI1*KH*VT                                                 HDU14030
      DY(7)=(TI*V1+T2*(VTSQ*Y(14)-VDOTX*V1)+T3*X1CH1+T4*Y(14))/Y(1)-G1  HDU14040
     1+NU1+CY(7)                                                   HDU14050
      DY(8)=(TI*V2+T2*(VTSQ*Y(15)-VDCTX*V2)+T3*X2CH2+T4*Y(15))/Y(1)-G2  HDU14060
     1+NU2+CY(8)                                                   HDU14070
      DY(9)=(TI*V3+T2*(VTSQ*Y(16)-VDCTX*V3)+T3*X3CH3+T4*Y(16))/Y(1)-G3  HDU14080
     1+NU3+CY(9)                                                   HDU14090
      DY(4)=Y(7)                                                   HDU14100
      DY(5)=Y(8)                                                   HDU14110
      DY(6)=Y(9)                                                   HDU14120
      HDXX1=+CX*Y(14)                                              HDU14130
      HDXX2=+CX*Y(15)                                              HDU14140
      HDXX3=+CX*Y(16)                                              HDU14150
      DY(11)=T5*V1CX1+(T6*(HDXX1-Y(11))-T7*(Y(11)-HDXX1))/B+DY(11) HDU14160
      DY(12)=T5*V2CX2+(T6*(HCXX2-Y(12))-T7*(Y(12)-HDXX2))/B+DY(12) HDU14170
      DY(13)=T5*V3CX3+(T6*(HCXX3-Y(13))-T7*(Y(13)-HDXX3))/B+DY(13) HDU14180
      DY(14)=-X1CH1/B                                              HDU14190
      DY(15)=-X2CH2/B                                              HDU14200
      DY(16)=-X3CH3/B                                              HDU14210
      GO TO                                                        HDU14220
26    HDX=Y(11)*Y(14)+Y(12)*Y(15)+Y(13)*Y(16)                     HDU14230
      T9=HDX/A                                                     HDU14240
      WRITE (6,57)                                                 HDU14250
      CALL PNEST (13,MACH,TALPH,KF)                                HDU14260
      KF=KF*TICC*T5/Y(1)                                          HDU14270
      CALL PNEST (44,MACH,TALPH,KTA)                               HDU14280
      KTA=KTA*ALPSQ                                                HDU14290
      CALL PNEST (15,MACH,TALPH,KT)                                HDU14300
      KT=KT+KTA                                                    HDU14310
      TK=TI1*T5*KT                                                 HDU14320
      CALL PNEST (41,MACH,TALPH,KLA)                               HDU14330
      KLA=KLA*ALPSQ                                                HDU14340
      KL=KL+KLA                                                    HDU14350
      CALL PNEST (42,MACH,TALPH,KMA)                               HDU14360
      KMA=KMA*ALPSQ                                                HDU14370
      KM=KM+KMA                                                    HDU14380
      CALL PNEST (43,MACH,TALPH,KHA)                               HDU14390
      KHA=KHA*ALPSQ                                                HDU14400
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KH=KH+K+A                                        +DUI4410
CALL PNEST (17,MACH,TALPH,KA)                    +DUI4420
KA=KA*TI1*VT*T9                                  +HDUI4430
CALL PNEST (24,MACH,TALPH,KE)                    +HCUI4440
KE=KE*T10*E*VTSQ                                 +DUI4450
AM=(Y(2)-TSRI)*CTS+ISRIST                        +DUI4460
CALL PNEST (25,AM,TALPH,TS)                      +DUI4470
TS=TS*CTS*TSCF*CCRS                              +DUI4480
TO=-KA+KE+TS                                     +HDUI4490
TI2=DY(1)*RNESQ2*TS                              +HDUI4500
DY(7)=-KF*VICX1                                  +HCUI4510
DY(8)=-KF*V2CX2                                  +DUI4520
DY(9)=-KF*V3CX3                                  +CUI4530
TOTI2=TC+TI2                                      +HCUI4540
DY(11)=TK*(VDOTX*Y(14)-V1)+Y(14)*TOTI2           +DUI4550
DY(12)=TK*(VDOTX*Y(15)-V2)+Y(15)*TOTI2           +DUI4560
DY(13)=TK*(VDOTX*Y(16)-V3)+Y(16)*TOTI2           +HDUI4570
GO TO 2E                                          +DUI4580
27  GO TO (25,26,28,30), I8                       +DUI4590
26  DKDB=0.                                        +HDUI4600
DY(7)=C.                                          +DUI4610
DY(8)=C.                                          +DUI4620
DY(9)=C.                                          +DUI4630
25  TO=-DENS*C22*(KDB+CKDB)*VT                     +CUI4640
COSAE=CCS(SQRT(ALPE))                             +DUI4650
COSAVT=COSAE/VT                                   +HDUI4660
ALP1=T4*(V1*COSAVT+ALPQ1)                         +HDUI4670
ALP2=T4*(V2*COSAVT+ALPQ2)                         +DUI4680
ALP3=T4*(V3*COSAVT+ALPQ3)                         +DUI4690
DY(7)=(ALP1+TO*V1)/Y(1)-G1+NU1+DY(7)             +DUI4700
DY(8)=(ALP2+TO*V2)/Y(1)-G2+NU2+DY(8)             +CUI4710
DY(9)=(ALP3+TO*V3)/Y(1)-G3+NU3+DY(9)             +CUI4720
DY(4)=Y(7)                                        +HDUI4730
DY(5)=Y(8)                                        +DUI4740
DY(6)=Y(9)                                        +DUI4750
GO TO 33                                          +DUI4760
30  WRITE ((6,57)                                  +DUI4770
CALL PNEST (13,MACH,TALPH,KF)                     +DUI4780
CALL PNEST (15,MACH,TALPH,KT)                     +DUI4790
CALL PNEST (44,MACH,TALPH,KTO)                    +CUI4800
KT=KT+KTC*ALPE                                    +HDUI4810
CALL PNEST (42,MACH,TALPH,KMA)                    +CUI4820
KM=KM+KMA*ALPE                                    +HDUI4830
CALL PNEST (41,MACH,TALPH,KLA)                    +CUI4840
KL=KL+KLA*ALPE                                    +CUI4850
CALL PNEST (43,MACH,TALPH,KHA)                    +CUI4860
CALL PNEST (8,MACH,TALPH,KF)                      +CUI4870
KH=KH+KF*ALPE                                     +CUI4880
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      TO=KL*KA*VTSQ/Y(10)
      TO=TO+CSG*KF*KT*Y(10)
      TO=TIO*VTSQ*TO
      ALPA=A*KL/TO
      ALPE=Y(1)*DSQ*KT/TO
      T1=ALPE-ALFA
      T2=T2*KL
      IF (IKL.EC.12) GC TC 31
      ALPQ1=TI*(V2*DY(9)-V3*DY(8))+ALPB*(V2*G2-V3*G2)
      ALPQ2=TI*(V3*DY(7)-V1*DY(9))+ALPB*(V3*G1-V1*G3)
      ALPQ3=TI*(V1*DY(8)-V2*DY(7))+ALPB*(V1*G2-V2*G1)
      GO TO 32
31    ALPQ1=V2*V1/VTSQ
      ALPQ2=-1.+V2**2/VTSC
      ALPQ3=V3/VTSQ
32    ALPE=ALFC1**2+ALPQ2**2+ALPQ3**2
      DKCB=DKCB*ALPE*CSQ
      T1=T2*SL*VTSQ
      T2=TIO*KF*Y(10)*G
      TALPH=ALPE
      ALFE1=ALPC2*V3-ALPQ3*V2
      ALFE2=ALFC3*V1-ALPG1*V3
      ALFE3=ALPG1*V2-ALPQ2*V1
      RMASS=1./Y(1)
      DY(7)=(T1*ALPQ1+T2*ALPE1)*RMASS
      DY(8)=(T1*ALPQ2+T2*ALPE2)*RMASS
      DY(9)=(T1*ALPQ3+T2*ALPE3)*RMASS
      CALL PNEST(I7,MACH,TALPH,KA)
      DY(10)=-TIO*D*KA*VT*Y(10)/A
      GO TO 25
33    IEPD=5
      IF (IFIRST.EQ.1) CALL SPRINT (Y,DY,1)
34    RETLRN
35    TO=SQRI(RSQ-Y(4)**2)
      EC=Y(5)+REARTH-TO
      GO TO (36,42),J2
36    T1=Y(8)+(Y(7)+Y(4)/TO)
      T2=REARTH+EC
      GPF=REARTH*EC/T2
      IF (EC.GT.90000.) GO TC 41
      IF (GPF.LE.FA(1)) GC TC 42
      IF (GPF.LE.HA(IMZ+2)) GO TO 38
      IMZ=IMZ+1
      GO TO 35
37    IF (GPF.GE.FA(IMZ+1)) GO TO 39
      IMZ=IMZ-1
      GO TO 35
39    TEMF=TM(IMZ+1)+ALM(IMZ+1)*(GPH-HA(IMZ+1))
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      CY(3)=(-.034163154744*Y(3)*RSQ*T1)/(TEMP*T2**2)             +CUI15370
      PA=Y(3)*22.48085431*PRESF                                   +CUI15380
      TO=EC                                                       +CUI15390
      DENS=(Y(3)/TEMP)*.76801917C2*DENSF                          +CUI15400
      TEMP=TEMP*TEMPF                                             +CUI15410
   40 VAS=20.C468C276*SQRT(TEMP)                                  +CUI15420
      GO TO (2,13,14), I4                                         +CUI15430
   41 GPH=EC                                                      +CUI15440
      GO TO 21                                                    +CUI15450
   42 IMZ2=0                                                      +CUI15460
      GO TO 35                                                    +CUI15470
   43 TO=EC*AM TOF                                                +CUI15480
      IF (TO.LE.0.) GC TC 46                                      +CUI15490
      IF (TO.LE.ATM(IMZ1+8)) GO TO 45                             +CUI15500
      IMZ1=IMZ1+7                                                 +CUI15510
      IF (IMZ1.LT.NATM) GC TO 44                                  +CUI15520
      WRITE (6,52)                                                +CUI15530
      GO TO IER, (56)                                             +CUI15540
   45 IF (TO.GE.ATM(IMZ1+1)) GO TO 47                             +CUI15550
      IMZ1=IMZ1-7                                                 +CUI15560
      GO TO 45                                                    +CUI15570
   46 IMZ1=0                                                      +CUI15580
   47 T1=(TO-ATM(IMZ1+1))/(ATM(IMZ1+8)-ATM(IMZ1+1))               +CUI15590
      WBX=ATM(IMZ1+2)+T1*(ATM(IMZ1+9)-ATM(IMZ1+2))               +CUI15600
      WSX(1)=WBX                                                  +CUI15610
      WSZ=ATM(IMZ1+3)+T1*(ATM(IMZ1+10)-ATM(IMZ1+3))              +CUI15620
      WBZ=WSZ                                                     +CUI15630
      IF (TO.LE.0.) GO TO 50                                      +CUI15640
      IF (TO.LE.ATM(IMZ2+11)) GO TO 49                            +CUI15650
      IMZ2=IMZ2+7                                                 +CUI15660
      IF (IMZ2.LT.NATM) GO TO 48                                  +CUI15670
      WRITE (6,53)                                                +CUI15680
      GO TO IER, (56)                                             +CUI15690
   49 IF (TO.GE.ATM(IMZ2+4)) GO TO 51                             +CUI15700
      IMZ2=IMZ2-7                                                 +CUI15710
      GU TO 49                                                    +CUI15720
   50 IMZ2=0                                                      +CUI15730
   51 T1=(TO-ATM(IMZ2+4))/(ATM(IMZ2+11)-ATM(IMZ2+4))             +CUI15740
      TEMP=ATM(IMZ2+7)+T1*(ATM(IMZ2+14)-ATM(IMZ2+7))            +CUI15750
      TEMP=TEMF+273.15                                            +CUI15760
      DENS=(ATM(IMZ2+5)+T1*(ATM(IMZ2+12)-ATM(IMZ2+5)))*.00220406262Z22 +CUI15770
      PA=(ATM(IMZ2+6)+T1*(ATM(IMZ2+13)-ATM(IMZ2+6)))*22.48085431  +CUI15780
      GO TO 4C                                                    +CUI15790
   52 FURMAT (24H EXCEEDS METRO FCR WINDS)                        +CUI15800
   53 FORMAT (42H ERROR METRC EXCEEDED FOR DENSITY AND TEMP)      +CUI15810
   54 FORMAT (15H ROUNC TUMBLED,2F10.3,A5,I5)                     +CUI15820
   55 FORMAT (27H ALPHA VDX GREATER THAN Vt ,2F10.3,A5,I5)        +CUI15830
   57 FORMAT (21H GONE TC PREST FM DER)                           +CUI15840
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56    RETURN
      END
      SUBROUTINE SPRINT (Y,CY,INEST)
      DIMENSION Y(16), DY(16), LE(1), QE(1), SX(1)
      COMMON LE, MTBST, RN, RK, R2TEM, RNE, C, E, LL, GO, TBMST, TBST, IST, PE,
     1 AE, LZI, ETB, EPB, EUB, EXI, EZI, SRIST, TSRBST, TSRBST, QE, IF2, TDI,
     2 CXI, LZI, MDI, DELIB, DETFF, XICEL, XIMAX, IH2B, TSRIST, RS, QE, IF2,
     3 IH3, IF, BC, SL, UO, SPN, IXI, IX2, IU, AZU, EU, TEM, IL, TDI,
     4 TSRE, TSQF, TCFF, PTB, PTFF, AZD, MTBM, MF, MTB, ISP, TSRI,
     5 PHMCB, THMCB, CGTBM, CGTBM, ATBM, ATC, BTBM, LAT, AZ, TMCB, UMCB,
     6 TEMPF, SL6D, TI, XI, ZI, YI, WSX, WEX, WBZ, DENSF, PRESF,
      COMMON ATM(700), IMZI, IMZ, IMZ2, ATM, J2, IDGREE(1), IROI,
     1 IREDLC, IUPLEG, IUNIT, ISPRT, RSET, ICURE, ISTIM, ISCOUT,
     2 I3DBUF, I2DP, ISAVEC, ITONQE, IXIAYI, I5DIG, IX2N, IUN, LAM(3),
     3 A, SINCE, COSGE, LSQ, IKL, GEOLT, XOUT(1), YOUT, ZCUT, TUF,
     4 AA, ILI, AZU1, EUL, EC, PPL, PP2, FPP1, PPP2, ETB, CON, ICRN,
     5 CENS, PA, VAS, RILFB, R2TBSQ, RETBQ, RK12, RK2, KNESU2, RTTE, TRCONS,
     6 D44, GCRS, SG, RILFB, R2TBSQ, RETBQ, RK12, ICI, HDX, CTS, TI, T2, T3,
     7 IEPD, IS, I3, I4, I5, I6, I7, I8, I9, NEX, ILSA, IYP,
     8 ICNP, TST, IT, ITTT, IFERR, ALPU1, ALFU2, ALPU3, CODE, D22,
     9 T4, TS, TALPH, THETA, ALPE, ALPU1, PMTOF, TJ(2900), VT, V2, V3, TSTAR, KDE,
     A IFIRST, ICCT3, PHI, I6LP, R3, ALPTA, VT, V2, V3, TSTAR, KDE,
     B ICOT2, KCT3, XDX, KH, DKDB, DKDBA, MACH, ISUN, SINLAT, COSLAT,
     C KM, KL, COSAZ, SINC, CGSD, DEL
      COMMON /ERR/ IER
      COMMON /ECH/ TMCPHI, AMTCIN, AMTOKN, AMTCMH, FTOM2, CVDTOR, CVMTOR, RSQF
     1 CTOM, TMCFHI, AMTCIN, AMTCMH, FTOM2, CVDTOR, CVMTOR, RSQF
     2 HA(23), TM(23), ALM(22), HEAD(165)
      REAL IF2B, IH3B, IF2, IH3, IU, IUI, IUN, IST, ISP, IXI, IX2, IX2N,
     1 KDB, LAR, LAT, LE, LL, LZI, CI, F, MTB, MTBM, MTBST, MACH,
     2 KM, KL, KT, KH
      DATA PI2/3.14159265/ PI2, 3.141592654, 1.570796327/
      GO TO (49, 51), INEST
      GO TO (49, 52, 51, 29, 2, 2), IEPD
 1  2 IF IRST=C
      UN=SQRT(Y(7)**2+Y(8)**2+Y(5)**2)
      ARSIN=AS  ARCS IN
      PHI=PDTCM*RTOD*ARSIN(Y(8)/UN)
      THETA=PLTOM*RTOD*ATAN(Y(9)/Y(7))
      YP=EC
      IF (IYP.EU.C) YP=Y(5)
      UN=PMTCF*UN
      IF ((I6CF.EC.1) GO TC 3
      T1=Y(IUC)/TMOPHI
      T2=RTOC*SCRT(ALPE)
      AE1=ALFC1
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      AE2=ALFC2
      AE3=ALPC3
      GO TO 4
    3 T1=0.
      IF (A.GT.0.) T1=HDX/(TWCPHI*A)
      T2=RTOC*ALPHA
      AE1=Y(14)
      AE2=Y(15)
      AE3=Y(16)
    4 IF (T2.GT.0.) GO TO 5
      PSI=0.
      GO TO 6
    5 T3=(V1*AE3-V3*AE1)*VT
      T4=V1*(V1*AE2-V2*AE1)-V3*(V2*AE3-V3*AE2)
      IF (T3.NE.0..OR.T4.NE.0.) GO TO 500
      PSI=0.
      GO TO 6
  500 PSI=ATAN2(T3,T4)
      IF (PSI.GE.0.) GO TO 6
      PSI=TWCFI+PSI
    6 PSI=RTCC*PSI
      IF (I16CF.EQ.1) GO TO 7
      T3=KDB+CKCB
      GO TO 8
    7 T3=KDB+CKCBA
    8 IF (T1.GT.2C.) GO TO 9
      TJ(IT+11)=0.0
      TJ(IT+12)=0.0
      GO TO 10
    9 T6=CENS*C33/Y(1)
      T4=T6*(KL-KT*(Y(1)*C22/A))
      T5=T6*(KL-T2+KH*(Y(1)*C22/B))
      T6=KM*CENS*C22*D33/B
      T7=TWUPT+I*T1*D**A/(B*VT)
      SDY=2.*T4/T5
      SGY=T7**2/(4.*T6)
      IDY=0
      IGY=0
      IF (1./SGY.LT.1.) GO TC 10
      IGY=1
      IDY=1
   10 GO TO 11
      IF (1./SGY.LE.SCY*(2.-SDY)) GO TO 11
      IDY=1
   11 IF (IGY.EQ.1) GO TC 12
      SGY=TJ(IT+18)
      ENCODE (10,58,TJ(IT+11))SGY
      GO TO 13
C
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C       12  SGY=TJ(IT+11)
            ENCODE (10,59,TJ(IT+11) )SGY
        13  IF (ICY.EQ.1) GO TO 14
            SDY=TJ(IT+12)
            ENCODE (10,58,TJ(IT+12) )SDY
            GO TO 15
C       14  SDY=TJ(IT+12)
            ENCODE (10,59,TJ(IT+12) )SCY
C       15  TJ(IT+1)=Y(2)
            TJ(IT+2)=PMTOF*Y(4)
            TJ(IT+3)=PMTOF*YP
            JAH=0
            TJ(IT+4)=PMTOF*Y(6)
            TJ(IT+5)=LN
            TJ(IT+6)=PHI
            TJ(IT+7)=THETA
            TJ(IT+8)=T1
            TJ(IT+9)=T2
            TJ(IT+14)=ICOT1
            TJ(IT+10)=PSI
            TJ(IT+13)=CODE
            IT=IT+14
            IF (I16CF.EQ.0) GO TO 25
            TJ(IT+E41)=Y(2)
            IF (ISLN.EQ.1) GO TO 16
            TJ(IT+E42)=0.
            GO TO 22
        16  TLHA=DEL+7.27220521E-5*Y(2)+(Y(4)*SINAZ+Y(6)*COSAZ)/(REARTH*COSLAT)
            IF (TLHA+4-FI.GE.0.) GO TO 17
            TMERID=TLHA
            GO TO 19
        17  IF (TLHA-TWOPHI.GE.0.) GO TO 18
            TMERID=TWOPFI-TLHA
            GO TO 19
        18  TMERID=TLHA-TWOPHI
        19  SINH=SINLAT*SIND+COSLAT*COSD*COS(TMERID)
            H=ASIN(SINH)
            Z=ARCOS((SIND-SINLAT*SINH)/(COSLAT*COS(H)))
            IF (TLHA-PI.LT.0.) GO TO 20
            IF (TLHA-TWOPHI.GE.0.) GO TO 20
            THE=PI2-Z
            GO TO 21
        20  THE=Z-PI-PI2
        21  PH=PI2-H
C           CALL SINCCS (PH,SINPH,CCSPH)
            SINPH=SIN(PH)
            COSPH=CCS(PH)
```

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```
      CALL SINCOS (THE,SINTH,COSTH)
C     SINTH=SIN(TH)
      COSTH=COS(TH)
      S1=COSAZ*SINPH*SINTH+SINAZ*SINPH*COSTH
      S2=COSPH
      S3=COSAZ*SINPH*COSTH-SINAZ*SINPH*SINTH
      TJ(ITT+842)=RTOD*ASIN(S1*Y(14)+S2*Y(15)+S3*Y(16))
   22 T1=Y(14)
      T2=Y(16)
      TJ(ITT+844)=RTOD*ATAN2(T2,T1)
      T1=SQRT(T1**2+T2**2)
      T2=Y(15)
      TJ(ITT+843)=RTOD*ATAN2(T2,T1)
      IF (PP1.NE.10000.) GO TO 23
      GO TO 24
   23 T1=-(T5*PP1-T7*T4+PPP1)/(2.*PP1-T7)*1000.
      T2=-(T5*PP2-T7*T4+PPP2)/(2.*PP2-T7)*1000.
      ENCODE (40,60; TJ(ITT+845) )T1,T2,PP1,PP2
   24 TJ(ITT+845)=T1
      TJ(ITT+846)=T2
      TJ(ITT+847)=PP1
      TJ(ITT+848)=PP2
      TJ(ITT+849)=TSTAR
      TJ(ITT+850)=Y(1)
      TJ(ITT+851)=B/FTOM 2
      TJ(ITT+852)=XDX
      TJ(ITT+853)=COCE
      TJ(ITT+854)=ICOT2
      IIT=IIT+14
   25 IF (ISPRT.EQ.0) GO TO 26
      TJ(IT+1667)=Y(2)
      TJ(IT+1668)=PMTCF*Y(7)
      TJ(IT+1669)=PMTOF*Y(8)
      TJ(IT+1670)=PMTOF*Y(9)
      TJ(IT+1671)=PMTCF*CY(7)
      TJ(IT+1672)=PMTOF*DY(8)
      TJ(IT+1673)=PMTOF*DY(9)
      TJ(IT+1674)=2.5464750&8&*T3
      TJ(IT+1675)=MACH
      TJ(IT+1676)=Y(1)
      TJ(IT+1677)=PMTOF*VT
      TJ(IT+1678)=CODE
      TJ(IT+1679)=ICCT3
   26 IF (I5LIG.EC.1) GO TO 54
   27 IF (ICCI1.EC.IC1) GC TC 28
      IC 1=ICCI1
      ICNF=ICNP+1
   28 IF (ICNF.GE.56) GO TO 291
```

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```
      GO TO (252,29), J7
  25  ICNP=ICNP+1
      GO TO (57,57,57,46,57), NEX
 291  JAH=1
      GOTC 30
 292  IF(JAH.EC.1)GOTO 45
  30  K=27
      IF (PMTCF.EC.1.) K=14
      II=0
      J=2
      KI=K
      KII=KI+12
      IF (IYF.EQ.0) GC TC 31
      WRITE (6,61) (HEAD(II),I=1,13)
      GO TO 32
  31  WRITE (6,61) (HEAD(II),I=157,169)
  32  WRITE (6,62) (HEAD(II),I=KI,KII)
  33  WRITE (6,63)
      J=J+1
  34  KI=II+1
      KII=KI+13
      WRITE (6,64) (TJ(I),I=KI,KII)
      J=J+1
      IF (J.EC.58) GO TO 36
      IF (IIT.EQ.II+14) GO TO 35
      II=II+14
      IF (TJ(II).EQ.TJ(II+14)) GC TO 34
      GO TO 33
  35  WRITE (6,63)
  36  GO TO (37,41), J7
  37  IF (TJ(53).EQ.0) GO TO 40
      IF (J.NE.58) WRITE (6,63)
      II=841
      J=2
      KI=K+39
      KII=KI+12
      WRITE (6,61) (HEAD(II),I=40,52)
      WRITE (6,62) (HEAD(II),I=KI,KII)
      WRITE (6,63)
      J=J+1
  38  KI=II+13
      WRITE (6,65) (TJ(I),I=II,KII)
      J=J+1
      IF (J.EC.58) GO TO 40
      IF (IIT.EQ.II-827) GO TC 40
      II=II+14
      IF (TJ(II-1).EQ.TJ(II+13)) GO TO 39
      GO TO 38
```

```
40    ITT=0
      GO TO 42
41    IF (Y(2).LT.IE6) GO TC 37
      IF (I6CF.EC.1) GC TO 37
42    IF (ISFFT.EC.0) GO TO 45
      IF (J.NE.58) WRITE (6,63)
      II=1681
      J=2
      K=105
      IF (PMTCF.EC.1.) K=92
      KII=K+12
      WRITE (6,61) (HEAD(I),I=79,91)
      WRITE (6,62) (HEAD(I),I=K,KII)
43    WRITE (6,63)
      J=J+1
      IF (TJ(1652).EQ.0.) GC TO 45
44    KII=II+12
      WRITE (6,66) (TJ(I),I=II,KII)
      J=J+1
      IF (TJ.EC.58) GO TO 45
      II=II+14
      IF (TJ(II-1).EQ.TJ(II+13)) GO TO 44
      GO TO 43
45    IT=0
      ICAP=3
      J7=2
      GO TO (57,57,57,46,57), NEX
46    WRITE (6,63)
      II=270C
      J=2
      KI=144
      IF (PMTCF.EC.1.) KI=121
      KII=KI+12
      WRITE (6,61) (HEAD(I),I=118,130)
      WRITE (6,62) (HEAD(I),I=KI,KII)
47    WRITE (6,63)
      J=J+1
      IF (TJ(2709).EQ.0.) GC TO 49
48    KII=II+5
      WRITE (6,67) (TJ(I),I=II,KII)
      J=J+1
      IF (ITTT.EQ.0) GC TC 49
      IF (ITTT.EC.II-2690) GC TO 49
      II=II+1C
      IF (TJ(II-1).EQ.TJ(II+5)) GO TC 48
      GO TO 47
49    ITTT=0
```

```
      DO 50 I=1,2700
   50 TJ(I)=0.
      GO TO 55
   51 J7=1
      NEX=4
      GO TO 2
   52 J7=1
      NEX=4
      GO TO 30
   53 IF (ISC(LT).EQ.0) GO TO 56
   54 XOLT=Y(4)
      YOLT=Y(5)
      ZOLT=Y(6)
      TOF=Y(2)
      AA=IX2*AMTOF
      IU1=IL*AMTOKN
      AZU1=AZL
      EU1=EU
      LTL=UO*AMTOF
      GECUT=GE(1)
      TEMPN=TEMFF
      DENSN=DENSF
      WX=WBX*AMTOMH
      WZ=WBZ*AMTOMH
      CUN=COLE
      IDAN=IDCCE
      IF (I15LIG.EQ.0) GO TO 56
      GO TO 27
   56 CONTINUE
   57 RETURN
   58 FORMAT (F10.6)
   58 FORMAT (F8.4,2H *)
   60 FORMAT (4F10.7)
   61 FORMAT (1H1,13A10)
   62 FORMAT (13A10)
   63 FORMAT (1H )
   64 FORMAT (F10.5,3F10.3,4F10.2,F10.5,2A10,1X,A5,F5.0)
   65 FORMAT (4F10.5,4A10,F10.2,F10.3,F10.7,1X,A5,F5.0)
   66 FORMAT (F10.5,6F10.4,F10.7,F10.6,F10.3,F10.4,11X,A5,F5.0)
   67 FORMAT (2X,F10.4,5X,6(F10.8,5X),F10.4,2X,A5,F5.0)
      END
      SUBROUTINE AERCH
      DIMENSION B(16600), C(7), A(8), IND(45), MULTI(45)
      REAL MULTI
      COMMON /AERCB/ E
      DATA INC /1, 2, 3, 4, 5, 6, 24, 7, 8, 5, 9, 10, 11, 11,
     219, 15, 15, 19, 13, 13, 14, 26, 15, 16, 17, 25, 27, 26, 25, 15,
     2    15, 19, 15, 19, 15, 19, 20, 21, 22, 23, 23/
```

```
      DATA MULTI /1., .3926990816, ..3926990816, ..3926990816,
     1 ..3926990816, -.3926990816, 1., -.3926990816, 1., -.3926990816,
     2 ..3926990816, -.3926990816, 1., -.3926990816, 1., -.3926990816,
     3, 1., 1., 1., .3926990816, 1., 1., .3926990816, 1., -.3926990816,
     4 1., 1., 1., .3926990816, 1., 1., .3926990816, -.3926990816,
     599080816, -.3926990816, 1./
       DO 1 I=1,16600
     1 B(I)=0.
       WRITE (6,24)
     2 READ (5,28) C,JCBCC,ICNT,MCNT,ICCC,ITYPE
       WRITE (6,28) C,JCBCGO,ICNT,MCNT,ICCC,ITYPE
       IF (ITYPE.EQ.0) GO TO 19
       IF (ITYPE.EQ.2.OR.ITYPE.EQ.6) GC TC 9
C      AEROPACK CPTION SET AT 6
       IF (ITYPE.EQ.1.OR.ITYPE.EQ.5) GC TC 3
       WRITE (6,27) ITYPE
       STOP
     3 DECCDE (79,21) A(1),(C(I),I=1,6)
CC     IF (ITYPE.EQ.1) GO TO 5
       DO 4 I=1,5
     4 C(I)=MULTI(ICOD)*C(I)
       I=(INC(ICOD)-1)*572+1
       B(I)=1.
       B(I+1)=E(I+1)+6.
       J=E(I+1)+1.+FLOAT(I)
       IF (B(I+1).EQ.6.) GC TC 6
       IF (C(6).GT.B(J-6)) GO TO 6
       WRITE (6,25) ICCC,C(6)
       STOP
     6 K=J-5
     7 II=1
       DO 8 I=K,J
     8 E(I)=C(III)
       II=II+1
       GO TO
C      THIS CFTION USED ONLY
     9 DECODE (79,22) A(1),C,ICNT
       IF (ITYPE.EQ.2) GO TO 11
    10 DO 10 J=1,6,2
CCC    C(J)=C(J)*MULTI(ICCD)
    11 CO 12 J=2,6,2
    12 C(J)=.C030461742*C(J)
       I=(INC(ICOD)-1)*572+1
       B(I)=2.
       J=I+35
       IF (B(I+1).EQ.0.) J=J-19
    12 IF (B(J).EQ.0.) GO TC 14
       J=J+15
```

```
      GO TO 13
14    IF (ICNT.EQ.1) GO TO 16
      IF (C(7).EQ.B(J-19)) GO TO 15
      WRITE (6,26) ICOO,C(7),E(J-19)
      WRITE (6,30)
      STOP
15    IF (ICNT.EQ.3) GO TO 18
      K=J-31
      J=J-26
      GO TO 7
16    IF (B(I+1).EQ.0.) GO TO 17
      IF (C(7).GT.B(J-19)) GO TO 17
      WRITE (6,25) ICOD,C(7)
      STOP
17    B(J)=C(7)
      E(I+1)=E(I+1)+19.
      K=J-18
      J=J-13
      GO TO 7
18    K=J-25
      J=J-20
      GO TO 7
19    WRITE (6,29)
      RETURN
20    FORMAT (7A10,A7,I2,I1)
21    FORMAT (6E12.8,5X,I2)
22    FORMAT (7E10.5,3X,I2,2X,I2)
23    FORMAT (25X,7A10,A7,I2,I1)
24    FORMAT (1H1,55X,19HAERODYNAMIC PACKAGE//)
25    FORMAT (27H AERC IS OUT OF ORDER CODE,I4,12H BREAK POINT,E15.7)
26    FORMAT (48H TYPE 2 OR 6 AERO SECOND CR THIRD CARD MACH NO. ,6HWRON-
     1G  ,I4,9H FOR MACH,E15.7,9H AND MACH,E15.7)
27    FORMAT (31H ERROR COLUMN 80 OF AERC WAS A ,I2,23H INSTEAD OF A 1,2
     1,5,OR6)
28    FORMAT (7F10.4,I3,I2,I2,I1)
29    FORMAT (16H LEAVING AERC(SUB))
30    FORMAT (19H STOPPED AT AERC 14)
31    FORMAT (19H STOPPED AT AERC 16)
      END
      SUBROUTINE PNEST (II,AM,ALPHA,R)
      DIMENSION B(166CO), RA(2), IND(45)
      COMMON /AEROB/ B
      COMMON /ERR/ IER
      DATA INC /1, 2, 3, 4, 5, 6, 24, 7, 8, 5, 9, 10, 11, 11,
     1 12, 12, 13, 13, 14, 26, 15, 16, 17, 25, 27, 28, 25, 15,
     219, 15, 19, 19, 15, 19, 19, 20, 21, 22, 23, 23, 23/
      I=(INC(II)-1)*572+1
```

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```
N=I+7
BR=AM
K=E(I+1)+1.+FLOAT(I)
IF (B(I+1).EQ.2.) GO TO 4
DO 1 J=N,K,6
IF (BR.LE.B(J)) GO TO 3
1 CONTINUE
2 WRITE (6,11) II,BR
J=J-11
IF (B(I+1).EQ.2.) J=J-15
WRITE (6,10) (B(I),I=J,K)
GO TO 167
3 R=B(J-5)+BR*(B(J-4)+BR*(B(J-3)+BR*(B(J-2)+BR*B(J-1))))
RETURN
4 A2=ALPHA
N=N+13
K=K-15
DO 5 J=N,K,19
IF (BR.GE.B(J).AND.BR.LE.B(J+19)) GO TO 6
5 CONTINUE
GO TO 2
6 JS=J-3
DO 7 I=1,2
K=JS
KK=K-14
DO 7 L=KK,K,2
IF (A2.GE.B(L).AND.A2.LE.B(L+2)) GO TO 8
7 CONTINUE
WRITE (6,12) A2,II,BR
GO TO 2
8 RA(I)=E(L+1)+(B(L-1)-B(L+1))*(A2-B(L+2))/(B(L)-B(L+2))
9 JS=JS+19
R=RA(2)+(BR-B(J+19))*(RA(1)-RA(2))/(B(J)-B(J+19))
RETURN
10 FORMAT (6E15.8)
11 FORMAT (20H AERO EXCEEDED CODE=,I4,12H BREAK POINT,E15.8)
12 FORMAT (10H ALPHA2 OF,E15.8,9H FOR TYPE,I4,12H BREAK POINT,E15.6)
167 RETURN
END
SUBROUTINE COA (PY,CPY)
DIMENSION PY(2),DFY(2)
COMMON /BDH/ REARTH, CC, AMTOMS, PQ, AMTOF, FTCM, ANTOM, KTOD,
CTOM, TWCPHI, AMTOIN, AMTOKN, AMTCMH, FTGM2, CVDTOR, CVMTOR, RSQ,
2 HA(25), TM(25), ALP(25), HEAD(169)
J=2
T2=REAFIT+PY(1)
GPH=REARTH*PY(1)/T2
1 IF (GPH.LE.HA(J)) GC TO 2
```

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```
      J=J+1
      GO TO 1
    2 J=J-1
      TEMP=TM(J)+ALM(J)*(GPH-HA(J))
      CPY(2)=-.034163194474*PY(2)*RSQ/(TEMP*T2**2)
      RETURN
      END
      BLOCK DATA
      COMMON /ECH/ REARTH, GC, AMTOMS, PO, AMTOF, FTOM, ANTOM, RTOD,
     1 DTOM, TWOPHI, AMTOIN, AMTOKN, AMTOMH, FTG/2, CVDTCR, CVMTCR, RSQ/LL
     2 HA(23), TM(23), ALM(22), HEAD(169)
      DATA REARTH, GC, AMTOMS, PO, AMTOF, FTCM, ANTOM, RTOD, CTOM, TWOPH/
     1 I, AMTOIN, AMTOKN, AMTOMH, FTOM2/6.35766EC6, 9.80665, .44704, 1.
     2 .01325EC, 3.28083, 9895, .30481, 1.94384449, 2.23693362, .09290304/
     3 18530, 7.3.37007874, 1.9438444922, 2.23693362$,.09290304/
      DATA CVDTCR, CVMTCR/-.0174532925, .00098174770044/
      DATA RSQ /4.0408473S76756E13/
      DATA HA /0., 11E5, .2E5, .32E5, .47E5, .52E5, .61E5,
     1 .7$E5, .88743E5, .9E5, .1E6, .12E6, .15E6, .16E6, .17E6, .1H
     2 5EE, .2$E6, .3E6, .4E6, .5E6, .6E6, .7E6/
      DATA TM /28C.15, 216.65, 216.65, 270.65, 270.65, 960.65,
     1 252.65, 180.65, 180.65, 210.65, 260.65, 360.65, 960.65,
     2 110.65, 1210.65, 1350.65, 1550.65, 1830.65, 2160.65, 2426.65, 25
     3 90.65/
      DATA ALM /-.0065, .C, .001, .0028, 0., -.0023, -.0043, 0.,
     1 0., .0026, .0017, .0011/
      DATA HEAD/169*4H    /
      DATA HEAD /7H TIME,  6H EI,  6H  E2,  6H  E3, 6
     1H     , 8H GAMMAV, 8H GAMMAE, 7H  SPIN, 8H ALPHAR, 10HPHI ALP
     2HAR, 10H GYROSCOPI, 9HC DYNAMIC, 7H CODE, 7H  SEC, 6H  M2, 6
     3H        , M, 8H M/SEC, MIL, 10H  MIL, 9H REV/SEC, 7H  REV/SEC, 6
     4H        , DEG, 10H STABILITY, 10H STABILITY, 1H , 7H  SEC, 7
     5, 6H  FT, 6H  FT, 6H   FT, 7H  DEG, 10H STABILITY, 1H  DEG, 1
     6, 6SH REV/SEC, 7H  DEG, 10H  DEG, 7H  DEG, 10H STABILITY, 1H DEG, 1
     7H, 7H  TIME, 10H SIGMA N, 8H  EULEL, 10H STABILITY, 10H LAMBDAN, 1
     8, 9H LAPECAP, 9H NLT RATE, 10H PREC RATE, 8H THRUST, 8H WEIGHT, 7
     9, 1H, 7H     , X.X, 7H      , 1H     SEC, 7H    DEG, 7H  DEG, 7
     AH  DEG, 1CH 10**3/CAL, 1CH 10**3/CAL, 9H RAD/CAL, 9H RAD/CAL, 7HH
     BH, 6H   LB, 8H  LB-FT2, 1H  10**3/CAL, 9F RAD/CAL, 9F RAD/CAL, SH
     C RAC/CAL, 6H  DEG, 10H 10**3/CAL, 1CH 10**3/CAL, 1H , 7H TIME, 10H
     D, U1, 6H  U2, 6H  U3, 8H  UDOTll, 8H LB-FT2, 1H  7H  UDOT3, 7H
     E DRAG COEF, 7H MACH, 8H WEIGHT, 6H  V, 1H, 7H  CODE, 7H
     F G SEC, 8H  M/SEC, 8H  M/SEC, 8H  M/SEC2, 8H M/SEC, 8H M/SEC2, 8H F
     G, H8H M/SEC2, 7H  SEC, 6H  CD, 8H NUMBER, 6H  LB, FI/SEC, 8H F
     H, 1T/SEC, 8H FT/SEC2, 8H FT/SEC2, 6H  CD, 8H NUMBER, 6HCU21120
```

```
       END                                                        CDU21220
       SUBROUTINE RKG (CELTA, DERIV, Y, DY, Q, C1, C2, C3)        CDU21430
       DIMENSICN Y(N), DY(N), Q(N), C1(4), C2(4), C3(4)           CDU21440
       IF (J-1) 3,1,3                                             CDU21450
1      DO 2 I=1,N                                                 CDU21460
2      Q(I)=0.0                                                   CDU21470
       WRITE (6,200)                                              CDU21480
       CALL DERIV (Y, DY)                                         CDU21490
       RETURN                                                     CDU21500
3      DO 5 I=1,4                                                 CDU21510
       DO 4 K=1,N                                                 CDU21520
       R=C1(I)*(CY(K)-C2(I)*Q(K))                                 CDU21530
       Y(K)=Y(K)+DELTA*R                                          CDU21540
4      Q(K)=Q(K)+3.0*R-C3(I)*DY(K)                                CDU21550
       WRITE (6,200)                                              CDU21560
       CALL DERIV (Y, DY)                                         CDU21570
5      CONTINUE                                                   CDU21580
200    FORMAT (21H GONE TC DERIV FM RKG)                          CDU21590
       RETURN                                                     CDU21400
       DATA C1(1), C1(2), C1(3), C1(4) /.5, .2928932188134525, 1.70710678 CDU21410
1      1165411, .1666666666667/                                   CDU21420
       DATA C2(1), C2(2), C2(3), C2(4) /2.C, 1.0, 1.0, 2.0/       CDU21430
       DATA C3(1), C3(2), C3(3), C3(4) /.5, .2928932188134525, 1.70710678 CDU21440
1      1186541, .5/                                               CDU21450
       END                                                        CDU21460
```

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